

## **Supplementary material: The EMEP MSC-W chemical transport model – technical description**

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## S1 EMEP model revision history

Table S1: Summary of major EMEP MSC-W Eulerian model versions

Revision	Date	Main changes
rv1.7	Jul 2003	First 'unified' model, with both acidification and photochemical scheme, documented in Simpson et al. (2003).
rv2.5	Jul 2006	Used for IIASA (GAINS) source-receptor matrices. Changes in: N <sub>2</sub> O <sub>5</sub> hydrolysis, EQSAM scheme for nitrate formation, PM-water added, ozone-flux outputs added, move to netcdf file format. Global modelling capability added.
rv3.0	Feb. 2008	<b>First public-domain release.</b> Included various small changes, e.g. to vegetation parameters, and numerous technical changes.
rv3.2		Improved deposition scheme, including co-deposition for SO <sub>2</sub> , revised particle deposition scheme, daily snow instead of climatological. Code revisions for more flexible grids and global scale.
rv3.4	2009	Additional chemical schemes implemented, EmChem09 scheme developed, forecast model versions implemented.
rv3.6	2010	Boundary layer physics updates, convection routine added.
rv3.8	May 2011	<b>Second public-domain release.</b> Major revisions in: Aerosol dry deposition methodology, also revised sub-cloud scavenging; Biogenic VOC emission methods, rates; added cumulus scheme; ECMWF IFS model replaces PARLAM/HIRLAM NWP as default meteorological driver;
rv3.9	Nov 2011	Major revisions: pH dependence of sulphate formation; added organic aerosol and SOA formation; use of daily FINNv1 forest fire module; changed temporal variations for sectors SNAP-1 (changing winter/summer ratios) and SNAP-2 (degree-days);
rv4 $\beta$	March 2012	Soil NO emissions, preliminary road-dust production added, use of soil moisture index from ECMWF IFS fields. As used in Aas et al. (2012).
rv4.0	Summer 2012	<b>Third public-domain release.</b> Hourly emission variations replaced former day/night emission factors, more flexible handling of volcanic emissions, increased MMD of coarse nitrate to 3 $\mu$ m, small change in vertical distribution of emissions.

Many changes are continuous, for example there is an ongoing process to make the model more flexible with respect to meteorological drivers, chemical schemes, grid-projection, nesting and boundary conditions. The vertical coordinate scheme has been revised, and where possible global databases are being implemented (for example forest fires) for use by all model domains.

## S2 Physical formulation and Numerics, additional information

The main paper has dealt with the physical and chemical formulation of the model. Here we address some of the numerical and computational details associated with the model structure.

### S2.1 Convection

Numerical implementation of the convection scheme is as described in Jonson et al. (2010). We define the mass (per square meter) of a pollutant in the layer  $k$  as  $\frac{\chi \Delta_k P}{g}$  where  $\chi$  is the mass mixing ratio of a pollutant,  $\Delta_k P$  is the pressure difference between the bottom and the top of the layer and  $g$  is the gravitational constant. The advantage of this formulation compared to using density times  $\Delta z$ , is that it is not dependent on a particular definition of the vertical coordinates.

We assume that the convective fluxes leaving the layer  $k$  through the top (cf. Fig. 3),  $F_k$ , are given by the meteorological driver. For **updrafts**, the process starts at surface (largest  $k$ ). If  $\Delta_k F = F_k - F_{k+1} > 0$ , the pollutants are transported from the environment towards the cloud core (elevator). The mass of the pollutant removed from a grid cell and put into the core in layer  $k$  during time  $\Delta t$ , is given by  $\chi_{grid} \Delta_k F \Delta t$ , and the new mixing ratio becomes:

$$\chi_{grid}^{t+\Delta t} = \chi_{grid}^t - \chi_{grid}^t \frac{g \Delta_k F \Delta t}{\Delta_k P} \quad (1)$$

In this formulation  $\Delta_k P$  is kept constant during the convection process. The mixing ratio of the pollutant in the cloud core becomes:

$$\chi_{core}^{t+\Delta t} = \chi_{core}^t + \chi_{grid}^t \frac{g \Delta_k F \Delta t}{\Delta_k P} \quad (2)$$

If mass is transported from the cloud core towards the grid cell, the proportion of pollutants removed from the core is given by  $\frac{F_{k+1} - F_k}{F_{k+1}}$  and the new mixing ratios become

$$\chi_{grid}^{t+\Delta t} = \chi_{grid}^t + \chi_{core}^t \frac{F_{k+1} - F_k}{F_{k+1}} \quad (3)$$

$$\chi_{core}^{t+\Delta t} = \chi_{core}^t - \chi_{core}^t \frac{F_{k+1} - F_k}{F_{k+1}} \quad (4)$$

The pollutant in the core is then lifted to the next level:

$$\chi_{core(k-1)}^t = \chi_{core(k)}^{t+\Delta t} \frac{\Delta_{k+1} P}{\Delta_k P} \quad (5)$$

and the process is iterated until the top is reached.

A corresponding calculation for the downward fluxes is performed, starting from top and continuing down to the surface. After these detrainment and entrainment processes, the total mass of pollutants will be conserved, however there will be an imbalance between the quantity of air having entered and left the individual grid cells, because the large scale subsidence has

not yet been accounted for. In order to mimic the subsidence process, we perform the same procedure starting with  $\chi = 1$  at all levels, which will account for the modelled transport of “pure air”.

The mass in a specific level obtained,  $\frac{\chi \Delta_k P}{g}$  will then give a measure of the excess or deficiency of air. The air masses are then redistributed along the vertical column. The levels are filled successively starting from above until the original masses are recovered. The pollutants follow the same pattern.

## S2.2 Time-step control

The numerical solution of the advection requires that the so-called Courant number does not exceed 1. The Courant (or CFL) number  $CU_0$  is defined as  $\frac{\Delta t}{\Delta x} |u|$  where  $u$  is wind-speed. This ensures that material from one grid cell can not be advected beyond the borders of its downwind neighbour. For a variable horizontal grid size, this expression must be scaled by the map factor. If the Courant number is exceeded, the advection timestep is adjusted for different rows or columns where needed. The time step for the vertical advection can also be different from the time step in the horizontal directions, but all elementary time steps for the one dimensional advection have to be an integer fraction of  $\Delta t_{advect}$ . A too low Courant number will lead to an undesired increase in numerical diffusion and also an increase in CPU requirements.

For each row  $j$  and vertical level  $k$ , a maximum value for the time-step  $\Delta t$  in direction  $x$  is derived; the following expression is evaluated over all grid cells in the row:

$$\Delta t_{max}(j, k) \leq \frac{\Delta x}{\max(m^2 \frac{u(i,j,k)}{m_y(i,j)}, 0) - \min(m^2 \frac{u(i-1,j,k)}{m_y(i-1,j)}, 0)}$$

Where  $m^2 = m_x(i, j) m_y(i, j)$ , and  $m_x$ ,  $m_y$  are map-factors (see also Sect. 2.2). Corresponding expressions for the  $y$  and vertical directions are used.

The time step is set to the same value for all cells in one single row in each horizontal direction, although they can be different for different rows and at different heights. See Wind et al. (2002) for further details of the time-step control system.

## S2.3 Chemistry - numerical solution

As noted in Sect. 7.10, the chemical equations are solved using the TWOSTEP algorithm tested by Verwer et al. (1996) & Verwer and Simpson (1995). The formulae have however been rearranged for greater computational efficiency (S. Unger. Pers. comm.), and so here we outline the algorithm as used in the model. Note that the notation here is different to that used by Verwer and Simpson (1995).

The algorithm used for the chemistry solutions are summarised below. From the main model, at the start (time  $t$ ) of each advection time-step of length  $\Delta t_{\text{advec}}$  (typically 20 mins), we have 3-d arrays ( $C_m^{3D}(i, j, k)$ ) of the chemical concentrations (in molecules  $\text{cm}^{-3}$ ) of each species  $m$ , and of the chemical tendency,  $D_m$  (see below). Within one  $\Delta t_{\text{advec}}$  we use a number  $N_{\text{chem}}$  of chemical time-steps, of (uneven) width  $\Delta t(n)$ , where  $n = 1 \dots N_{\text{chem}}$  (see below). We will use the notation  $t(n) = t + \Delta t(1) + \dots + \Delta t(n)$ . The scheme uses two values of concentrations,  $C_m^{t(n-2)}$  and  $C_m^{t(n-1)}$ , to derive the next value  $C_m^{t(n)}$ .

### 1. Initialise time-step

$$C_m^{t(0)} = C_m^{3D}(i, j, k) \quad \text{start with concentrations from 3-D fields at time } t$$

$$C_m^{t(-1)} = C_m^{t(0)} - 1.5 D_m(i, j, k) \tau(1) \quad \text{Estimate based upon chemical tendency only.}$$

( $D_m$  and  $\tau$  defined below,  $D_m=0$  when program starts).

### 2. Integration loop

For each chemical time-step (for  $n = 1 \dots N_{\text{chem}}$ ) we then do:

$$C_m^* = \alpha(n)C_m^{t(n-1)} - \beta(n)C_m^{t(n-2)} \quad \text{help variable}$$

$$C_m^{t(n)} = C_m^{t(n-1)} + (C_m^{t(n-1)} - C_m^{t(n-2)})\gamma(n) \quad \text{First guess of new concs}$$

For the general time-step  $n$ , coefficients  $\alpha, \beta, \gamma, \tau$  are calculated with:

$$\theta(n) = \Delta t(n-1)/\Delta t(n) \quad (\text{for } n=1, \text{ we use } \theta(1)=1)$$

$$\beta(n) = 1/(\theta(n)^2 + 2\theta(n))$$

$$\alpha(n) = (\theta(n) + 1)^2\beta(n)$$

$$\tau(n) = (\theta(n) + 1)/(\theta(n) + 2) \Delta t(n)$$

$$\gamma(n) = 1/\theta(n)$$

#### 2a. Calculation of $C_m^{t(n)}$

Following Verwer and Simpson (1995), a Gauss-Seidel integration procedure is then used, where for each species  $m$ , the production rate  $P_m$ , loss-rate  $L_m$ , and then the updated concentrations  $C_m^{t(n)}$  are calculated in turn. The updated concentration for the iteration is then obtained using a Padé approximation of the second order backward difference formula:

$$C_m^{t(n)} = \frac{C_m^* + \tau(n)P_m}{1 + \tau(n)L_m} \quad (6)$$

At each stage the the latest values of concentrations are used for all reactants. Step 2a, running through all species and using Eqn. 6 is iterated a number of times (from 1 to 3, see below). We then save the chemical tendencies and return the new concentrations of advected species to the 3-D fields:

$$\begin{aligned} D_m &= (C_m^{t(n)} - C_m^{3D}(i, j, k))/\Delta t_{\text{advec}} \\ C_m^{3D}(i, j, k) &= C_m^{t(n)} \end{aligned}$$

At present, with an advection time-step  $\Delta t_{\text{advec}}$  of 20 minutes (1200 s) the algorithm starts with five successive timesteps of  $\Delta t_{\text{chem}} = 20$  s followed by seven larger timesteps of just under 160 s. Compared with a fixed timestep, increasing timesteps has been found more efficient, since at the start of the process the system is further away from a steady-state situation. This scheme improves with iteration. In the 4 layers near the ground, where emission and usually reaction tendencies are highest, we perform 3 iterations each timestep. Above this, 2 iterations are performed, except for the uppermost 6 layers where 1 iteration is used.

## S2.4 Parallel structure and CPU requirements

In order to produce results covering several years and several different situations, the model requires large computer resources. The program code is written in Fortran 90/95. The structure of the program is designed to allow for efficient parallelization on a system with distributed memory.

The horizontal grid is divided into a number of subdomains and each subdomain is assigned to a processor. Each processor holds only the data for its own subdomain. Because of this structure, the communication between the processors is kept to a minimum.

