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*Supplement of*

## **Vertical profile observations of water vapor deuterium excess in the lower troposphere**

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**Section S2.** Water vapor concentration-dependence calibration

**Section S3.** Water vapor  $\delta D$ ,  $\delta^{18}O$ , and d-excess error propagation

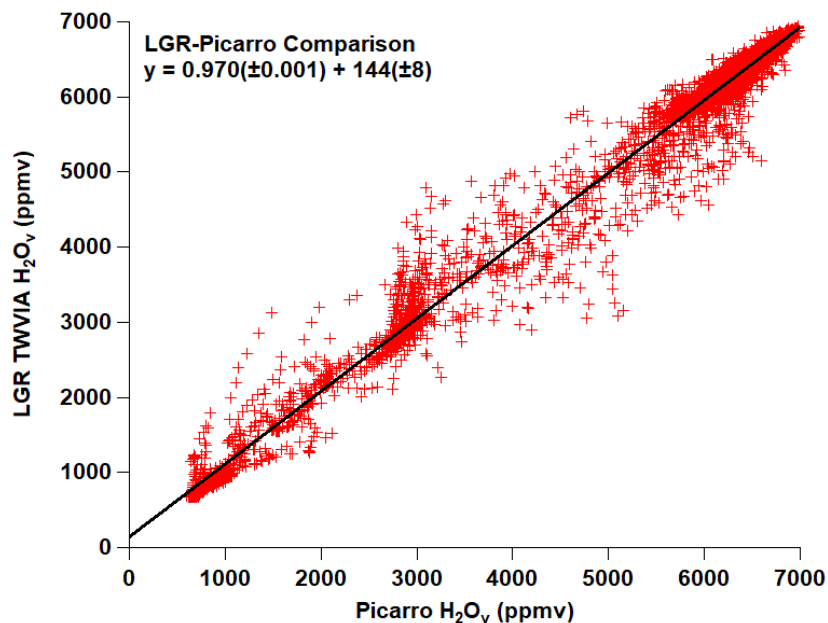
**Section S4.** Equilibrium fractionation factor method comparison

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## Section S1. Comparison of LGR and Picarro H<sub>2</sub>O<sub>v</sub> mole fraction



**Figure S1: Concentration-dependence calibrated H<sub>2</sub>O<sub>v</sub> mole fractions from the Los Gatos Research (LGR) Triple Water Vapor Isotope Analyzer (TWVIA) and the Picarro cavity ringdown spectrometer during the entire flight conducted on 6 March 2016 (CLR). The purpose of this plot is for measurement comparison only; it is not used to calibrate either H<sub>2</sub>O<sub>v</sub> data set.**

