

Radiation Effects on Free Convection Flow Near a Vertical Plate with Ramped Wall Temperature

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Abstract

The effect of radiation on the unsteady natural convection flow past an infinite vertical plate is presented, wherein the plate temperature is a ramped one. The fluid considered here is a gray, absorbing/emitting but a non-scattering medium. The influence of the various parameters entering into the problem on the velocity field, temperature field, skin friction and Nusselt number is studied.

Keywords: Natural Convection, Ramped Wall Temperature, Radiation

1. Introduction

The analysis of free convection flow near a vertical plate has been carried out as an important application in many industries. Numerous investigations are performed by using both analytical and numerical methods. The first exact solution of the Navier-Stokes equation was given by Stokes [1] and explains the motion of a viscous incompressible fluid past an impulsively started infinite horizontal plate in its own plane. This is known as Stokes's first problem in the literature. If the plate is in a vertical direction and gives an impulsive motion in its own plane in a stationary fluid, then the resulting effect of buoyancy force was first studied by Sundalgekar [2] by Laplace transformation technique and the effects of heating or cooling of the plate by free convection currents were discussed. Pohlhausen [3] was among the earlier research workers, who first analyzed the steady free convective flow of a viscous, incompressible fluid past a semi-infinite vertical plate by using integral method. Later on, Ostrach [4] studied the same problem using the similarity solution method. Siegel [5] and Gebhart [6] discussed the unsteady free convective flow of a viscous incompressible fluid, bounded by a semi-infinite vertical wall by using integral and approximation methods, respectively. Several authors (cf. [7-12]) have investigated a number of unsteady free convection flows near a vertical plate under different sets of thermal conditions at the bounding plate.

Practical problems usually occupy wall conditions that

are non-uniform or arbitrary. Therefore, it is very useful to investigate problems subject to step change in wall temperature. Schetz [13,14] developed an approximate analytical model for natural convection flow from a vertical plate with discontinuous wall temperature conditions. However, different techniques were attempted on this problem. Hayday *et al.* [10] used a numerical approach, Kelleher *et al.* [11] and Kao [15] used series expansions. Lee and Yovanovich [12] have attempted to improve the earlier results for step change in wall temperature.

The interaction of natural convection with thermal radiation has increased greatly during the last decade due to its importance in many practical involvements. When free convection flows occur at high temperature, radiation effects on the flow become significant. Radiation effects on the free convection flow are important in context of space technology, processes in engineering areas occur at high temperature. Sundalgekar and Takhar [16] have considered the radiative free convective flow of an optically thin gray-gas past a semi-infinite vertical plate. Radiation effects on mixed convection along an isothermal vertical plate were studied by Hossain and Takhar [17]. Raptis and Perdakis [18] studied the effects of thermal radiation and free convection flow past a moving vertical plate. Das *et al.* [19] have analyzed radiation effects on flow past an impulsively started infinite isothermal vertical plate by the Laplace transform technique.

Recently, Muthucumaraswamy and Janakiraman [20]

studied MHD and radiation effects on moving isothermal vertical plate with variable mass diffusion. Also, Chandran *et al.* [8] have analyzed the unsteady natural convection flow of a viscous incompressible fluid near a vertical plate with ramped wall temperature and they have compared the results with the case of constant wall temperature. The fluid convection resulting from such a wall temperature profile is likely to be of relevance in several industrial applications, especially, where the initial temperature profiles assume importance in design processes. Saha *et al.* [21] investigated the natural convection boundary layer adjacent to an inclined semi-infinite flat plate subjected to ramp heating. Recently, Deka *et al.* [22] have analyzed the unsteady free convection flow of a viscous incompressible fluid past an infinite vertical plate with ramped wall temperature in presence of heat source.

In the present problem, it is proposed to study the effect of thermal radiation on the unsteady free convection flow of a viscous incompressible fluid past an infinite vertical plate containing a ramped type temperature profile with respect to time. Two different solutions corresponding to ramped as well as constant wall temperature, are obtained by Laplace transform technique have been shown separately.

2. Mathematical Formulation

We consider a two-dimensional flow of a viscous incompressible fluid past an infinite vertical flat plate. The fluid considered here is a gray, absorbing/emitting but a non-scattering medium. With respect to an arbitrarily chosen origin on this plate, the x' -axis is taken along the wall in the vertically upward direction, and the y' -axis is taken normal to the plate into the fluid. Initially, for time $t' \leq 0$, both the fluid and the plate are at rest and assumed to be at the same temperature T_∞' . At time $t' > 0$, the temperature of the plate is raised or lowered to $T_\infty' + (T_w' - T_\infty')t'/t_0$, when $t' > t_0$ and thereafter maintained at the constant temperature T_w' for $t' > t_0$.