Still the advection routines fundamentally require information to be passed between processors. An additional limitation of the level of parallelity which can be achieved is that much input/output is currently done on one processor, and thus requires information to be passed between the processors. The meteorological data for example is stored on disc and has to be read serially and distributed to all the nodes. Also the writing of results cannot yet be done entirely in parallel. Further details on the parallel architecture of the code can be found in Skålin et al. (1995).

The most CPU demanding part of the program is the chemistry module, because of the large number of chemical components and reactions. The chemical reactions have to be described for all the grid-cells and with a small time scales. However the chemistry is local and is therefore perfectly suited for parallelization. The deposition and wet scavenging processes have only vertical data dependencies and will therefore also parallelize effectively with the partitioning adopted in the program.

A typical run covering one year in a 159x133 grid will require less than four real time hours (128 CPU hours) on 32 processors. The typical relative CPU usage of the different part of the

program are: Chemistry 60% , Advection 10%, Meteorology and input/output 10%, Synchronisation between nodes 10%, others 10%. For larger grids more processors are used; the model has been tested for up to 1024 CPUs and scales well.

## S3 Derivation of 'missing' meteorological parameters

As noted in Sect. 3 the EMEP model has to have systems for deriving parameters when missing, or can do without some meteorological fields. Two important cases are for 3-D precipitation and vertical wind-speed.

### S3.1 3-D precipitation fields

When precipitation data are not available as a three dimensional fields, they are derived from surface precipitation. The height of the precipitation release is derived either from cloud water, if available, or humidity if cloud water is not available. The height of the precipitation is then defined as the highest altitude above the lowest level, where the cloud water is larger than a threshold taken as  $1.0 \times 10^{-7}$  kg water per kg air ( or when the relative humidity is larger than 0.85 in case cloud water is not available). Precipitations are only defined in areas where surface precipitations occur. The intensity of the precipitation is assumed constant over all heights were they are non-zero.

### S3.2 Vertical wind speed

When the vertical wind speed  $\dot{\sigma}$  is not available, it is derived from the continuity equation (see also Travnikov et al. (2009)) using

$$(\dot{\sigma})_{k+\frac{1}{2}} (P_S - P_{top}) = \sigma_{k+\frac{1}{2}} \sum_{r=Surf}^{top} \vec{\nabla} (\vec{V}_r \Delta P_r) - \sum_{r=k}^{top} \vec{\nabla} (\vec{V}_r \Delta P_r) \quad (7)$$

Use of this formula directly ensures that  $(\dot{\sigma})_S = 0$  at surface since  $\sigma_S = 1$ , and  $(\dot{\sigma})_{top} = 0$  at top since  $\sigma_{top} = 0$ .

## S4 Emissions

### S4.1 Annual totals

Table S2: Emissions ( $\text{Gg a}^{-1}$ ) for the year 2008 used in the EMEP model.

	Anthropogenic						Biogenic <sup>‡</sup>		
	SOx (as SO <sub>2</sub> )	NOx (as NO <sub>2</sub> )	NMVOC	NH <sub>3</sub>	PMf	PMc	soil-NO (as NO <sub>2</sub> )	Isop.	MT
Albania	37	29	32	24	14	4.0	3.2	9.2	32
Armenia	26	24	41	17	0.3	0.5	–	–	0.1
Austria	22	204	150	63	21	16	2.5	12	35
Azerbaijan	91	91	238	53	3.8	0.6	–	–	0.4
Belarus	84	189	387	147	53	13	4.5	34	61
Belgium	97	239	118	67	20	8.1	–	5.0	4.0
Bosnia	431	51	43	17	19	24	1.8	13	18
Bulgaria	569	141	84	62	31	28	9.0	41	94
Croatia	58	85	109	38	11	4.7	1.1	17	20
Cyprus	23	20	12	5.3	2.8	1.5	–	–	0.5
Czech	174	261	166	58	21	14	1.3	14	22
Denmark	19	150	96	78	28	6.2	–	4.4	5.7
Estonia	69	36	38	11	20	5.4	–	2.8	3.3
Finland	70	168	118	38	38	14	1.4	35	41
France	344	1194	957	672	267	118	2.9	49	68
Georgia	22	46	231	26	1.9	0.3	–	–	0.3
Germany	490	1418	1017	568	110	85	4.3	56	99
Greece	444	394	228	65	63	37	9.7	25	112
Hungary	88	183	141	69	23	15	2.4	22	31
Iceland	74	24	5.7	3.0	0.5	0.1	–	1.0	4.0
Ireland	46	110	51	107	9.5	5.2	–	–	0.2
Italy	283	1057	1194	409	173	31	11	65	149
Kazakstan	381	171	155	573	25	14	11	61	149
Kyrgyzstan	26	63	25	27	11	9.3	–	–	0.1
Latvia	4.7	34	74	16	26	6.3	0.4	9.9	12
Lithuania	27	55	66	29	9.5	2.6	0.5	7.5	13
Luxembourg	2.3	50	10	4.7	2.2	0.9	–	1.3	0.9
FYR Macedonia	114	37	28	7.0	8.8	9.5	1.7	4.2	18
Malta	11	9.0	3.0	1.5	1.4	0.8	–	0.5	1.2
Moldova	7.5	32	35	26	6.2	3.8	2.6	10	26
Montenegro	15	9.5	10	3.2	5.5	4.2	0.8	2.7	8.4
Netherlands	51	309	162	127	17	14	–	0.3	1.0
Norway	20	189	154	23	46	6.3	0.2	28	35
Poland	995	832	641	285	122	125	4.8	31	72
Portugal	108	211	192	47	59	26	–	9.4	9.7
Romania	566	287	465	187	123	21	15	73	182
Russia	1575	3789	2566	599	384	216	71	457	978
Serbia	265	194	133	89	25	16	6.7	30	61
Slovakia	69	94	67	25	28	3.7	1.2	3.0	20
Slovenia	13	53	33	18	13	3.1	–	0.6	1.4
Spain	513	1061	730	354	82	35	1.7	44	65
Sweden	30	158	196	52	28	12	0.3	27	33
Switzerland	14	83	93	65	10.0	11	0.5	6.0	6.4
Turkey	1041	860	1000	409	247	93	0.6	5.2	25
UK	491	1317	922	283	73	52	–	11	13
Ukraine	1386	825	311	206	276	185	37	212	419

Notes: Data from anthropogenic sources were updated in 2012 (see [www.ceip.at/webdab-emission-database](http://www.ceip.at/webdab-emission-database)); '–' indicates values less than 0.1  $\text{Gg a}^{-1}$ .

‡ Emissions from biogenic sources are estimated from gridded data using country area fractions only. Values for small countries are very approximate;



## S4.2 Spatial distribution

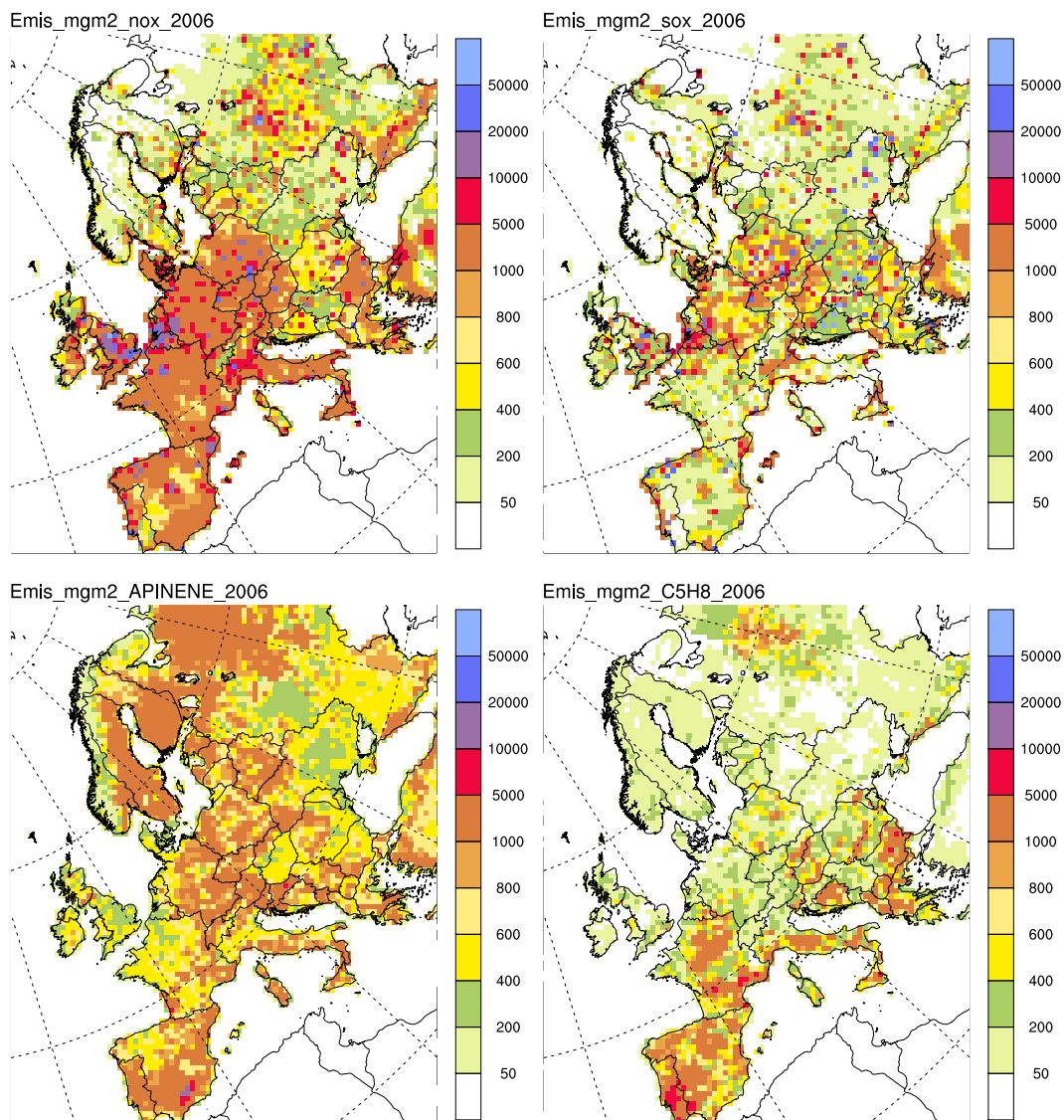


Figure S1: Emissions of  $\text{NO}_x$ ,  $\text{SO}_2$ , monoterpenes (surrogate APINENE) and isoprene in the EMEP grid for the year 2006. Units:  $\text{mg m}^{-2}$ .

### S4.3 Anthropogenic emissions, additional Tables

Table S3: Vertical distribution of anthropogenic emissions: percentage of each SNAP emission sector allocated to the vertical layers of the EMEP model (given as heights of layers, in m, for a standard atmosphere).

No.	Sources	Height of Emission Layer (m)					
		0-92	92-184	184-324	324-522	522-781	781-1106
1	Combustion in energy and transformation industries			15	40	30	15
2	Non-industrial combustion plants	100 <sup>(a)</sup>	0 <sup>(a)</sup>				
3	Combustion in manufacturing industry	10	10	15	30	30	5
4	Production processes	90	10				
5	Extraction and distribution of fossil fuels and geothermal energy	90	10				
6	Solvents and other product use	100					
7	Road transport	100					
8	Other mobile sources and machinery	100					
9	Waste treatment and disposal	10	15	40	35		
10	Agriculture	100					

Notes: (a) Up to version rv4 $\beta$  SNAP-2 was split 90% into the lowest layer, then 10% in the next lowest.

Table S4: Day<sup>(a)</sup> and night factors applied to anthropogenic emissions in code versions up to rv4 $\beta$ . In the latest (rv4) model version, hourly emission factors are applied, depending on day-of-week and SNAP sector. (These new factors were provided by INERIS, B. Bessagnet, pers.comm.)