## Section S2. Water vapor concentration-dependence calibration

A Los Gatos Research (LGR) Water Vapor Isotope Standard Source (WVISS; model: 908-0004-9003) equipped with a secondary dry air mixing chamber for extended range operation was used to characterize the LGR Triple Water Vapor Isotope Analyzer's (TWVIA; model: 911-0034) non-linear response to water vapor ( $\text{H}_2\text{O}_v$ ) concentration (Rambo et al., 2011). The WVISS samples liquid water with a known isotopic composition from a reservoir. The standard sample is then nebulized using zero (dry) air into a heated chamber ( $75^\circ\text{C}$ ), where it evaporates completely and is further diluted with zero (dry) air with programmable flow rates to output a range of  $\text{H}_2\text{O}_v$  fractions with the same isotopic signature as the liquid standard. Different combinations of nebulizer sizes (flow rates) and standard versus extended range operation were required to span a large range of  $\text{H}_2\text{O}_v$  values. The TWVIA's  $\text{H}_2\text{O}_v$  dependence (while operating in extended range mode,  $\sim 80$  Torr) was evaluated over the range from 550 ppmv – 14,000 ppmv, consistent with range of  $\text{H}_2\text{O}_v$  mole fractions observed during the research flights (Table 1). Free troposphere  $\text{H}_2\text{O}_v$  mole fractions were sometimes less than 550 ppmv, but the lowest  $\text{H}_2\text{O}_v$  mole fraction the WVISS can produce is 500 ppmv. We found that stable flows of  $\text{H}_2\text{O}_v$  mole fractions lower than 550 ppmv were difficult to achieve with the WVISS, so we opt not to report  $\delta\text{D}$  and  $\delta^{18}\text{O}$  values corresponding to observed  $\text{H}_2\text{O}_v$  mole fractions below 550 ppmv. The  $\delta\text{D}$  and  $\delta^{18}\text{O}$  values of the  $\text{H}_2\text{O}_v$  isotope standards, which bracket the ranges observed during the research flights (Table 1), are listed in Table S2. The WVISS was programmed to sample each  $\text{H}_2\text{O}_v$  mole fraction for  $\geq 20$  min. The  $\delta\text{D}$  and  $\delta^{18}\text{O}$   $\text{H}_2\text{O}_v$  dependence calibration curves were constructed from the average  $\delta\text{D}$  and  $\delta^{18}\text{O}$  values reported during the last 200 s of each calibration period to remove any influence of transition instability caused by water moving onto and off of the walls of the system during the calibration  $\text{H}_2\text{O}_v$  step changes. The  $\delta^{18}\text{O}$  and  $\delta\text{D}$   $\text{H}_2\text{O}_v$  dependence curves shown in Fig. S2.1 and Fig. S2.2, respectively, were fit using the locally weighted polynomial regression “locpoly” function from R's “locfit” package (Bailey et al., 2015). A 100 ppmv sliding window was used for the local polynomial regression fitting over the range from 550 ppmv – 14,000 ppmv  $\text{H}_2\text{O}_v$ .

**Table S2: Calibration standards**

Standard*	$\delta\text{D}$ (‰)	$\delta^{18}\text{O}$ (‰)	d-excess (‰)
Purdue tap water	-39.9	-8.7	29.7
Boulder tap water	-117.3	-15.4	5.9
USGS-46	-235.8	-29.8	2.6
South Pole Glacier Water	-434.5	-54.3	-0.1
Custom Light Blend <sup>†</sup>	-573.7	-76.2	36.1

\*Standard values are reported relative to the VSMOW-SLAP scale

<sup>†</sup>The Custom Light Blend is a mixture of Purdue tap water, Sigma Aldrich deuterium depleted water ( $\leq 1$  ppm HDO), and Isotec 95%  $\text{H}_2^{18}\text{O}$  ( $^{18}\text{O}$ -enriched) to achieve a depleted isotopic signature that brackets the most depleted research flight observations of  $\delta\text{D}$  and  $\delta^{18}\text{O}$  that also has a realistic d-excess signature. Because the Custom Light Blend is isotopically more depleted than our standards, known amounts of the Custom Light Blend and Purdue tap water were combined to make three mixtures, which were analysed using an LGR liquid water isotope analyser (T-LWIA-45-EP; model: 912-0050-0001) to determine the Custom Light Blend's isotopic signature.

The TWVIA's  $\text{H}_2\text{O}_v$  dependence curve was reproducible over all  $\delta^{18}\text{O}$  isotope standard signatures considered (Table S2). The  $\delta\text{D}-\text{H}_2\text{O}_v$  dependence curve was reproducible for the three relatively enriched isotope standards, more enriched than  $-235.8\text{‰}$  in Table S2, but was not always reproducible using the most depleted standards (South Pole Glacier and Custom Light Blend) over the  $\text{H}_2\text{O}_v$  range of  $\sim 3000$  ppmv to  $\sim 8000$  ppmv (Fig. S2.1a and Fig. S2.2a). At  $\text{H}_2\text{O}_v$  mole fractions outside that range, the calibration curve remained reproducible. The cause of the  $3000$  ppmv –  $8000$  ppmv irreproducibility of the  $\delta\text{D}-\text{H}_2\text{O}_v$  dependence curve associated with very depleted  $\delta\text{D}$  values remains unknown, perhaps small leaks in the experimental setup, uncertainty associated with curve fitting, or instrument biases or lower instrument precision for very depleted  $\delta\text{D}$  values. To our knowledge this behaviour has not been described in the literature. However,  $\delta\text{D}$  values consistent with the two most depleted standards (Table S2) were only observed in the free troposphere. These correspond to low  $\text{H}_2\text{O}_v$  mole fractions ( $<1000$  ppmv) and were outside of the irreproducible window of  $\text{H}_2\text{O}_v$  values. Therefore, it was not consequential to actual flight observations in this experiment. We note that there also appears to be large variability in the TWVIA-reported  $\delta\text{D}$  values  $<1000$  ppmv  $\text{H}_2\text{O}_v$  for the two depleted standards, but there is also relatively larger variability in this  $\text{H}_2\text{O}_v$  range for the enriched standards as well. To avoid biases resulting from the depleted  $\delta\text{D}$  irreproducibility, the  $\delta\text{D}$  water vapor dependence curve is defined using calibration data from the three relatively enriched standards. However,  $\delta\text{D}$  calibration data from each of the five standards is used to define uncertainties (see below in Section S3).