We assume that the flow is laminar and is such that the effects of the convective and pressure gradient terms in the momentum equations can be neglected (see Currie *et al.* [23]). It is also assumed that the effect of viscous dissipation is negligible. Moreover, as the plate is infinite in extent in the x' -direction, the derivatives of all the flow variables with respect to x' vanish and as a result of the boundary layer approximations, the physical variables are functions of y', t' only. Thus the motion is one dimensional with only non-zero vertical velocity u' varying with y' and t' only. Due to one-dimensional nature, the equation of continuity is trivially satisfied.

Then under usual Boussinesq's approximation, the un-

steady flow is governed by,

$$\frac{\partial u'}{\partial t'} = \nu \frac{\partial^2 u'}{\partial y'^2} + g\beta(T' - T_\infty') \tag{1}$$

$$\frac{\partial T'}{\partial t'} = \frac{k}{\rho C_p} \frac{\partial^2 T'}{\partial y'^2} - \frac{1}{\rho C_p} \frac{\partial q_r}{\partial y'} \tag{2}$$

The initial and boundary conditions are,

$$\left. \begin{aligned} t' \leq 0 : u' = 0, \quad T' = T_\infty', \quad \forall y' \geq 0 \\ \left. \begin{aligned} u' = 0, \quad \text{at } y' = 0 \\ T' = \begin{cases} T_\infty' + (T_w' - T_\infty') \frac{t'}{t_0}, & 0 < t' \leq t_0 \\ T_w', & t' > t_0 \end{cases} \text{ at } y' = 0 \\ u' \rightarrow 0, \quad T' = T_\infty', \quad \text{as } y' \rightarrow \infty \end{aligned} \right\} t' > 0 \end{aligned} \right\} \tag{3}$$

The local radiant for the case of an optically thin gray gas is expressed by,

$$\frac{\partial q_r}{\partial y'} = -4a^* \sigma (T_\infty'^4 - T'^4) \tag{4}$$

It is assumed that the temperature differences with the flow are sufficiently small so that T'^4 may be expressed as a linear function of the temperature, which is accomplished by expanding T'^4 in a Taylor series about T_∞' and neglecting the higher order terms. Thus,

$$T'^4 \cong 4T_\infty'^3 T' - 3T_\infty'^4 \tag{5}$$

By using Equations (4) and (5), Equation (2) reduces to,

$$\rho C_p \frac{\partial T'}{\partial t'} = k \frac{\partial^2 T'}{\partial y'^2} + 16a^* \sigma T_\infty'^3 (T_\infty' - T') \tag{6}$$

Introducing the non-dimensional quantities,

$$\left. \begin{aligned} u = u' \sqrt{\frac{t_0}{\nu}}, \quad t = \frac{t'}{t_0}, \quad y = \frac{y'}{\sqrt{\nu t_0}} \\ T = \frac{T' - T_\infty'}{T_w' - T_\infty'}, \quad Pr = \frac{\mu C_p}{k}, \quad R = \frac{16a^* \sigma T_\infty'^3 \nu t_0}{k} \end{aligned} \right\} \tag{7}$$

the Equations (1) and (2) reduce to,

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial y^2} + T \tag{8}$$

$$Pr \frac{\partial T}{\partial t} = \frac{\partial^2 T}{\partial y^2} - RT \tag{9}$$

According to the above non-dimensional process, the characteristic time t_0 can be defined as,

$$t_0 = \left[\frac{\sqrt{\nu}}{g\beta(T_w' - T_\infty')} \right]^{2/3} \tag{10}$$

and then the initial and boundary conditions in non-dimensional form are,

$$\left. \begin{aligned} t \leq 0: \quad u = 0, \quad T = 0, \quad \forall y \geq 0 \\ \left. \begin{aligned} u = 0, & \quad \text{at } y = 0 \\ T = \begin{cases} t & \text{for } 0 < t \leq 1 \\ 1 & \text{for } t > 1 \end{cases} & \text{at } y = 0 \\ u \rightarrow 0, \quad T \rightarrow 0 & \text{as } y \rightarrow \infty \end{aligned} \right\} t > 0 \end{aligned} \right\} \quad (10)$$

All the physical quantities are mentioned in Nomenclature.