SNAP:	1	2	3	4	5	6	7	8 <sup>(b)</sup>	9	10
Day	1.0	1.2	1.2	1.5	1.0	1.5	1.5	1.2	1.0	1.4
Night	1.0	0.8	0.8	1.0	1.0	0.5	0.5	0.8	1.0	0.6

Notes: (a) Defined as between 7am and 6pm local time; (b) SNAP8 covers a range of non-road traffic sources, including shipping. Emissions from international shipping assumed constant over 24 h.

Table S5: Default speciation of VOC emissions: Percentage (by mass) of each emissions (SNAP) sector allocated to model species. Data derived from Passant (2002), see also Hayman et al. (2012).

SNAP	C2H6	NC4H10	C2H4	C3H6	C5H8	OXYL	CH3OH	C2H5OH	HCHO	CH3CHO	MEK	GLYOX	MGLYOX	UNREAC
1	12.559	14.836	2.406	4.376	0.000	9.479	0.000	0.000	55.691	0.034	0.620	0.000	0.000	0.000
2	12.589	39.790	8.174	10.767	0.000	18.632	0.000	3.912	5.586	0.207	0.089	0.000	0.000	0.255
3	4.996	35.610	9.044	2.089	0.000	18.323	0.561	3.034	24.134	0.059	1.347	0.000	0.000	0.805
4	2.652	34.519	5.458	4.257	0.142	13.380	1.176	31.414	0.077	0.978	1.608	0.000	0.000	4.337
5	17.842	79.895	0.018	1.569	0.008	0.505	0.000	0.000	0.078	0.000	0.000	0.000	0.000	0.085
6	0.444	44.052	0.244	0.678	0.008	17.904	6.101	16.416	0.011	0.000	9.965	0.000	0.000	4.176
7	4.832	36.698	6.796	10.896	0.000	35.051	0.000	0.000	2.700	2.606	0.421	0.000	0.000	0.000
8	3.775	47.416	6.636	10.608	0.000	24.676	0.000	0.000	3.115	3.261	0.235	0.146	0.117	0.014
9	25.718	36.778	5.237	1.830	1.153	7.881	0.427	2.439	16.060	0.000	0.093	0.000	0.000	2.383
10	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	100.000

Notes: For definition of model species (e.g. MEK, OXYL) see Table S5, Table S5, except for non-reacting species here (UNREAC) which are excluded from the calculations.

Table S6: Default speciation of coarse (2.5–10 $\mu$ m) PM emissions: Percentage (by mass) of each emission (SNAP) sector allocated to organic matter (OM), elemental carbon (EC) and remaining coarse primary particulate matter (REMPPM\_c).

SNAP	OM	EC <sup>(a)</sup>	REMPPM_c
1	1	5	94
2	50	20	30
3	5	10	85
4	5	5	90
5	5	5	90
6	10	40	50
7	40	30	30
8	45	45	10
9	40	30	30
10	40	20	40
11	70	0	30

(a) EC further split into 80% ECnew.f, 20% ECage.f. If explicit wood-burning emissions available, a 50:50 split is assumed between ECnew.f, ECage.f.

## S4.4 Foliar emissions, additional Tables

Table S7: Forest-specific biomass density and emission factors (leaf-level).

EMEP Code ( $\Lambda$ )	Species ( $\lambda$ )	Common name	Biomass density ( $D$ ) $\text{gm}^{-2}$	Emission factors ( $\mu\text{g g}^{-1}\text{h}^{-1}$ )		
				Isoprene $\varepsilon_{\Lambda_{c,iso}}$	Monoterpenes $\varepsilon_{\Lambda_{c,mtl}}$	$\varepsilon_{\Lambda_{c,mtp}}$
CF	Abies alba	Silver Fir	1200	0	0	1
CF	Abies bori.	Bulgarian Fir	1200	10	0	3
CF	Abies	other Fir	1200	0	0	3
DF	Acer		320	0	2	0
DF	Alnus glutinosa	Common Alder	320	0.2	3	0
DF	Alnus	other Alder	320	0	1.5	0
BF	Arbutus		300	0.1	0.1	0
DF	Betula	Birch	320	0	0	3
NF	Buxus Semi.	Common box	320	10	0	0.2
DF	Carpinus bet.	European Hornbeam	320	0	0	0.7
DF	Carpinus	other Hornbeam	320	0	1	0.5
DF	Castanea	Chestnut - all	320	0	10	0
NF	Cedrus	Cedar	700	0	0	0.7
DF	Cercis sil.	Judas tree	320	0	0	0
NF	Ceratonia silq	Carob tree	320	0	0	0
DF	Corylus avel.	Hazel tree	320	0	0	0
NF	Cupressus	Cypress	700	0.1	0	0.7
NF	Erica arbor.	Tree Heath	100	10	0	3
NF	Erica	other Erica	150	0	0	0
NF	Eucalyptus	Eucalyptus	400	35	0	3
DF	Fagus	Beech	320	0	10	0

Cont. on next page

Notes: See Sect. 6.6 for explanation of rates and algorithms.

Table S7: cont.

$\Lambda$	$\lambda$		$D$	$\varepsilon_{\Lambda_c, iso}$	$\varepsilon_{\Lambda_c, mtl}$	$\varepsilon_{\Lambda_c, mtp}$
DF	Fraxinus	Ash (all)	320	0	0	0
NF	Ilex aquifolium	Holly	320	0	0	0
BF	Juglans	Walnut	320	0	0	1
NF	Juniperus	Juniper	700	0	0	1
DF	Larix kaempferi		300	0	0	8
DF	Larix	Larch (other)	300	0	0	5
NF	Laurus nobilis	Laurel	500	0	0	0
DF	malus domestica	Apple	320	0	0	0
NF	Olea	Olive	200	0	0.2	0
DF	Ostrya Carpinifolia	Hop Hornbeam	320	0	0	0
NF	Phillyrea latifolia	Green Olive	300	0	0.4	0.1
CF	Picea abies	Norway spruce	1400	1	0.5	1
CF	Picea sitchensis	Sitka spruce	1400	5	0	3
CF	Picea	Other spruce	1400	1	0.5	1
NF	Pinus pinaster	Maritime pine	700	0	0	1.5
NF	Pinus pinea	Stone pine	700	0	4	2
CF	Pinus sylvestris	Scots pine	700	0.1	1	2
CF	Pinus uncinata	Mountain pine	700	0.1	0	3
NF	Pinus radiata	Monterey pine	700	0	1	1
CF	Pinus - other	Other pine	700	0	0	3
BF	Pistacia lentiscus		320	0	0	0.7
BF	Pistacia terebinthus		320	0	0.5	0
DF	Platanus orientalis	Oriental plane	320	50	0	3
DF	Populus alba		320	60	1	0
DF	Populus tremula		320	45	3	0
DF	Populus	Other Poplar	320	45	1	0
DF	Prunus		300	0	0.2	0
CF	Pseudotsuga menziesii	Douglas Fir	1000	1	0	3

Cont. on next page

Table S7: cont.

$\Lambda$	$\lambda$		$D$	$\varepsilon_{\Lambda_c, iso}$	$\varepsilon_{\Lambda_c, mtl}$	$\varepsilon_{\Lambda_c, mtp}$
DF	Pyrus comm.	European pear	320	0	0	0
DF	Quercus cerr.	Turkey oak	320	0.1	1	0.5
BF	Quercus cocc.	Kermes oak	320	0.1	10	0
DF	Quercus fagi.	Portugese oak	320	100	0.5	0
DF	Quercus frai.	Hungarian (Italian) oak	320	100	0	0
BF	Quercus fruc.		320	0.1	20	0
BF	Quercus ilex.	Holm (Holly) Oak	500	0.1	30	0
DF	Quercus macr.	Caucasian (Persian)	320	0.2	0	0.5
DF	Quercus petr.	Sessile oak	320	45	0.5	0
DF	Quercus pube.	Downy oak	320	80	0.2	0
DF	Quercus pyre.	Pyrenean oak	320	60	0.5	0
DF	Quercus robu.	Pendunculate (En- glish) oak	320	80	0.2	0.2
BF	Quercus rotu.		320	0.2	15	0
DF	Quercus rubra	N. Red Oak	320	60	1	0
BF	Quercus sube.	Cork oak	500	0.2	20	0
BF	Quercus troj.	Macedonian oak	320	0.2	0.2	0
DF	Robinia pseu.	Locust	320	20	3	0
DF	Salix	Willow	150	20	0	1
DF	Sorbus	Whitebeam	320	0	0	0
DF	Taxus baccata	Yew	320	0	0	0
CF	Thuja sp.		320	0	0	0.5
DF	Tila sp.	Lime/Linden	320	0	0	0
CF	Tsuga sp.	Hemlock	320	0.1	0	1.5
DF	Ulmus sp.	Elm	320	0.1	0	0.1
DF	Other broadleaf		320	5	0	0.2
CF	Other coniferous		500	1	1	2

## S4.5 Sea-salt, equations

The parameterisation scheme for calculating sea salt generation has been presented and discussed in Tsyro et al. (2011), so here we present just the basic equations for the two source functions. The first one is a source function constructed by Monahan et al. (1986):

$$\frac{dF}{dr_{80}} = 1.373 V_{10}^{3.41} r_{80}^{-3} \left(1 + 0.057 r_{80}^{1.05}\right) \times 10^{1.19 \exp(-B^2)} \quad (8)$$

where  $dF/dr_{80}$  is the rate of sea salt droplet generation per unit area of sea surface and per increment of the aerosol radius  $r_{80}$  at 80 % relative humidity (see below),  $V_{10}$  is the wind speed at 10 m, and  $B = (0.380 - \log(r_{80}))/0.650$ .

The second scheme is a source function from the work of Mårtensson et al. (2003), which is formulated for sea water salinity of 33 ‰:

$$\frac{dF}{d \log D_d} = 3.84 \cdot 10^{-6} (A_k T_w + B_k) \cdot V_{10}^{3.41} \quad (9)$$

where  $dF/d(\log D_d)$  is the flux of sea salt particle per unit area of the whitecap cover and per increment of  $(\log D_d)$ ,  $D_d$  is the dry diameter,  $T_w$  is the temperature of sea water, equal to Sea Surface Temperature (SST), or to  $T_2$  if SST is unavailable from the NWP model, and  $A_k$  and  $B_k$  are the parameters describing the dependence of sea salt flux on the aerosol size:

$$\begin{aligned} A_k &= c_4 D_d^4 + c_3 D_d^3 + c_2 D_d^2 + c_1 D_d + c_0 \\ B_k &= d_4 D_d^4 + d_3 D_d^3 + d_2 D_d^2 + d_1 D_d + d_0 \end{aligned} \quad (10)$$

and the empirical coefficient  $c_i$  and  $d_i$  are tabulated according to Mårtensson et al. (2003).

The relationship between the dry radius  $r_d$  and radius at the supersaturation  $S=0.8$  (for relative humidity of 80 %) for sea salt aerosols is expressed through an empirical formula, as suggested in Gong et al. (1997):

$$r_{80} = \left( \frac{0.7674 r_d^{3.079}}{2.573 \cdot 10^{-11} r_d^{-1.424} - \log_{10} S} + r_d^3 \right)^{1/3} \quad (11)$$

First, sea aerosol fluxes are calculated for ten size bins, using Mårtensson et al. (2003) parameterisation for the first six bins (up to dry diameter of  $1.25 \mu\text{m}$ ) and Monahan et al. (1986) scheme for the larger sizes. The generated sea salt aerosols are aggregated in two size fractions, i.e. the fine fraction with (Mass Median Diameter  $\text{MMD} = 0.33 \mu\text{m}$ ) and the coarse fraction ( $\text{MMD} = 4.0 \mu\text{m}$ ). The total production rates of the fine and coarse sea salt are found by integrating the size resolved fluxes over respective size intervals. Finally, the generated sea salt aerosols are assumed to be instantaneously mixed within the model lowest layer (approximately 90 m height) at each time step.