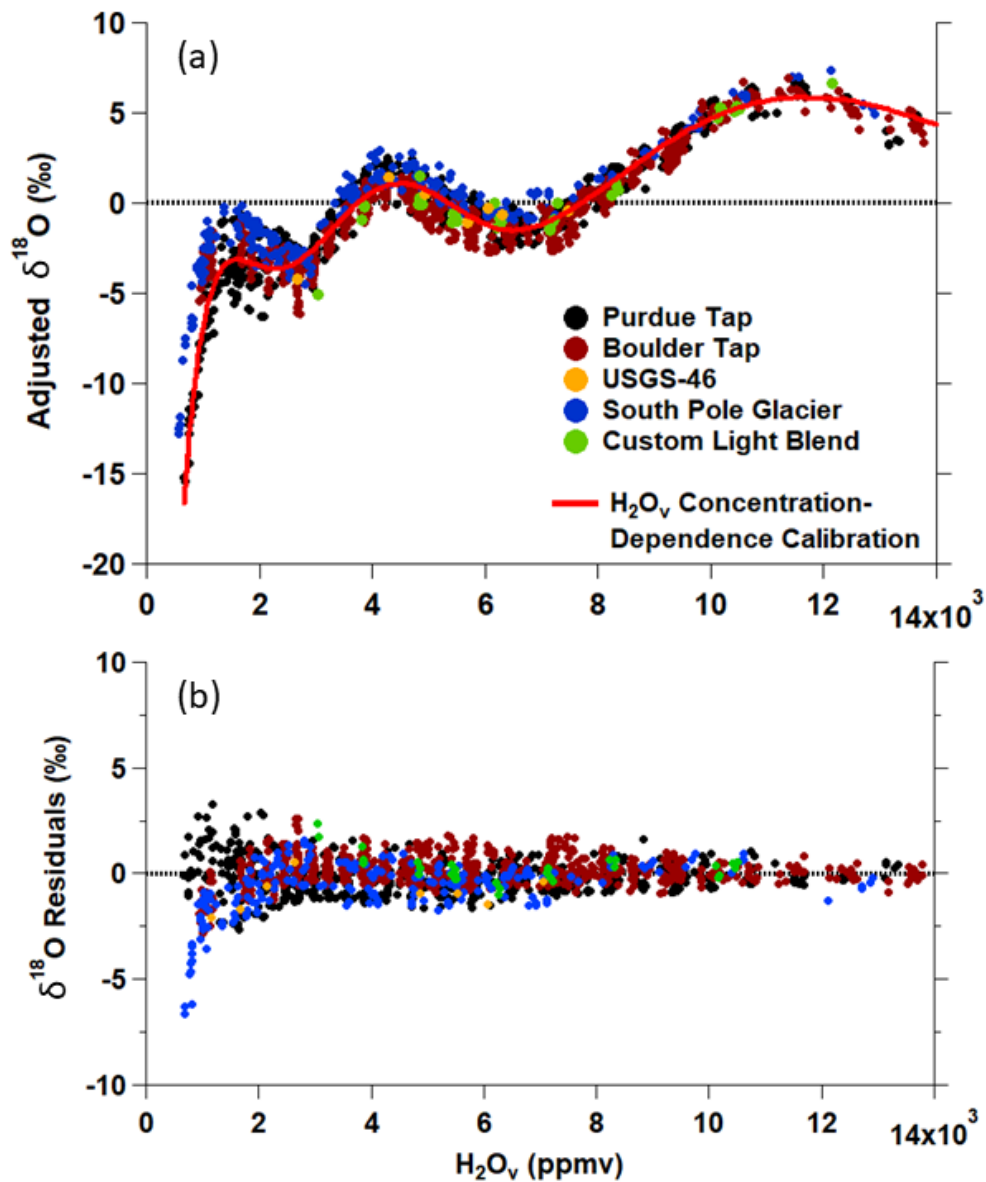