3. Method of Solution

The Equations (8) and (9) subject to the conditions (10) are solved by the usual Laplace-transform technique and the solutions are as follows:

Case I: $Pr \neq 1$

The exact solutions for temperature and velocity are given by,

$$T(y, t) = F_1(y, t) - F_1(y, t-1)H(t-1) \quad (11)$$

$$u(y, t) = \frac{1}{c^2(1-Pr)} \left[\{u_1(y, t) - u_2(y, t)\} - \{u_1(y, t-1) - u_2(y, t-1)\}H(t-1) \right] \quad (12)$$

where, (see the equation at the bottom of this page).

where $c = \frac{R}{Pr-1}$.

Case II: $Pr = 1$.

The exact solutions for temperature and velocity are,

$$T(y, t) = F_1(y, t) - F_1(y, t-1)H(t-1) \quad (13)$$

$$u(y, t) = \frac{1}{R} [u_3(y, t) - u_3(y, t-1)H(t-1)] \quad (14)$$

where,

$$\begin{aligned} F_1(y, t) &= \left(\frac{t}{2} + \frac{y}{4\sqrt{R}} \right) e^{y\sqrt{R}} \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} + \sqrt{Rt} \right) \\ &\quad + \left(\frac{t}{2} - \frac{y}{4\sqrt{R}} \right) e^{-y\sqrt{R}} \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} - \sqrt{Rt} \right) \\ u_3(y, t) &= \left[\left(t + \frac{y^2}{2} \right) \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} \right) - \sqrt{\frac{t}{\pi}} y e^{-y^2/4t} \right] \\ &\quad - \left(\frac{t}{2} + \frac{y}{4\sqrt{R}} \right) e^{y\sqrt{R}} \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} + \sqrt{Rt} \right) \\ &\quad + \left(\frac{t}{2} - \frac{y}{4\sqrt{R}} \right) e^{-y\sqrt{R}} \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} - \sqrt{Rt} \right) \end{aligned}$$

Here, $H(t-1)$ is the unit step function defined, in general as,

$$H(t-a) = \begin{cases} 1, & t \geq a \\ 0, & 0 \leq t < a \end{cases}$$

To differentiate the effect of the ramped temperature distribution from the constant wall temperature on the flow, we compare both solutions obtained. The solutions for temperature and velocity for the flow near an isothermal stationary plate can be obtained as,

$$T = \frac{1}{2} \left[e^{y\sqrt{R}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} + \sqrt{\frac{Rt}{Pr}} \right) + e^{-y\sqrt{R}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} - \sqrt{\frac{Rt}{Pr}} \right) \right] \quad (15)$$

$Pr > 0$

$$u(y, t) = \begin{cases} \frac{1}{c(Pr-1)} [u_4(y, t) - u_5(y, t)], & Pr \neq 1 \\ \frac{1}{R} u_6(y, t), & Pr = 1 \end{cases} \quad (16)$$

$$\begin{aligned} u_1(y, t) &= c \left[\left(\frac{t}{2} + \frac{yPr}{4\sqrt{R}} \right) e^{y\sqrt{R}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} + \sqrt{\frac{Rt}{Pr}} \right) + \left(\frac{t}{2} - \frac{yPr}{4\sqrt{R}} \right) e^{-y\sqrt{R}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} - \sqrt{\frac{Rt}{Pr}} \right) \right] \\ &\quad + \frac{e^{-ct}}{2} \left[e^{y\sqrt{R-cPr}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} + \sqrt{\left(\frac{R}{Pr} - c \right) t} \right) + e^{-y\sqrt{R-cPr}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} - \sqrt{\left(\frac{R}{Pr} - c \right) t} \right) \right] \\ &\quad - \frac{1}{2} \left[e^{y\sqrt{R}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} + \sqrt{\frac{Rt}{Pr}} \right) + e^{-y\sqrt{R}} \operatorname{erfc} \left(\frac{y\sqrt{Pr}}{2\sqrt{t}} - \sqrt{\frac{Rt}{Pr}} \right) \right] \\ u_2(y, t) &= c \left[\left(t + \frac{y^2}{2} \right) \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} \right) - \sqrt{\frac{t}{\pi}} y e^{-y^2/4t} \right] - \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} \right) \\ &\quad + \frac{e^{-ct}}{2} \times \left[e^{iy\sqrt{c}} \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} + i\sqrt{ct} \right) + e^{-iy\sqrt{c}} \operatorname{erfc} \left(\frac{y}{2\sqrt{t}} - i\sqrt{ct} \right) \right] \end{aligned}$$