## S5 Default chemical mechanism, EmChem09

We give below the gas and inorganic particle phase chemical mechanism. (For comments on secondary organic aerosol, see Sect. 7.9.)

Table S8: Listing of non-advected (short-lived) species used in default EmChem09 chemical scheme.

Model species	Formula
OD	O
OP	O
OH	OH
HO2	HO <sub>2</sub>
CH3O2	CH <sub>3</sub> O <sub>2</sub>
C2H5O2	C <sub>2</sub> H <sub>5</sub> O <sub>2</sub>
SECC4H9O2	sec-C <sub>4</sub> H <sub>9</sub> O <sub>2</sub>
ISRO2	HOC <sub>5</sub> H <sub>8</sub> O <sub>2</sub>
ETRO2	CH <sub>2</sub> O <sub>2</sub> CH <sub>2</sub> OH
PRRO2	CH <sub>3</sub> CHO <sub>2</sub> CH <sub>2</sub> OH
OXYO2	C <sub>8</sub> H <sub>11</sub> O <sub>3</sub> O <sub>2</sub>
MEKO2	CH <sub>3</sub> COCHO <sub>2</sub> CH <sub>3</sub>
MALO2	CH <sub>3</sub> COCH(OH)CH(O <sub>2</sub> )CHO
MVKO2	HOCH <sub>2</sub> CH(OO)C(CH <sub>3</sub> )=O
MACRO2	O=CHC(O <sub>2</sub> )(CH <sub>3</sub> )CH <sub>2</sub> OH
MACO3	CH <sub>2</sub> C(CH <sub>3</sub> )C(=O)O <sub>2</sub>



Table S9: Listing of advected core species used in default EmChem09 chemical scheme.

Model species	Formula	DRY <sup>†</sup>	WET <sup>†</sup>
O3	O <sub>3</sub>	O3	
NO	NO		
NO2	NO <sub>2</sub>	NO2	
PAN	CH <sub>3</sub> COO <sub>2</sub> NO <sub>2</sub>	PAN	
MPAN	CH <sub>2</sub> CH(CH <sub>3</sub> )COO <sub>2</sub> NO <sub>2</sub>	PAN	
NO3	NO <sub>3</sub>		
N2O5	N <sub>2</sub> O <sub>5</sub>		
ISONO3	NO <sub>3</sub> C <sub>5</sub> H <sub>8</sub> O		
HNO3	HNO <sub>3</sub>	HNO3	HNO3
HONO	HONO	HNO2	HNO3
H2	H <sub>2</sub>		
CO	CO		
CH4	CH <sub>4</sub>		
SO2	SO <sub>2</sub>	SO2	SO2
SO4	SO <sub>4</sub> <sup>2-</sup>	PMfS	SO4
NH3	NH <sub>3</sub>	NH3	NH3
NO3_f	NO <sub>3</sub> <sup>-</sup>	PMfN	PMf
NO3_c	NO <sub>3</sub> <sup>-</sup>	PMc	PMc
NH4_f	NH <sub>4</sub> <sup>+</sup>	PMfN	PMf
CH3COO2	CH <sub>3</sub> COO <sub>2</sub>		
MACR	CH <sub>2</sub> =CCH <sub>3</sub> CHO		
ISNI	generic		
ISNIR	generic		
GLYOX	HCOHCO		
MGLYOX	CH <sub>3</sub> COCHO		
MAL	CH <sub>3</sub> COCH=CHCHO	ALD	
MEK	CH <sub>3</sub> COC <sub>2</sub> H <sub>5</sub>		
MVK	CH <sub>3</sub> C(=O)CH=CH <sub>2</sub>		
HCHO	HCHO	HCHO	HCHO

Table gives: Model species – name as used in code, Formula – chemical formula when needed by GenChem (sometimes omitted), DRY – species from which dry-deposition rates calculated, WET – species from which wet-deposition rates calculated. Suffix \_f, \_c refer to fine and coarse mode aerosol species.

† Notation for gaseous compounds relates to *Wesely, 1989*, although methodology differs. PMf, PMc indicate particle deposition rates for fine and coarse aerosols, for sulphate-like (PMfS) or fine-nitrate-like (PMfN) compounds.

The Table omits the species involved in the SOA mechanism, since these vary very much with mechanism, and also do not affect the core chemistry.

Table S9: cont.

Model species	Formula	DRY	WET
CH3CHO	CH <sub>3</sub> CHO	ALD	
C2H6	C <sub>2</sub> H <sub>6</sub>		
NC4H10	nC <sub>4</sub> H <sub>10</sub>		
C2H4	C <sub>2</sub> H <sub>4</sub>		
C3H6	C <sub>3</sub> H <sub>6</sub>		
OXYL	o-C <sub>6</sub> H <sub>4</sub> (CH <sub>3</sub> )CH <sub>3</sub>		
C5H8	CH <sub>2</sub> =HCC=CH <sub>2</sub> CH <sub>3</sub>		
CH3O2H	CH <sub>3</sub> O <sub>2</sub> H	ROOH	
C2H5OOH	C <sub>2</sub> H <sub>5</sub> OOH	ROOH	
BURO2H	secC <sub>4</sub> H <sub>9</sub> O <sub>2</sub> H		
ETRO2H	CH <sub>2</sub> O <sub>2</sub> HCH <sub>2</sub> OH		
PRRO2H	CH <sub>3</sub> CHO <sub>2</sub> HCH <sub>2</sub> OH		
OXYO2H	C <sub>8</sub> H <sub>11</sub> O <sub>3</sub> O <sub>2</sub> H		
MEKO2H	CH <sub>3</sub> COCHO <sub>2</sub> HCH <sub>3</sub>		
MALO2H	CH <sub>3</sub> COCHOHCHO <sub>2</sub> CHO		
MVKO2H	HOCH <sub>2</sub> CH(O <sub>2</sub> H)C(CH <sub>3</sub> )=O		
MACROOH	O=CHC(CH <sub>3</sub> )(OOH)CH <sub>2</sub> OH		
MACO3H	CH <sub>2</sub> =C(CH <sub>3</sub> )C(=O)OOH		
MACO2H	CH <sub>2</sub> =C(CH <sub>3</sub> )C(=O)OH		
ISRO2H	HOC <sub>5</sub> H <sub>8</sub> O <sub>2</sub> H		
H2O2	H <sub>2</sub> O <sub>2</sub>	SO2	H2O2
CH3COO2H	CH <sub>3</sub> COO <sub>2</sub> H		
ISONO3H	NO <sub>3</sub> C <sub>5</sub> H <sub>8</sub> O <sub>2</sub> H		
ISNIRH	generic		
CH3OH	CH <sub>3</sub> OH		
C2H5OH	C <sub>2</sub> H <sub>5</sub> OH		
ACETOL	CH <sub>3</sub> COCH <sub>2</sub> OH	ALD	

Table S10: Listing of some optional, inert and tracer species

Model species	Formula	DRY <sup>†</sup>	WET <sup>†</sup>	Comments
APINENE	C <sub>10</sub> H <sub>16</sub>			Used if SOA scheme
ECnew_f		PMfS	PMecf	Fresh (hydrophobic) EC
ECage_f		PMfS	PMf	Aged (mixed, and hydrophilic) EC
SeaSalt_f		PMfS	PMssf	
SeaSalt_c		PMc	PMssc	
Dust_f		PMfS	PMf	
Dust_c		PMc	PMc	
REMPPM_f		PMfS	PMf	'remaining' primary particulate matter, fine-mode (excluding OM, EC)
REMPPM_c		PMc	PMc	As REMPPM_f, coarse mode
PPM25_FIRE		PMfS	PMf	Fire tracer
CO_FIRE	CO			Fire tracer
Rn222				Radon isotope tracer
Pb210		PMfS	PMf	Product from radon decay

Notes: Suffix \_f, \_c refer to fine and coarse mode aerosol species.

Table S11: Default Chemical Mechanism of EMEP model, EmChem09. For Notes, see end of Table

N	Rate coefficient	Reaction
<i>Inorganic chemistry</i>		
IN-1	$(6.0 \times 10^{-34} \text{ O}_2 \dots$ $\dots + 5.6 \times 10^{-34} \text{ N}_2) \times \text{O}_2 \times (T/300)^{-2.6}$	$\text{OP} + \text{O}_2 + \text{M} \Rightarrow \text{O}_3$
IN-2	$1.8 \times 10^{-11} \exp(107/T) \times \text{N}_2$	$\text{OD} + \text{N}_2 \Rightarrow \text{OP}$
IN-3	$3.2 \times 10^{-11} \exp(67/T) \times \text{O}_2$	$\text{OD} + \text{O}_2 \Rightarrow \text{OP}$
IN-4	$2.2 \times 10^{-10} \text{ H}_2\text{O}$	$\text{OD} + \text{H}_2\text{O} \Rightarrow 2. \text{OH}$
IN-5	$1.4 \times 10^{-12} \exp(-1310/T)$	$\text{O}_3 + \text{NO} \Rightarrow \text{NO}_2 + \text{O}_2$
IN-6	$1.4 \times 10^{-13} \exp(-2470/T)$	$\text{O}_3 + \text{NO}_2 \Rightarrow \text{NO}_3 + \text{O}_2$
IN-7	$1.7 \times 10^{-12} \exp(-940/T)$	$\text{O}_3 + \text{OH} \Rightarrow \text{HO}_2 + \text{O}_2$
IN-8	$2.03 \times 10^{-16} \times \dots$ $\dots (300/T)^{-4.57} \exp(693/T)$	$\text{O}_3 + \text{HO}_2 \Rightarrow \text{OH} + 2 \text{O}_2$
IN-9	$1.8 \times 10^{-11} \exp(110/T)$	$\text{NO} + \text{NO}_3 \Rightarrow \text{NO}_2 + \text{NO}_2$
IN-10	$3.6 \times 10^{-12} \exp(270/T)$	$\text{NO} + \text{HO}_2 \Rightarrow \text{NO}_2 + \text{OH}$
IN-11	$4.5 \times 10^{-14} \exp(-1260/T)$	$\text{NO}_2 + \text{NO}_3 \Rightarrow \text{NO} + \text{NO}_2$
IN-12	$4.8 \times 10^{-11} \exp(250/T)$	$\text{OH} + \text{HO}_2 \Rightarrow \text{H}_2\text{O} + \text{O}_2$
IN-13	$2.9 \times 10^{-12} \exp(-160/T)$	$\text{OH} + \text{H}_2\text{O}_2 \Rightarrow \text{HO}_2 + \text{H}_2\text{O}$
IN-14	$7.7 \times 10^{-12} \exp(-2100/T)$	$\text{OH} + \text{H}_2 \Rightarrow \text{HO}_2 + \text{H}_2\text{O}$
IN-15	$k_{\text{OH}+\text{HNO}_3}$	$\text{OH} + \text{HNO}_3 \Rightarrow \text{NO}_3 + \text{H}_2\text{O}$
IN-16	$k_{\text{HO}_2+\text{HO}_2}$	$\text{HO}_2 + \text{HO}_2 \Rightarrow \text{H}_2\text{O}_2$
IN-17	$2.5 \times 10^{-12} \exp(-260/T)$	$\text{OH} + \text{HONO} \Rightarrow \text{NO}_2$
IN-18	$k_{\text{N}_2\text{O}_5} \text{ (a)}$	$\text{N}_2\text{O}_5 \Rightarrow 2. \text{HNO}_3$
IN-19	$k_{\text{aero}}$	$\text{HNO}_3 \Rightarrow \text{NO}_3\text{-c}$
IN-20	$kt_{\text{NO}+\text{OP}}$	$\text{OP} + \text{NO} + \text{M} \Rightarrow \text{NO}_2$
IN-21	$kt_{\text{NO}_2+\text{NO}_3}$	$\text{NO}_2 + \text{NO}_3 \Rightarrow \text{N}_2\text{O}_5$
IN-22	$kt_{\text{N}_2\text{O}_5}$	$\text{N}_2\text{O}_5 \Rightarrow \text{NO}_2 + \text{NO}_3$
IN-23	$kt_{\text{NO}_2+\text{OH}}$	$\text{NO}_2 + \text{OH} + \text{M} \Rightarrow \text{HNO}_3$
IN-24	$kt_{\text{OH}+\text{NO}}$	$\text{OH} + \text{NO} \Rightarrow \text{HONO}$
<i>Sulphate (inc. in-cloud) formation</i>		
cl-OH	(b)	$\text{OH} + \text{SO}_2 \Rightarrow \text{HO}_2 + \text{SO}_4$
cl-1	(b)	$\text{SO}_2 + \text{H}_2\text{O}_2 \Rightarrow \text{SO}_4$
cl-2	(b)	$\text{SO}_2 + \text{O}_3 \Rightarrow \text{SO}_4$
cl-3	(b)	$\text{SO}_2 + \text{Fe} \Rightarrow \text{SO}_4$

Table S11: cont.