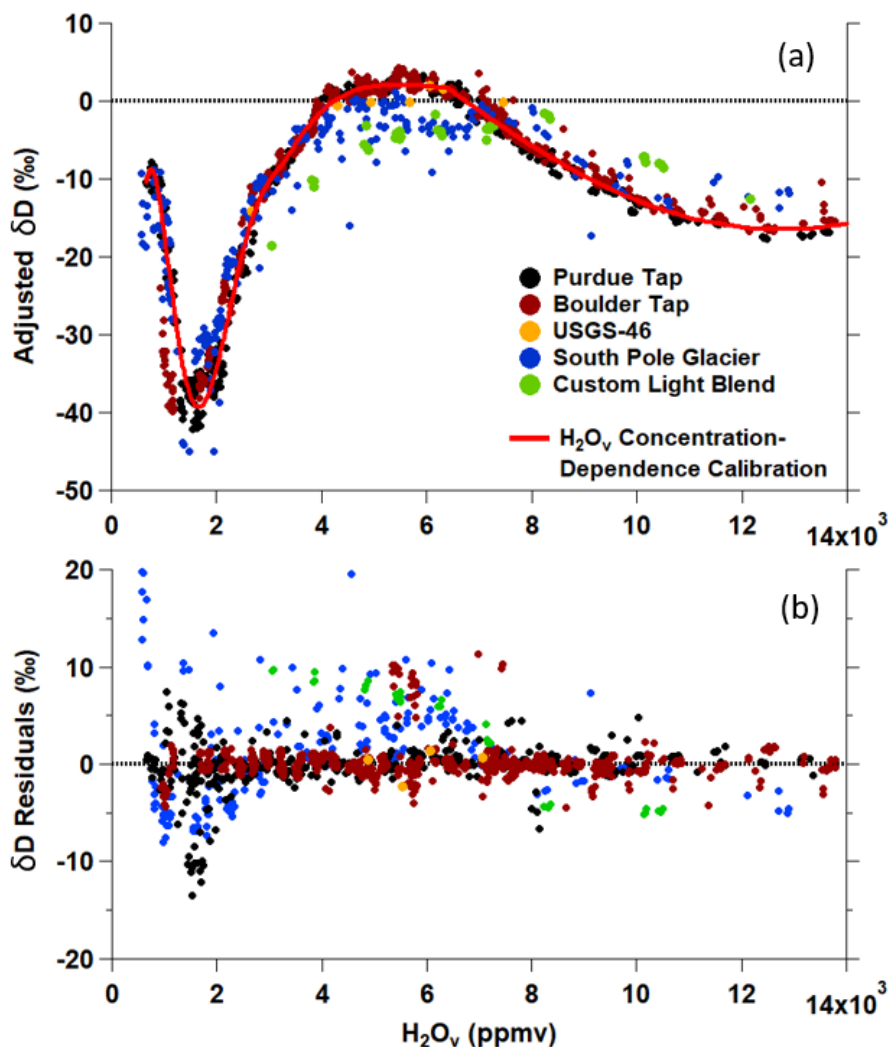