where,

$$u_4(y,t) = \operatorname{erfc}\left(\frac{y}{2\sqrt{t}}\right) - \frac{e^{-ct}}{2} \left[e^{iy\sqrt{c}} \operatorname{erfc}\left(\frac{y}{2\sqrt{t}} + i\sqrt{ct}\right) + e^{-iy\sqrt{c}} \operatorname{erfc}\left(\frac{y}{2\sqrt{t}} - i\sqrt{ct}\right) \right]$$

$$u_5(y,t) = \frac{1}{2} \left[e^{y\sqrt{R}} \operatorname{erfc}\left(\frac{y\sqrt{Pr}}{2\sqrt{t}} + \sqrt{\frac{Rt}{Pr}}\right) + e^{-y\sqrt{R}} \operatorname{erfc}\left(\frac{y\sqrt{Pr}}{2\sqrt{t}} - \sqrt{\frac{Rt}{Pr}}\right) \right] - \frac{e^{-ct}}{2} \left[e^{y\sqrt{R-cPr}} \operatorname{erfc}\left(\frac{y\sqrt{Pr}}{2\sqrt{t}} + \sqrt{\left(\frac{R}{Pr} - c\right)t}\right) + e^{-y\sqrt{R-cPr}} \operatorname{erfc}\left(\frac{y\sqrt{Pr}}{2\sqrt{t}} - \sqrt{\left(\frac{R}{Pr} - c\right)t}\right) \right]$$

$$u_6(y,t) = \operatorname{erfc}\left(\frac{y}{2\sqrt{t}}\right) - \frac{1}{2} \left[e^{y\sqrt{R}} \operatorname{erfc}\left(\frac{y}{2\sqrt{t}} + \sqrt{Rt}\right) + e^{-y\sqrt{R}} \operatorname{erfc}\left(\frac{y}{2\sqrt{t}} - \sqrt{Rt}\right) \right]$$

4. Nusselt Number and Skin-Friction

We now study the heat transfer coefficient, *i.e.* Nusselt number, which is given in non-dimensional form by,

$$Nu = -\frac{\partial T}{\partial y}\bigg|_{y=0} = F_2(t) - F_2(t-1)H(t-1)$$

where,

$$F_2(t) = \left[t\sqrt{R} + \frac{Pr}{2\sqrt{R}} \right] \operatorname{erf}\left(\sqrt{Rt/Pr}\right) + \sqrt{\frac{Pr}{\pi t}} e^{-Rt/Pr}$$

while, for the isothermal plate,

$$Nu = \sqrt{R} \operatorname{erf}\left(\sqrt{\frac{Rt}{Pr}}\right) + \sqrt{\frac{Pr}{\pi t}} e^{-Rt/Pr}$$

From the velocity field, we now study the skin friction. The non-dimensional form of skin-friction is given by,

$$\tau = -\frac{\partial u}{\partial y}\bigg|_{y=0} = \begin{cases} -\frac{1}{c^2(1-Pr)} [I_1(t) - I_1(t-1)H(t-1)], & \text{for } Pr \neq 1, \\ -\frac{1}{R} [I_2(t) - I_2(t-1)H(t-1)], & \text{for } Pr = 1. \end{cases}$$

where,

$$I_1(t) = \operatorname{erf}\left(\sqrt{\frac{Rt}{Pr}}\right) \left[\sqrt{R} - ct\sqrt{R} - \frac{cPr}{2\sqrt{R}} \right] - c\sqrt{\frac{Pr t}{\pi}} e^{-Rt/Pr} - \sqrt{R-cPr} e^{-ct} \operatorname{erf}\left(\sqrt{\left(\frac{R}{Pr} - c\right)t}\right) + 2c\sqrt{\frac{t}{\pi}} + i\sqrt{c} e^{-ct} \operatorname{erf}(i\sqrt{ct})$$

$$I_2(t) = (e^{-Rt} - 2)\sqrt{\frac{t}{\pi}} + \left(t\sqrt{R} + \frac{1}{2\sqrt{R}} \right) \operatorname{erf}(\sqrt{Rt})$$

Again, the skin friction for isothermal plate is given by,

$$\tau = \begin{cases} -\frac{1}{R} I_3(t), & \text{for } Pr \neq 1 \\ -\frac{1}{R} I_4(t) & \text{for } Pr = 1 \end{cases}$$

where,

$$I_3(y,t) = i\sqrt{c} e^{-ct} \operatorname{erf}(i\sqrt{ct}) + \sqrt{R} \operatorname{erf}\left(\sqrt{Rt/Pr}\right) - \sqrt{(R-cPr)} e^{-ct} \operatorname{erf}\left(\sqrt{(R/Pr-c)t}\right)$$

$$I_4(y,t) = \sqrt{R} \operatorname{erf}\left(\sqrt{Rt}\right) + \frac{e^{-Rt}}{\sqrt{\pi t}} - \frac{1}{\sqrt{\pi t}}$$

5. Results and Discussions

In order to understand the effects of different physical parameters, namely; *Pr* (Prandtl number), *R* (radiation parameter) and *t* (time), on the nature of the flow, computations are carried out for velocity, temperature, Nusselt number and skin friction. The computed results are presented graphically. In all the figures, dotted lines correspond to solutions without ramped wall temperature.