N	Rate coefficient	Reaction
<i>Methane chemistry</i>		
MA-1	$1.85 \times 10^{-20} \times T^{2.8} \dots$ $\dots \times \exp(-987/T)$	$\text{OH} + \text{CH}_4 \Rightarrow \text{CH}_3\text{O}_2$
MA-2	$1.44 \times 10^{-13} + 3.43 \times 10^{-33} \text{ M}$	$\text{OH} + \text{CO} \Rightarrow \text{HO}_2$
MA-3	$2.3 \times 10^{-12} \exp(360/T)$	$\text{CH}_3\text{O}_2 + \text{NO} \Rightarrow \text{HCHO} + \text{HO}_2 + \text{NO}_2$
MA-4	$7.4 \times 10^{-13} \exp(-520/T)$	$\text{CH}_3\text{O}_2 + \text{CH}_3\text{O}_2 \Rightarrow 2. \text{HCHO} + 2. \text{HO}_2$
MA-5	$1.03 \times 10^{-13} \exp(365/T) -$ $7.4 \times 10^{-13} \exp(-520/T)$	$\text{CH}_3\text{O}_2 + \text{CH}_3\text{O}_2 \Rightarrow \text{CH}_3\text{OH} + \text{HCHO}$
MA-6	$6.38 \times 10^{-18} \exp(144/T) \times T^2$	$\text{OH} + \text{CH}_3\text{OH} \Rightarrow \text{HO}_2 + \text{HCHO} + \text{H}_2\text{O}$
MA-7	$3.8 \times 10^{-13} \exp(780/T)$	$\text{HO}_2 + \text{CH}_3\text{O}_2 \Rightarrow 0.9 \text{CH}_3\text{O}_2\text{H} + 0.1 \text{HCHO}$
MA-8	$5.3 \times 10^{-12} \exp(190/T)$	$\text{CH}_3\text{O}_2\text{H} + \text{OH} \Rightarrow 0.4 \text{HCHO} + 0.4 \text{OH} + 0.6 \text{CH}_3\text{O}_2$ $+ 0.6 \text{H}_2\text{O}$
<i>Ethane and ethanol chemistry</i>		
EA-1	$1.25 \times 10^{-17} \times T^2 \dots$ $\dots \times \exp(615/T)$	$\text{OH} + \text{HCHO} \Rightarrow \text{CO} + \text{HO}_2 + \text{H}_2\text{O}$
EA-2	$2.0 \times 10^{-12} \exp(-2440/T)$	$\text{NO}_3 + \text{HCHO} \Rightarrow \text{HNO}_3 + \text{CO} + \text{HO}_2$
EA-3	$6.9 \times 10^{-12} \exp(-1000/T)$	$\text{OH} + \text{C}_2\text{H}_6 \Rightarrow \text{C}_2\text{H}_5\text{O}_2 + \text{H}_2\text{O}$
EA-4	$2.55 \times 10^{-12} \exp(380/T)$	$\text{C}_2\text{H}_5\text{O}_2 + \text{NO} \Rightarrow \text{HO}_2 + \text{CH}_3\text{CHO} + \text{NO}_2$
EA-5	$3.8 \times 10^{-13} \exp(900/T)$	$\text{C}_2\text{H}_5\text{O}_2 + \text{HO}_2 \Rightarrow \text{C}_2\text{H}_5\text{OOH}$
EA-6	$8.01 \times 10^{-12}$	$\text{C}_2\text{H}_5\text{OOH} + \text{OH} \Rightarrow \text{CH}_3\text{CHO} + \text{OH}$
EA-7	$k_{\text{OH}+\text{ROOH}}$	$\text{C}_2\text{H}_5\text{OOH} + \text{OH} \Rightarrow \text{C}_2\text{H}_5\text{O}_2$
EA-8	$4.4 \times 10^{-12} \exp(365/T)$	$\text{OH} + \text{CH}_3\text{CHO} \Rightarrow 0.95 \text{CH}_3\text{COO}_2 + 0.05 \text{CH}_3\text{O}_2 +$ $0.05 \text{CO}$
EA-9	$kt_{\text{panf}}$	$\text{CH}_3\text{COO}_2 + \text{NO}_2 + \text{M} \Rightarrow \text{PAN}$
EA-10	$kt_{\text{panb}}$	$\text{PAN} + \text{M} \Rightarrow \text{CH}_3\text{COO}_2 + \text{NO}_2$
EA-11	$7.5 \times 10^{-12} \exp(290/T)$	$\text{CH}_3\text{COO}_2 + \text{NO} \Rightarrow \text{NO}_2 + \text{CH}_3\text{O}_2 + \text{CO}_2$
EA-12	$2.0 \times 10^{-12} \exp(500/T)$	$\text{CH}_3\text{O}_2 + \text{CH}_3\text{COO}_2 \Rightarrow 0.9 \text{HO}_2 + \text{HCHO} + 0.9$ $\text{CH}_3\text{O}_2 + 0.1 \text{CH}_3\text{COOH}$
EA-13	$2.9 \times 10^{-12} \exp(500/T)$	$\text{CH}_3\text{COO}_2 + \text{CH}_3\text{COO}_2 \Rightarrow \text{CH}_3\text{O}_2 + \text{CH}_3\text{O}_2$
EA-14	$5.2 \times 10^{-13} \exp(980/T)$	$\text{CH}_3\text{COO}_2 + \text{HO}_2 \Rightarrow 0.41 \text{CH}_3\text{COO}_2\text{H} + 0.15 \text{O}_3 +$ $0.44 \text{OH} + 0.44 \text{CH}_3\text{O}_2 + 0.15 \text{CH}_3\text{COOH}$
EA-15	$1.9 \times 10^{-12} \exp(190/T)$	$\text{CH}_3\text{COO}_2\text{H} + \text{OH} \Rightarrow \text{CH}_3\text{COO}_2$
EA-16	$6.7 \times 10^{-18} \exp(511/T) \times T^2$	$\text{OH} + \text{C}_2\text{H}_5\text{OH} \Rightarrow \text{CH}_3\text{CHO} + \text{HO}_2$

Table S11: cont.

N	Rate coefficient	Reaction
<i>n-butane chemistry</i>		
NB-1	$2.03 \times 10^{-17} \exp(78/T) T^2$	$\text{OH} + \text{NC}_4\text{H}_{10} \Rightarrow \text{SECC}_4\text{H}_9\text{O}_2$
NB-2	$k_{\text{NO}+\text{RO}_2}$	$\text{NO} + \text{SECC}_4\text{H}_9\text{O}_2 \Rightarrow \text{NO}_2 + 0.65 \text{HO}_2 + 0.65 \text{MEK} + 0.35 \text{CH}_3\text{CHO} + 0.35 \text{C}_2\text{H}_5\text{O}_2$
NB-3	$0.625 \times k_{\text{HO}_2+\text{RO}_2}$	$\text{SECC}_4\text{H}_9\text{O}_2 + \text{HO}_2 \Rightarrow \text{BURO}_2\text{H}$
NB-4	$2.53 \times 10^{-18} \exp(503/T) T^2$	$\text{OH} + \text{MEK} \Rightarrow \text{MEKO}_2$
NB-5	$k_{\text{NO}+\text{RO}_2}$	$\text{MEKO}_2 + \text{NO} \Rightarrow \text{NO}_2 + \text{CH}_3\text{COO}_2 + \text{CH}_3\text{CHO}$
NB-6	$0.625 \times k_{\text{HO}_2+\text{RO}_2}$	$\text{MEKO}_2 + \text{HO}_2 \Rightarrow \text{MEKO}_2\text{H}$
NB-7	$1.9 \times 10^{-12} \exp(190/T)$	$\text{MEKO}_2\text{H} + \text{OH} \Rightarrow \text{MEKO}_2$
NB-8	$k_{\text{OH}+\text{ROOH}}$	$\text{BURO}_2\text{H} + \text{OH} \Rightarrow \text{SECC}_4\text{H}_9\text{O}_2$
NB-9	$2.15 \times 10^{-11}$	$\text{BURO}_2\text{H} + \text{OH} \Rightarrow \text{OH} + \text{MEK}$
<i>Ethene chemistry</i>		
EE-1	$kt_{\text{OH}+\text{C}_2\text{H}_4}$	$\text{C}_2\text{H}_4 + \text{OH} + \text{M} \Rightarrow \text{ETRO}_2$
EE-2	$k_{\text{NO}+\text{RO}_2}$	$\text{ETRO}_2 + \text{NO} \Rightarrow \text{NO}_2 + 2. \text{HCHO} + \text{HO}_2$
EE-3	$1.2 \times 10^{-11}$	$\text{ETRO}_2 + \text{HO}_2 \Rightarrow \text{ETRO}_2\text{H}$
EE-4	$1.38 \times 10^{-11}$	$\text{ETRO}_2\text{H} + \text{OH} \Rightarrow \text{CH}_3\text{CHO} + \text{OH}$
EE-5	$k_{\text{OH}+\text{ROOH}}$	$\text{ETRO}_2\text{H} + \text{OH} \Rightarrow \text{ETRO}_2$
EE-6	$9.1 \times 10^{-15} \exp(-2580/T)$	$\text{C}_2\text{H}_4 + \text{O}_3 \Rightarrow 1.14 \text{HCHO} + 0.63 \text{CO} + 0.13 \text{HO}_2 + 0.13 \text{OH} + 0.14 \text{H}_2\text{O}_2 + 0.23 \text{HCOOH}$
<i>Propene chemistry</i>		
PE-1	$5.5 \times 10^{-15} \exp(-1880/T)$	$\text{O}_3 + \text{C}_3\text{H}_6 \Rightarrow 0.545 \text{HCHO} + 0.545 \text{CH}_3\text{CHO} + 0.56 \text{CO} + 0.36 \text{OH} + 0.28 \text{HO}_2 + 0.09 \text{H}_2\text{O}_2 + 0.1 \text{CH}_4 + 0.28 \text{CH}_3\text{O}_2 + 0.075 \text{HCOOH} + 0.075 \text{CH}_3\text{COOH}$
PE-2	$kt_{\text{OH}+\text{C}_3\text{H}_6}$	$\text{OH} + \text{C}_3\text{H}_6 + \text{M} \Rightarrow \text{PRRO}_2$
PE-3	$k_{\text{NO}+\text{RO}_2}$	$\text{NO} + \text{PRRO}_2 \Rightarrow \text{NO}_2 + \text{CH}_3\text{CHO} + \text{HCHO} + \text{HO}_2$
PE-4	$0.52 \times k_{\text{HO}_2+\text{RO}_2}$	$\text{PRRO}_2 + \text{HO}_2 \Rightarrow \text{PRRO}_2\text{H}$
PE-5	$2.44 \times 10^{-11}$	$\text{PRRO}_2\text{H} + \text{OH} \Rightarrow \text{ACETOL} + \text{OH}$
PE-6	$k_{\text{OH}+\text{ROOH}}$	$\text{PRRO}_2\text{H} + \text{OH} \Rightarrow \text{PRRO}_2$

Table S11: cont.