Figure S2.1:  $\delta^{18}O$ - $H_2O_v$  dependence (a) calibration curve and (b) residuals. The true  $\delta^{18}O$  signature of each standard (Table S2) has been subtracted from the TWVIA measurements to give the “adjusted”  $\delta^{18}O$  signature in (a). Residuals are calculated by subtracting points along the  $H_2O_v$  dependence curve from the measured calibration data points.



**Figure S2.2:  $\delta D$ - $H_2O_v$  dependence (a) calibration curve and (b) residuals. The true  $\delta D$  signature of each standard (Table S2) has been subtracted from the measurements to give the “adjusted”  $\delta D$  signature in (a). Residuals are calculated by subtracting points along the  $H_2O_v$  dependence curve from the measured calibration data points.**

The linear regressions of the isotope standards’  $H_2O_v$  concentration-dependence corrected  $\delta$  values versus true gas phase isotopic signature for  $\delta^{18}O$  and  $\delta D$  have slopes near unity and intercepts near zero (Fig. S2.3).  $\delta^{18}O$  had a slope of  $1.009(\pm 0.001)$ , a y-intercept of  $0.08(\pm 0.03)$ , and an  $R^2$  of 0.997254 (Fig. S2.3a). The  $\delta D$  ordinary least squares regression line had a slope of  $0.9954(\pm 0.0005)$ , a y-intercept of  $-0.5(\pm 0.09)$ , and an  $R^2$  of 0.99958 (Fig. S2.3b). A VSMOW-SLAP correction was not applied because it would be negligible compared to the uncertainty associated with the concentration-dependence correction and the instrument precision (Section S3).