Figures 1-3 display the effect of *t* (time) on the temperature field for the case of air (*Pr* = 0.71). It is observed that temperature increases with an increase in *t* (time). It is also found that the temperature decreases with *y* from its ramped value on the plate to its free stream value for all values of time *t*.

Figure 2 represents the temperature profiles for different values of *Pr* at *t* = 0.5 and *R* = 2.0. It is found that the temperature decreases with an increase in *Pr*. **Figure 3** shows the effect of radiation parameter *R* on the temperature field for fixed values of *t* = 0.5 and *Pr* = 0.71 and demonstrates that the temperature decreases gradually with increasing values of *R*.

From **Figures 1-3** we have presented the temperature variation with the two types of boundary conditions,

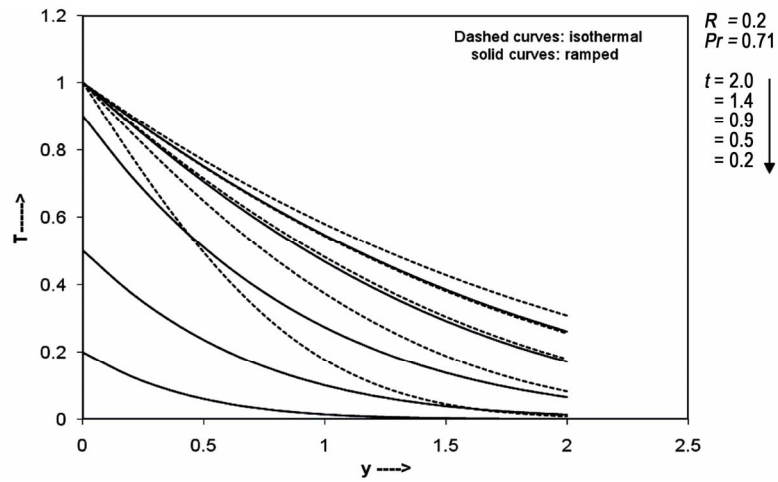


Figure 1. Temperature profile for different time t .

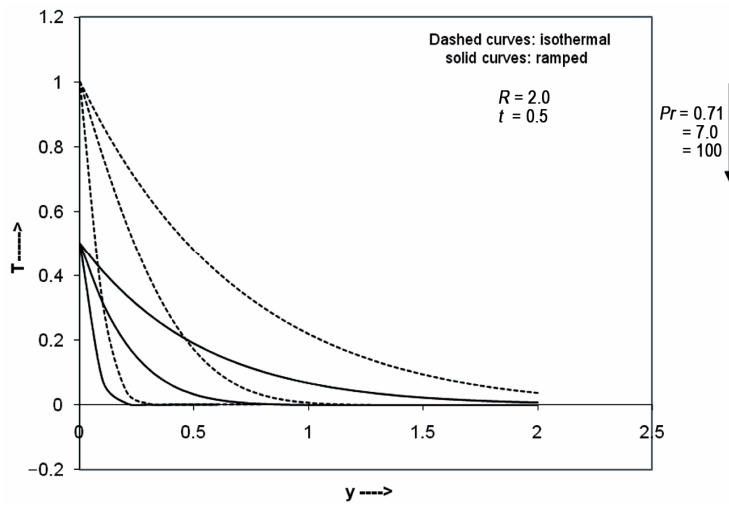


Figure 2. Temperature profile for different Pr .