N	Rate coefficient	Reaction
<i>o</i> -xylene chemistry		
OX-1	$1.36 \times 10^{-11}$	OXYL + OH $\Rightarrow$ OXYO2
OX-2	$k_{NO+RO2}$	OXYO2 + NO $\Rightarrow$ NO2 + MGLYOX + MAL + HO2
OX-3	$0.859 \times k_{HO2+RO2}$	OXYO2 + HO2 $\Rightarrow$ OXYO2H
OX-4	$4.2 \times 10^{-11}$	OXYO2H + OH $\Rightarrow$ OXYO2
OX-5	$5.58 \times 10^{-11}$	MAL + OH $\Rightarrow$ MALO2
OX-6	$k_{NO+RO2}$	MALO2 + NO $\Rightarrow$ NO2 + HO2 + MGLYOX + GLYOX
OX-7	$0.706 \times k_{HO2+RO2}$	MALO2 + HO2 $\Rightarrow$ MALO2H
OX-8	$1.9 \times 10^{-12} \exp(190/T)$	MALO2H + OH $\Rightarrow$ MALO2
OX-9	$6.6 \times 10^{-18} \exp(820/T) \times T^2$	OH + GLYOX $\Rightarrow$ HO2 + 2 CO
<i>Isoprene chemistry</i>		
IS-1	$1.03 \times 10^{-14} \exp(-1995/T)$	C5H8 + O3 $\Rightarrow$ 0.67 MACR + 0.26 MVK + 0.3 OP + 0.55 OH + 0.07 C3H6 + 0.8 HCHO + 0.06 HO2 + 0.05 CO
IS-2	$2.7 \times 10^{-11} \exp(390/T)$	C5H8 + OH $\Rightarrow$ ISRO2
IS-3	$k_{NO+RO2}$	ISRO2 + NO $\Rightarrow$ 0.32 MACR + 0.42 MVK + 0.74 HCHO + 0.14 ISNI + 0.12 ISRO2 + 0.78 HO2 + 0.86 NO2
IS-4	$0.706 \times k_{HO2+RO2}$	ISRO2 + HO2 $\Rightarrow$ ISRO2H
IS-5	$2.6 \times 10^{-12} \exp(610/T)$	MVK + OH $\Rightarrow$ MVKO2
IS-6	$k_{NO+RO2}$	MVKO2 + NO $\Rightarrow$ 0.684 CH3CHO + 0.684 CH3COO2 + 0.266 MGLYOX + 0.266 HCHO + 0.05 ISNI + 0.95 NO2 + 0.95 HO2
IS-7	$7.5 \times 10^{-11}$	ISRO2H + OH $\Rightarrow$ OH + ISRO2
IS-8	$1.36 \times 10^{-15} \exp(-2112/T)$	MACR + O3 $\Rightarrow$ 0.59 MGLYOX + 0.41 HO2 + 0.82 CO + 0.82 OH + 0.534 HCHO + 0.124 H2O2 + 0.41 CH3COO2 + 0.056 HCOOH
IS-9	$8.0 \times 10^{-12} \exp(380/T)$	MACR + OH $\Rightarrow$ 0.5 MACRO2 + 0.5 MACO3
IS-10	$kt_{panf}$	MACO3 + NO2 $\Rightarrow$ MPAN
IS-11	$kt_{panb}$	MPAN $\Rightarrow$ MACO3 + NO2
IS-12	$7.6 \times 10^{-12} \exp(180/T)$	MACRO2 + NO $\Rightarrow$ 0.95 HO2 + 0.95 CO + 0.95 ACETOL + 0.05 ISNI + 0.95 NO2
IS-13	$2.5 \times 10^{-12}$	MACRO2 + NO3 $\Rightarrow$ NO2 + ACETOL + HCHO + HO2
IS-14	$0.625 \times k_{HO2+RO2}$	MACRO2 + HO2 $\Rightarrow$ MACROOH + O2
IS-15	$2.82 \times 10^{-11}$	MACROOH + OH $\Rightarrow$ MACRO2
IS-16	$1.6 \times 10^{-12} \exp(305/T)$	ACETOL + OH $\Rightarrow$ MGLYOX + HO2
IS-17	$8.7 \times 10^{-12} \exp(290/T)$	MACO3 + NO $\Rightarrow$ CH3COO2 + HCHO + NO2

Table S11: cont.

N	Rate coefficient	Reaction
<i>Isoprene cont.</i>		
IS-18	$8.5 \times 10^{-16} \exp(-1520/T)$	MVK + O3 $\Rightarrow$ 0.82 MGLYOX + 0.8 HCHO + 0.2 OP + 0.05 CO + 0.06 HO2 + 0.04 CH3CHO + 0.08 OH
IS-19	$5.96 \times 10^{-11}$	ISNI + OH $\Rightarrow$ ISNIR
IS-20	$k_{NO+RO2}$	ISNIR + NO $\Rightarrow$ 0.05 ISNI + 0.05 HO2 + 1.9 NO2 + 0.95 CH3CHO + 0.95 ACETOL
IS-21	$3.15 \times 10^{-12} \exp(-450/T)$	C5H8 + NO3 $\Rightarrow$ ISONO3
IS-22	$k_{NO+RO2}$	ISONO3 + NO $\Rightarrow$ 1.1 NO2 + 0.8 HO2 + 0.85 ISNI + 0.1 MACR + 0.15 HCHO + 0.05 MVK
IS-23	$0.706 \times k_{HO2+RO2}$	ISONO3 + HO2 $\Rightarrow$ ISONO3H
IS-24	$0.625 \times k_{HO2+RO2}$	MVKO2 + HO2 $\Rightarrow$ MVKO2H
IS-25	$4.3 \times 10^{-13} \exp(1040/T)$	MACO3 + HO2 $\Rightarrow$ 0.71 MACO3H + 0.29 MACO2H + 0.29 O3
IS-26	$1.87 \times 10^{-11}$	MACO3H + OH $\Rightarrow$ MACO3
IS-27	$1.51 \times 10^{-11}$	MACO2H + OH $\Rightarrow$ CH3COO2 + HCHO
IS-28	$0.706 \times k_{HO2+RO2}$	ISNIR + HO2 $\Rightarrow$ ISNIRH
IS-29	$2.0 \times 10^{-11}$	ISONO3H + OH $\Rightarrow$ ISONO3
IS-30	$2.2 \times 10^{-11}$	MVKO2H + OH $\Rightarrow$ MVKO2
IS-31	$3.7 \times 10^{-11}$	ISNIRH + OH $\Rightarrow$ ISNIR
IS-32	$2.9 \times 10^{-11}$	MPAN + OH $\Rightarrow$ ACETOL + CO + NO2
<i>Miscellaneous</i>		
MS-1	2.1E-6	RN222 $\Rightarrow$ PB210
MS-2	$1.0E-12 \times H2O$	PB210 $\Rightarrow$ aerosol sink
MS-3	1.0E-5	H2O2 $\Rightarrow$ aerosol sink
MS-4	1.0E-5	CH3O2H $\Rightarrow$ aerosol sink
MS-5	$k_{ECage}$	ECnew_f $\Rightarrow$ ECage_f

Notes. T is temperature, M is third body; Reaction coefficients are in units of  $s^{-1}$  for unimolecular reactions,  $cm^3 \text{ molecule}^{-1} s^{-1}$  for bimolecular reactions, and  $cm^6 \text{ molecule}^{-2} s^{-2}$  for termolecular reactions. Reaction steps labelled as "Immediate" are given for clarity only. Rate-coefficients labelled with  $kt$  are given as Troe expressions in Table S12, and coefficients labelled with  $k$  are given in Table S13 (except (a), below). (a)  $k_{N2O5}$  discussed in Sect. 7.7, main article. (b) The 'cl' rates for sulphate formation involve cloud-water calculations and are discussed in Sect. 7.5–7.6, main article.



Table S12: Rate-constants for 3-body reactions using the Troe expression<sup>(a)</sup> The reaction rates are calculated as:  $k = \frac{k_0 k_\infty}{k_0 + k_\infty} F$ , with the broadening factor  $F$  calculated using the approximate expression:  $\log_{10} F \cong \frac{\log_{10} F_c}{1 + [\log_{10}(k_0/k_\infty)/N]^2}$  where  $N = [0.75 - 1.27 \log_{10} F_c]$  The first column (Rate coeff.) refers to the notation in Table S11.

Rate coeff.	$k_0/[M]$	$k_\infty$	$F_c$
$kt_{NO+OP}$	$1.0 \times 10^{-31} (300/T)^{1.6}$	$3.0 \times 10^{-11} (300/T)^{-0.3}$	0.85
$kt_{NO_2+NO_3}$	$3.6 \times 10^{-30} (300/T)^{4.1}$	$1.9 \times 10^{-12} (300/T)^{-0.2}$	0.35
$kt_{N_2O_5}$	$1.3 \times 10^{-3} (300/T)^{3.5} e^{(-11000/T)}$	$9.70 \times 10^{14} (300/T)^{-0.1} e^{(-11080/T)}$	0.35
$kt_{NO_2+OH}$	$3.3e \times 10^{30} (300/T)^{3.0}$	$4.1 \times 10^{-11}$	0.40
$kt_{OH+NO}$	$7.4 \times 10^{-31} (300/T)^{2.4}$	$3.3 \times 10^{-11} (300/T)^{0.3}$	$e^{(-T/1420)}$
$kt_{OH+C_2H_4}$	$8.6 \times 10^{-29} (300/T)^{3.1}$	$9.0 \times 10^{-12} (300/T)^{0.85}$	0.48
$kt_{NO+OP}$	$1.0 \times 10^{-31} (300/T)^{1.6}$	$3.0 \times 10^{-11} (300/T)^{-0.3}$	0.85
$kt_{OH+C_3H_6}$	$8.0 \times 10^{-27} (300/T)^{3.5}$	$3.0 \times 10^{-11} \exp(300/T)$	0.5
$kt_{panf}$	$2.7 \times 10^{-28} (300/T)^{7.1}$	$1.2 \times 10^{-11} (300/T)^{0.9}$	0.3
$kt_{panb}$	$4.9 \times 10^{-3} (300/T)^{-12100}$	$5.4 \times 10^{16} \exp(-13830/T)$	0.3

(a) For form of Troe expressions, see eg Atkinson et al. (2006)).

Table S13: Other rate coefficients

No.	rate	Comments
$k_{OH+HNO_3}$	$= K_1 + (K_3[M]) / (1.0 + (K_3[M]) / K_4)$ , where $K_1 = 2.4 \times 10^{-14} \exp(460/T)$ $K_2 = 6.5 \times 10^{-34} \exp(1335/T)$ $K_3 = 2.7 \times 10^{-17} \exp(2199/T)$	
$k_{HO_2+HO_2}$	$= F_{H_2O} \times 2.2 \times 10^{-13} \exp(600/T) \dots$ $+ F_{H_2O} \times 1.9 \times 10^{-33} \exp(980/T) \times M$ ,	where $F_{H_2O} =$ $1 + 1.4 \times 10^{-21} \exp(2200/T) [H_2O]$
$k_{OH+ROOH}$	$= 1.9 \times 10^{-12} \exp(190/T)$	
$k_{HO_2+RO_2}$	$= 2.91 \times 10^{-13} \exp(1300/T)$	
$k_{NO+RO_2}$	$= 2.54 \times 10^{-12} \exp(360/T)$	
$k_{aero}$	$= 1.0 \times 10^{-5}$ when RH > 90%, else $5.0 \times 10^{-6}$	
$k_{ECage}$ (day)	$= 3.3 \times 10^{-6}$ for lowest 3 layers (<300m approx) $= 1.4 \times 10^{-4}$ for upper layers (>300m approx)	Tsyro et al. (2007)
$k_{ECage}$ (night)	$= 1.0 \times 10^{-5}$ for lowest 3 layers (<300m approx)	

Table S14: Photolysis reactions. For some reactions, rates are taken from given surrogate species, scaled if necessary

N	Reaction
J-O3A	$O_3 \Rightarrow OP$
J-O3B	$O_3 \Rightarrow OD$
J-NO2	$NO_2 \Rightarrow OP + NO$
J-H2O2	$H_2O_2 \Rightarrow 2 OH$
J-HNO3	$HNO_3 \Rightarrow NO_2 + OH$
J-HCHOA	$HCHO \Rightarrow CO + 2 HO_2$
J-HCHOB	$HCHO \Rightarrow CO + H_2$
J-CH3CHO	$CH_3CHO \Rightarrow CH_3O_2 + HO_2 + CO$
J-NO3	$NO_3 \Rightarrow NO_2 + OP$
J-CH3O2H	$CH_3O_2H \Rightarrow HCHO + OH + HO_2$
J-GLYOX	$GLYOX \Rightarrow 1.9 CO + 0.1 HCHO + 0.5 HO_2$
J-RCOHCO	$MGLYOX \Rightarrow CH_3COO_2 + CO + HO_2$
J-CH3O2H	$C_2H_5OOH \Rightarrow HO_2 + CH_3CHO + OH$
J-CH3O2H	$ETRO_2H \Rightarrow HO_2 + OH + 1.56 HCHO + 0.22 CH_3CHO$
J-CH3O2H	$BURO_2H \Rightarrow OH + 0.65 HO_2 + 0.65 MEK + 0.35 CH_3CHO + 0.35 C_2H_5O_2$
J-CH3O2H	$PRRO_2H \Rightarrow CH_3CHO + HCHO + HO_2$
J-CH3O2H	$MEKO_2H \Rightarrow CH_3CHO + CH_3COO_2 + OH$
J-CH3COX	$MEK \Rightarrow CH_3COO_2 + C_2H_5O_2$
J-CH3O2H	$CH_3COO_2H \Rightarrow CH_3O_2 + OH$
J-CH3O2H	$OXYO_2H \Rightarrow OH + MGLYOX + MAL + HO_2$
J-CH3O2H	$MALO_2H \Rightarrow OH + HO_2 + MGLYOX + GLYOX$
0.222 J-NO2	$HONO \Rightarrow OH + NO$

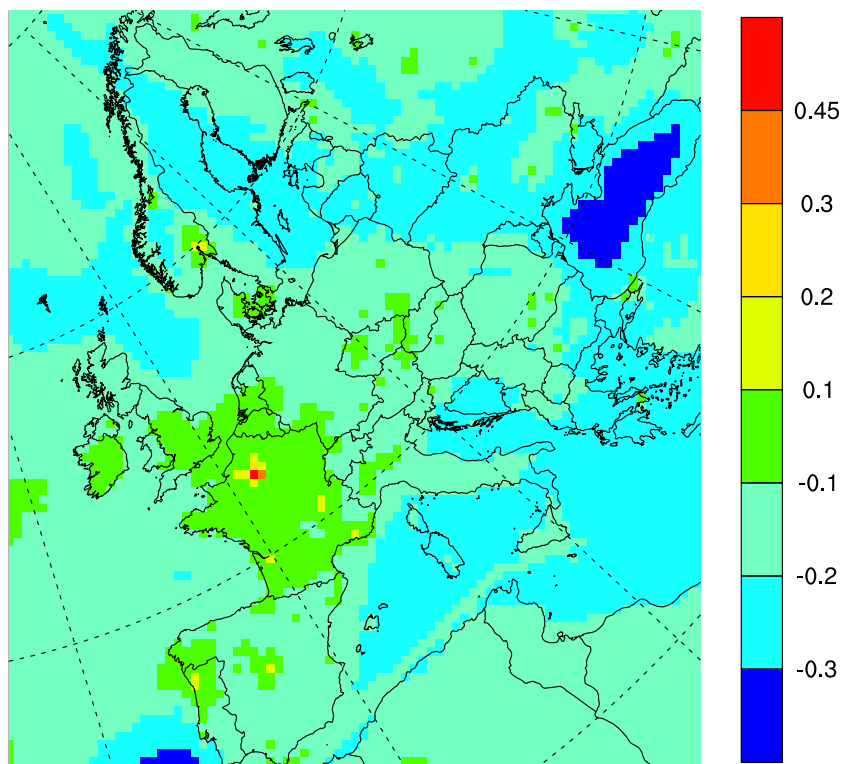


Figure S2: Relative difference in fine organic aerosol concentrations obtained using the NPAS scheme (with inert POA) to those obtained with the PAA scheme of Bergström et al. 2012, which has volatile POA emissions and atmospheric aging of the emitted semi- and intermediate volatility OC. Calculations for the year 2006. (Relative difference defined as:  $[\text{NPAS}-\text{PAA}]/\text{PAA}$ ).

## S6 Sensitivity test: POA

As discussed in Sects. 7.9 and 12, the 'standard' EMEP model, using our so-called NPAS version of the VBS methodology, assumes that primary organic aerosol (POA) emissions are inert, whereas the research versions of the model presented by Bergström et al. (2012) have allowed for the volatility of POA emissions and also introduced related emissions of semi- and intermediate-volatility gases. Fig. S2 shows the relative difference in modelled OA concentrations using the NPAS assumptions compared to a scheme (PAA, see Bergström et al. 2012) using these more complex VBS assumptions. The results are discussed in Sect. 12.

## S7 Dry deposition, additional information

### S7.1 Leaf area index calculations

Leaf area index (LAI, which is one-sided, projected) is calculated according to Table S15, making use of Table 3.

Table S15: Calculation of LAI as a function of daynumber  $d_n$ , start and end days of growing season ( $d_{SGS}$ ,  $d_{EGS}$ ), and other parameters as given in Table 3. See also Fig. 4.

Time of year	LAI
$d_n \leq d_{SGS}$ or $d_n \geq d_{EGS}$	$LAI_{\min}$
$d_{SGS} < d_n \leq d_{SGS} + L_S$	$LAI_{\min} + (LAI_{\max} - LAI_{\min})(d_n - d_{SGS})/L_S$
$d_{SGS} + L_S < d_n \leq d_{EGS} - L_E$	$LAI_{\max}$
$d_{EGS} - L_E < d_n < d_{EGS}$	$LAI_{\min} + (LAI_{\max} - LAI_{\min})(d_{EGS} - d_n)/L_E$

### S7.2 Stomatal conductance calculations

As noted in Sect. 8.5, the calculation of stomatal conductance according to the DO<sub>3</sub>SE algorithm requires the calculation of factors accounting for time of year (leaf phenology factor,  $f_{phen}$ ), the minimum observed stomatal conductance ( $f_{\min}$ ), light (PAR, with factor  $f_{light}$ ), temperature ( $f_T$ ), vapour-pressure deficit ( $D$ , factor  $f_D$ ), and soil-water (SW, factor  $f_{SW}$ ). Such functions and their parameters have been presented widely in the literature, and in LRTAP (2009). However, the values and equations have been modified over the years. Here we present the equations and parameter values used in the current (rv4) EMEP model. These are loosely based upon those presented in LRTAP (2009), but (especially in the case of  $f_{phen}$ ) simplified somewhat to match the limitations inherent in large-scale modelling. As an important example, we have shown previously that even such basic parameters as the start of the growing season are difficult to capture with European-wide models (Tuovinen et al., 2009).

Table S16 lists  $g_{max}$  values (given at normal temperature and pressure, in mmole O<sub>3</sub> m<sup>-2</sup> (PLA) s<sup>-1</sup>, denoted  $g_{max}^m$ ) along with values of other parameters needed for the conductance modelling. For pressure  $P$  and temperature  $T$ ,  $g_{max}$  in m s<sup>-1</sup> units is given by:

$$g_{max} = g_{max}^m R T / P \quad (12)$$

$R$  is here the gas-constant (8.314 J mole<sup>-1</sup> K<sup>-1</sup>). At normal temperature and pressure,  $g_{max} \approx g_{max}^m / 41000$ . The canopy average stomatal conductance,  $g_{sto}$ , is calculated as:

$$g_{sto} = g_{max} f_{phen} f_{light} \max(f_{\min}, f_T f_D f_{SW}) \quad (13)$$

Table S16 gives the landcover species parameters associated with  $f_{phen}$ ,  $f_{light}$ ,  $f_T$  and  $f_D$ .  $f_{phen}$  is calculated according to Table S17, and is illustrated for two land-cover types in Fig. S3. The summertime dip in  $f_{phen}$  for the Mediterranean species is intended to reflect the well-documented effects of drought-stress on vegetation in this area, although it is an open question

if this procedure is double-counted in the  $f_{SW}$  function (see Alonso et al., 2008, for contrasting examples).

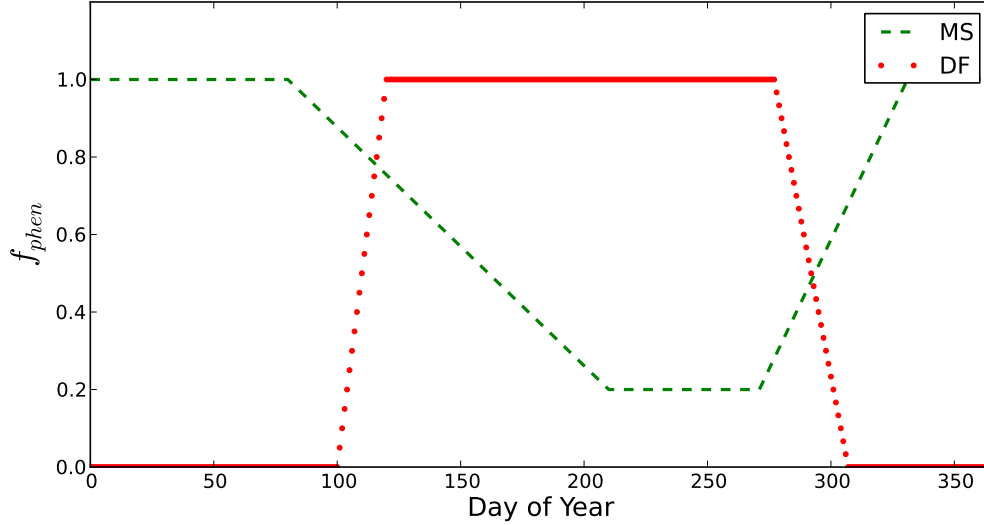


Figure S3: Illustration of  $f_{phen}$  function for two contrasting land-cover classes, DF (tempera-  
ture/boreal deciduous, here at 50° N) and (MS) Mediterranean scrub.