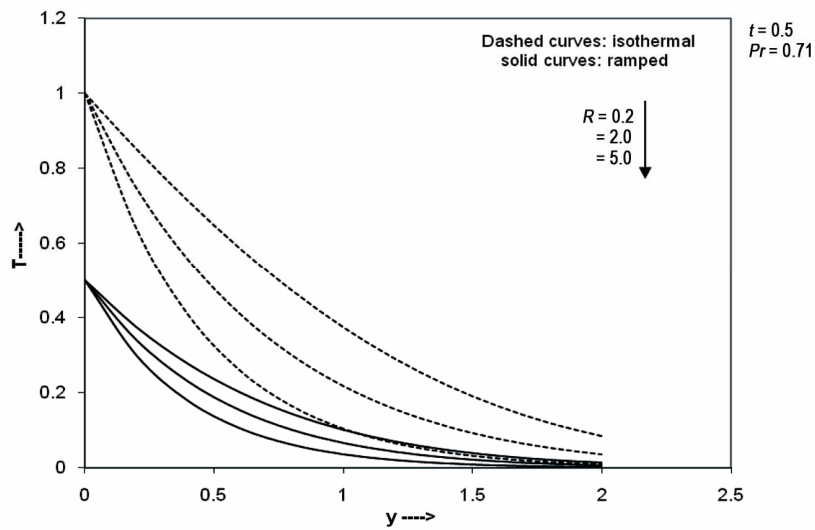


Figure 3. Temperature profile for different R .

ramped and constant plate temperature. We observe that the fluid temperature is greater in the case of isothermal plate than in the case of ramped temperature at the plate. This should be expected since in the latter case, the heating of the fluid takes place more gradually than in the isothermal case. Also, we observe that the temperature is maximum near the plate and decreases away from the plate and finally takes free stream value for all values of t , Pr and R .

In **Figures 4** and **5**, the velocity profiles are shown for different values of physical parameters involved. **Figure 4** reveals velocity variations with Pr and t at $R=3.0$. It demonstrates that the velocity decreases with increasing the Prandtl number. **Figure 5** illustrates the influence

of R on the velocity field for both ramped temperature and isothermal plate. It is observed that the fluid velocity decreases on increasing radiation parameter R in the boundary layer region. This implies that the radiation decelerates fluid velocity for both ramped temperature and isothermal plate. **Figures 4** and **5** also demonstrate that the velocity increases with an increase in time t . Again, from **Figures 4** and **5**, we observe that the velocity increases with y near the plate, becomes maximum and then decreases away from the plate and finally takes asymptotic value for all values of R . Lastly, it is seen that the velocity in case of ramped temperature plate is always less than the flow induced by a plate of constant temperature.

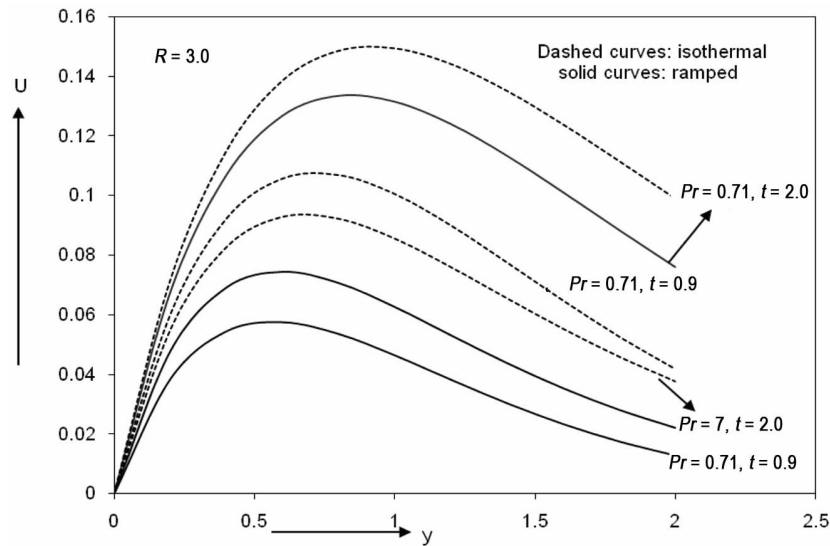


Figure 4. Velocity profile for different Pr and t .