Table S16: Land-cover specific parameters for stomatal conductance ( $DO_3SE$ ) calculations

Code	$g_{max}^m$	$f_{min}$	$f_{phen}$ factors								$f_{light}$	$f_T$			$f_D$		
			$\phi_a$	$\phi_b$	$\phi_c$	$\phi_d$	$\phi_e$	$\phi_f$	$\phi_{AS}$	$\phi_{AE}$		$\alpha$	$T_{min}$	$T_{opt}$	$T_{max}$	$D_{max}$	$D_{min}$
	†						days	days	days	days		°C	°C	°C	kPa	kPa	kPa
CF	140	0.1	0.8	0.8	0.8	0.8	1	1	0	0	0.006	0	18	36	0.5	3	
DF	150	0.1	0	0	1	0	20	30	0	0	0.006	0	20	35	1	3.25	
NF	200	0.1	1	1	0.2	1	130	60	80	35	0.013	8	25	38	1	3.2	
BF	200	0.02	1	1	0.3	1	130	60	80	35	0.009	1	23	39	2.2	4	
TC	300	0.01	0.1	0.1	1	0.1	0	45	0	0	0.0105	12	26	40	1.2	3.2	8
MC	300	0.019	0.1	0.1	1	0.1	0	45	0	0	0.0048	0	25	51	1	2.5	
RC	360	0.02	0.2	0.2	1	0.2	20	45	0	0	0.0023	8	24	50	0.31	2.7	10
SNL	60	0.01	1	1	1	1	1	1	0	0	0.009	1	18	36	1.3	3	
GR	270	0.01	1	1	1	1	0	0	0	0	0.009	12	26	40	1.3	3	
MS	200	0.01	1	1	0.2	1	130	60	80	35	0.012	4	20	37	1.3	3.2	
IAM.CR	500	0.01	0.1	0.1	1	0.1	0	45	0	0	0.0105	12	26	40	1.2	3.2	8
IAM_DF	150	0.1	0	0	1	0	15	20	0	0	0.006	0	21	35	1	3.25	
IAM.MF	175	0.02	1	1	0.3	1	130	60	80	35	0.009	2	23	38	2.2	4	

Notes: † Units of  $g_{max}^m$  are  $\text{mmole O}_3 \text{ m}^{-2} (\text{PLA}) \text{ s}^{-1}$

Table S17: Definition of phenology function,  $f_{phen}$  as a function of daynumber  $d_n$ , start and end of growing season ( $d_{SGS}$ ,  $d_{EGS}$ ), and other parameters as given in Table S16

Time of year	$f_{phen}$
$d_n \leq d_{SGS}$ or $d_n > d_{EGS}$	0
$d_{SGS} < d_n \leq A_{start}$	$\phi_a$
$A_{start} < d_n \leq A_{start} + \phi_e$	$\phi_b + (\phi_c - \phi_b)(d_n - A_{start})/\phi_e$
$A_{start} + \phi_e < d_n \leq A_{end} - \phi_f$	$\phi_c$
$A_{end} - \phi_f < d_n \leq A_{end}$	$\phi_d + (\phi_c - \phi_d)(A_{end} - d_n)/\phi_f$
$A_{end} < d_n \leq d_{EGS}$	$\phi_d$

Notes:  $A_{start}$  calculated from  $d_{SGS} + \phi_{A_S}$ ,  $A_{end}$  from  $d_{EGS} - \phi_{A_E}$ , c.f. Table S16.

Calculation of  $f_{\text{light}}$  makes use of the photosynthetic active radiation components,  $I_{\text{PAR}}^{\text{sun}}$  and  $I_{\text{PAR}}^{\text{shade}}$ , as presented in Sect. 4. We calculate the effects for sun and shade leaves with:

$$f_{\text{sun}} = 1 - e^{-\alpha I_{\text{PAR}}^{\text{sun}}} \quad (14)$$

$$f_{\text{shade}} = 1 - e^{-\alpha I_{\text{PAR}}^{\text{shade}}} \quad (15)$$

where  $\alpha$  values are land-cover specific and given in Table S16. Given the fraction of leaves in sun ( $f_{\text{LAI}}^{\text{sun}} = \text{LAI}_{\text{sun}}/\text{LAI}$ , Sect. 4), the canopy average  $f_{\text{light}}$  is calculated as:

$$f_{\text{light}} = f_{\text{LAI}}^{\text{sun}} f_{\text{sun}} + (1 - f_{\text{LAI}}^{\text{sun}}) f_{\text{shade}} \quad (16)$$

Calculation of  $f_T$  uses the 2m air temperature  $T_2$ , together with parameters from Table S16:

$$f_T = \frac{T_2 - T_{\text{min}}}{T_{\text{opt}} - T_{\text{min}}} \left( \frac{T_{\text{max}} - T_2}{T_{\text{max}} - T_{\text{opt}}} \right)^\beta \quad (17)$$

where  $\beta$  is given by  $(T_{\text{max}} - T_{\text{opt}})/(T_{\text{opt}} - T_{\text{min}})$ .  $f_T$  is constrained with a minimum value of 0.01 (all temperatures here are in °C). The effects of humidity are accounted for with  $f_D$ , with the basic calculation given by:

$$f_D = f_{\text{min}} + (1 - f_{\text{min}}) \frac{D_{\text{min}} - D}{D_{\text{min}} - D_{\text{max}}} \quad (18)$$

$f_D$  is further constrained to lie between  $f_{\text{min}}$  and 1.0.

For a few landcover categories (see Table S16),  $\Sigma D_{\text{Crit.}}$  values are specified. For these landcovers, we also calculate  $\Sigma D$  (h), the hourly time-integral all vapour pressure deficits from sunrise until the current hour, h.  $\Sigma D$  accumulates over the day, and when  $\Sigma D$  (h) exceeds  $\Sigma D_{\text{Crit.}}$ , then we enforce:

$$g_{\text{sto}}(h) \leq g_{\text{sto}}(h - 1) \quad (19)$$

This procedure is mainly designed to prevent afternoon  $g_{\text{sto}}$  increasing after a period of morning water stress, as suggested by Uddling et al. (2004) and LRTAP (2009).

As noted in Sect. 3.3, soil water (SW) is very difficult to model accurately in large-scale models, and the soil moisture index,  $S_{\text{MI}}$  is used instead. The equation used for  $f_{\text{SW}}$  is given in Sect. 8.5 (Eq. 58) of the main text.

## S7.3 Properties of gases for dry deposition

Table S18: Properties of gases for dry deposition calculations. Diffusivity ratio for a gas  $i$ ,  $D_r = D_{H_2O}/D_i$ , Solubility index  $H_*$  (based upon Effective Henry's coefficient), and Reactivity index  $f_o$ . Based upon Wesely et al. (1985).

Gas	$D_r$	$H_*$	$f_o$
SO2	1.9	$1.0 \times 10^5$	0.0
O3	1.6	$1.0 \times 10^{-2}$	1.0
NO2	1.6	$1.0 \times 10^{-2}$	0.1
HNO3	1.9	$1.0 \times 10^{14}$	0.0
H2O2	1.4	$1.0 \times 10^5$	1.0
HCHO	1.3	$6.0 \times 10^3$	0.0
ALD <sup>(a)</sup>	1.6	15	0.0
OP <sup>(b)</sup>	1.6	$2.4 \times 10^2$	0.1
NH3 <sup>(c)</sup>	1.0	$1.0 \times 10^5$	0.0
PAN	2.6	3.6	0.1

Notes: (a) Used for all aldehydes except HCHO; (b) OP=Wesely "Methyl hydroperoxide" - used for all hydroperoxides (c)  $H_*$  increased compared to Wesely value, reflecting European pH conditions.

Table S19: Base-values of ground-surface resistance for sulphur dioxide ( $\hat{R}_{gs}^{SO_2}$ ) and ozone ( $\hat{R}_{gs}^{O_3}$ ). Units:  $s\ m^{-1}$ .

Landuse	$\hat{R}_{gs}^{SO_2}$	$\hat{R}_{gs}^{O_3}$
Forests, Mediterranean scrub	-	200
Crops	-	200
Moorland	-	400
Grasslands	-	1000
Wetlands	50	400
Tundra	500	400
Desert	1000	2000
Water	1	2000
Ice+snow	1000	2000
Urban	400	400

Notes: '-' - denotes other formulation, using resistances calculated as given in Sect. 8.7.



## S8 Wet deposition, additional information

Table S20: Wet scavenging ratios and collection efficiencies used in the EMEP MSC-W model.

Components <sup>(a)</sup>	$W_{in} (\times 10^6)$	$W_{sub} (\times 10^6)$	$\bar{E}$	Comment
SO <sub>2</sub>	0.3	0.15	-	
HNO <sub>3</sub> , HONO, NH <sub>3</sub> , H <sub>2</sub> O <sub>2</sub>	1.4	0.5	-	
HCHO	0.1	0.03	-	
ROOH	0.05	0.015	-	
PMf	1.0	-	0.02	Generic fine particles, includes SO <sub>4</sub> <sup>2-</sup> , NH <sub>4</sub> <sup>-</sup> , fine-NO <sub>3</sub> <sup>-</sup> , ECage.f, OA <sup>(b)</sup> , fine-dust
PMecf	0.2	-	0.02	Fresh (hydrophobic) ECnew.f
PMssf	1.6	-	0.02	Fine sea-salt
PMssc	1.6	-	0.4	Coarse sea-salt
PMc	1.0	-	0.4	Other coarse particles, includes coarse: NO <sub>3</sub> <sup>-</sup> , PPM, dust

(a) ROOH, and PM- type components are generic labels, see also Table S5 for particles associated with these rates; (b) For semi-volatile compounds associated with organic aerosol (OA), only the particle fraction is scavenged.

## S8.1 Initial and boundary conditions, additional information

Table S21: Parameters used to set prescribed boundary conditions

	$\chi_{mean}$ ppb	$d_{max}$ days	$\Delta\chi$ ppb	$H_z$ km	$\chi_{min}^v$ ppb	$\chi_{min}^h$ ppb
SO2	0.15	15	0.05	$\infty$	0.15	0.03
SO4	0.15	180	0.00	1.6	0.05	0.03
NO	0.1	15	0.03	4.0	0.03	0.02
NO2	0.1	15	0.03	4.0	0.05	0.04
PAN	0.20	120	0.15	$\infty$	0.20	0.1
CO	125.0	75	35.0	25.0	70.0	30.0
HNO <sub>3</sub>	0.07	180	0.03	$\infty$	0.025	0.03
nitrate <sup>(a)</sup>	0.07	15	0.03	1.6	0.025	0.02
NH <sub>4</sub> <sup>+</sup>	0.15	180	0.0	1.6	0.5	0.03
C2H6	2.0	75	1.0	10.0	0.05	0.05
C4H10	2.0	45	1.0	6.0	0.05	0.05
HCHO	0.7	180	0.3	6.0	0.05	0.05
CH3CHO	0.3	180	0.05	6.0	0.005	0.005
Seasalt fine	0.5	15	0.3	1.6	0.01	0.01
Seasalt coarse	3.0	15	1.0	1.6	0.01	0.01

Notes: See text for definition of terms. (a) same values used for both coarse and fine nitrate. Concentrations and other parameters estimated largely from Warneck (1988); Derwent et al. (1998); Ehhalt et al. (1991); Emmons et al. (2000); Isaksen and Hov (1987); Lewis et al. (2005); Millet et al. (2010); Penkett et al. (1993); Singh et al. (2004); Solberg et al. (1996, 2001) and University of Oslo CTM2 model (Sundet, 1997).

Table S22: Latitude factors applied to prescribed boundary and initial conditions.

Component	Latitude (° N)								
	30	35	40	45	50	55	60	65	70-90
SO2 <sup>a</sup>	0.05	0.15	0.3	0.8	1.0	0.6	0.2	0.12	0.05
HNO3 <sup>b</sup>	1.00	1.00	1.00	0.85	0.7	0.55	0.4	0.3	0.2
PAN	0.15	0.33	0.5	0.8	1.0	0.75	0.5	0.3	0.1
CO	0.6	0.7	0.8	0.9	1.0	1.0	0.95	0.85	0.8

Notes: (a) Applied also for SO<sub>4</sub>, NO, NO<sub>2</sub>; (b) Applied also for HCHO, CH<sub>3</sub>CHO; See Simpson (1992) for sources of data

Table S23: Assumed trends for boundary concentrations

Species	Trend , pre-1990 %/year	Trend , post-1990 %/year	Notes
O3	1	(a)	(b)
CO	0.85	0	(c)
VOC	0.85	0	(d)
CH4	0.91	0.2	(e)

Notes: (a) Mace-head correction applied on yearly basis to climatological values from 1990-current year, see section 10-1. (b) pre-1990 from Janach (1989); Low et al. (1990); Volz and Kley (1988); Bojkov (1986); Logan (1994) (c) Trend for CO of 0.85%/yr from Zander et al. (1989b); (d) Trend for ethane of 0.85%/yr from Ehhalt et al. (1991). Same trends assumed for n-butane and ethene. (e) Pre-1990 values from Zander et al. (1989a) for 1975-1990. Post-1990 values valid for 1990-2000, derived from Mace-Head observations.

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