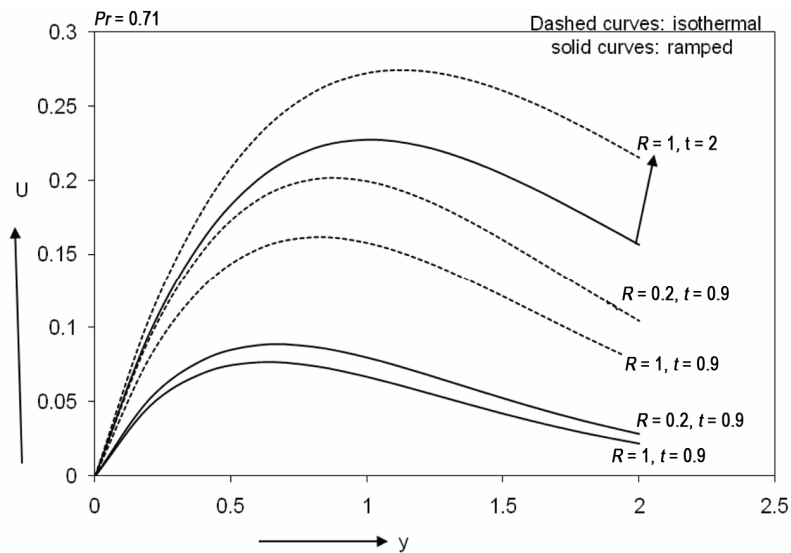


Figure 5. Velocity profile for different R and t .

Nu is calculated for different Pr , R and t and presented in **Figures 6** and **7**. It is clear from the figures that for the ramped plate temperature, the Nusselt number increases for a range $0 < t \leq 1$ and decreases for $t > 1$ for all Pr and R . But in case of constant wall temperature, the Nusselt number decreases with respect to t .

The numerical values of τ are evaluated for different values of $Pr = 0.71, 7.0$; $R = 2.0, 5.0$ and depicted in **Figure 8**. The effects of ramped and constant wall temperature on skin friction are also presented in this figure. We have seen that due to the presence of radiation, the skin-friction is greater in case of ramped temperature of

the plate than the case of an isothermal plate. It is also noticed that for small values of $t < 1$, there is a quick fall in the skin friction in the case of ramped temperature of the plate, whereas the skin friction decreases more gradually with time for the case of isothermal plate. Further, we observe that the skin friction co-efficient increases with R for both ramped temperature and isothermal plate, which illustrates that radiation has tendency to enhance the skin friction. It is also observed that the skin friction is enhanced with Pr . Lastly, we find that the ber.perayure skin-friction is more in water as compared to that in air.

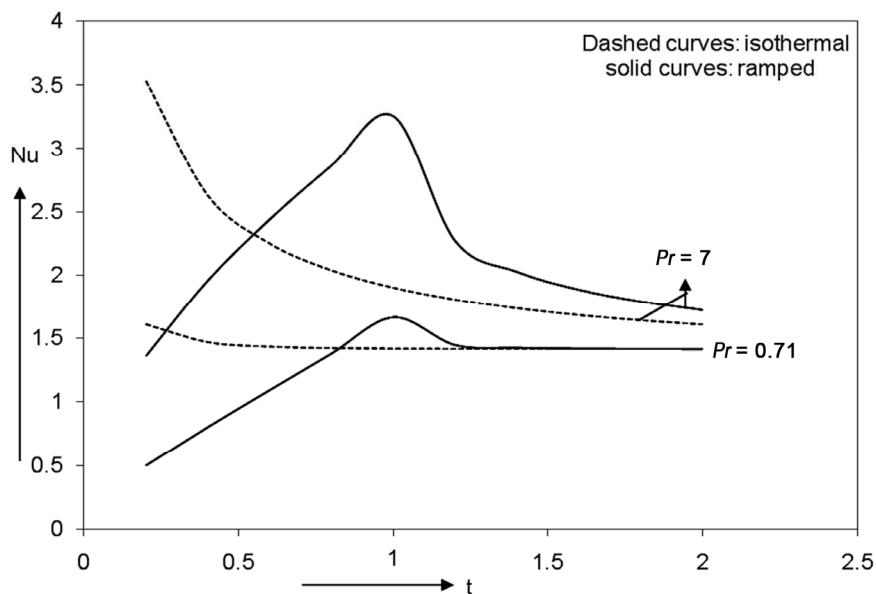


Figure 6. Variation of Nusselt number when $R = 2$.

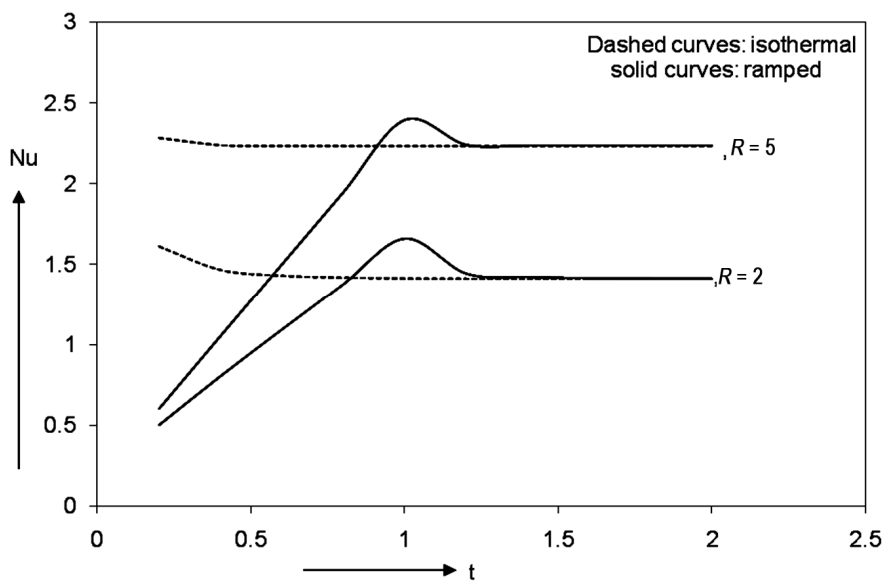


Figure 7. Variation of Nusselt number when $Pr = 0.71$.

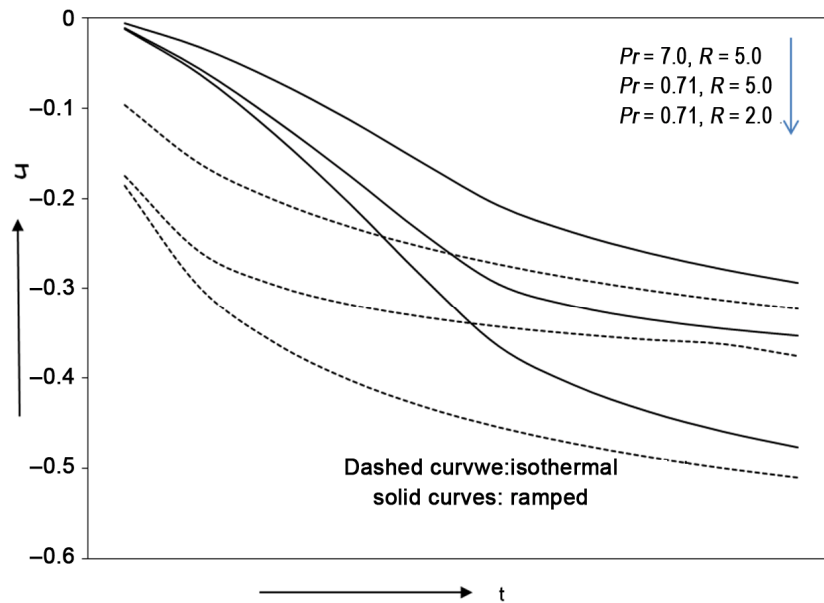


Figure 8. Variation of skin friction for ramped and isothermal temperature.

6. Conclusions

An analysis is performed to study the effect of radiation on unsteady free convection flow past an infinite vertical plate with ramped wall temperature. The non-dimensional forms of the governing equations of the fluid flow are solved by Laplace-transform technique. The solutions for velocity, temperature are studied graphically. Also, the Nusselt number and skin friction have been discussed.

Following observations are made from the study:

- 1) Temperature of the fluid increases with an increase in time t but as Pr increases, temperature decreases. Also, the temperature decreases gradually with R .
- 2) The temperature decreases with y from its ramped value on the plate to its free stream value.
- 3) The presence of radiation tends to decelerate the fluid flow for both ramped temperature and isothermal plate. Also, fluid velocity accelerates as time progresses.
- 4) The velocity decreases with increasing the Prandtl number.
- 5) Nusselt number increases for $0 < t \leq 1$ and decreases for $t > 1$ for all Pr and R .
- 6) Skin friction increases with increasing Pr and R .

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Nomenclature

a^*	Absorption coefficient	T'_∞	Temperature of fluid far away from the plate
C_p	Specific heat at constant pressure	t'	Time
g	Acceleration due to gravity	t	Dimensionless time
k	Thermal conductivity of the fluid	t_0	Characteristic time
Pr	Prandtl number	u'	Velocity of fluid in the x' -direction
q_r	Radiative heat flux in the y direction	u	Dimensionless velocity component in the x' -direction
R	Radiation parameter	x'	Spatial coordinate along the plate
T'	Temperature of fluid	y'	Coordinate normal to the plate
T'_w	Plate temperature	y	Dimensionless coordinate normal to the plate

Greek Symbols

β	Volumetric coefficient of thermal expansion	θ	Dimensionless temperature
μ	Coefficient of viscosity	$erfc$	Complementary error function
ν	Kinematic viscosity	erf	Error function
ρ	Density of fluid	$H(t-1)$	Is the unit step function