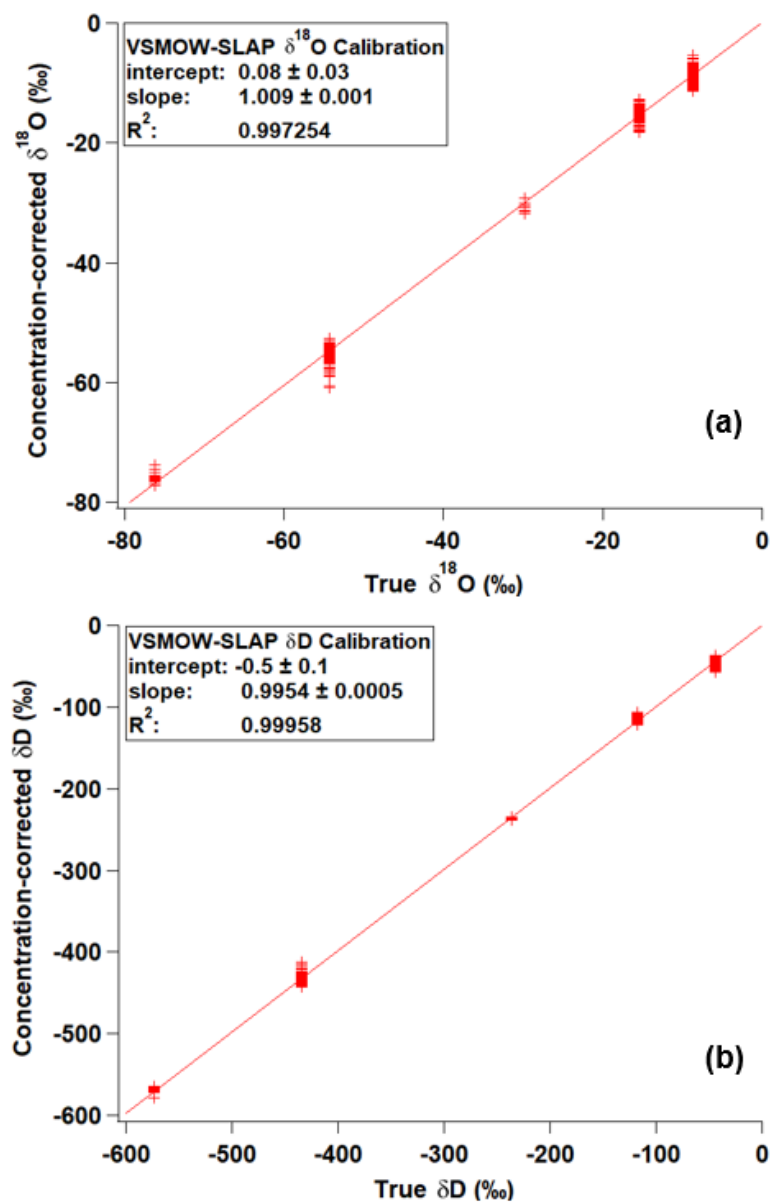


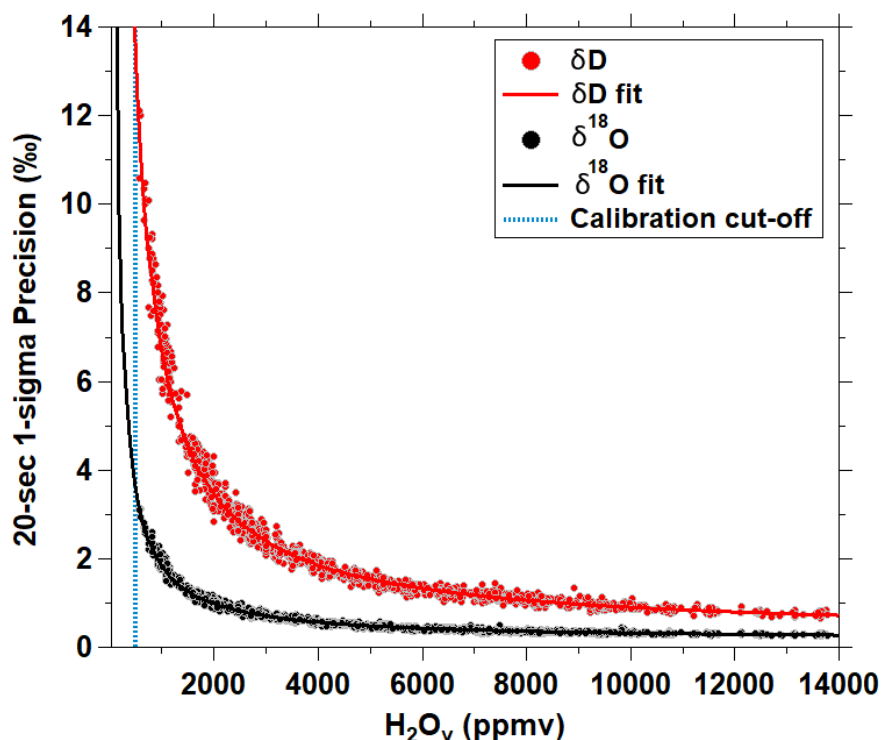
Figure S2.3. VSMOW-SLAP calibration curves for (a)  $\delta^{18}\text{O}$  and (b)  $\delta\text{D}$ .  $\text{H}_2\text{O}_v$ -concentration-corrected isotopic signatures are plotted against the standard's true isotopic signature. Linear regression fit slopes and intercepts are included in the figure insets.



### Section S3. Water vapor $\delta D$ , $\delta^{18}O$ , and d-excess error propagation

#### Instrument precision:

The TWVIA instrument precision was calculated as the  $1\sigma$  standard deviation for the last 20 seconds of every calibration period (Section S2). The interval used to smooth the  $\delta D$ ,  $\delta^{18}O$ , and d-excess values reported in this paper is 20 s, which corresponds to the time required for the TWVIA signal to stabilize after a change in the sample's  $H_2O_v$  mole fraction or isotopic signature. Power functions were fit to the  $\delta D$  and  $\delta^{18}O$  precision values from all the calibrations as a function of  $H_2O_v$  mole fraction (Fig. S3). Precision uncertainties for flight measurements were calculated using the measured  $H_2O_v$  mole fraction and the power fit functions.



**Figure S3: TWVIA  $\delta^{18}O$  and  $\delta D$  20-s instrument precision ( $1\sigma$ ) as a function of water vapor ( $H_2O_v$ ) mole fraction for all calibration data.**

#### $H_2O_v$ dependence calibration uncertainty:

The uncertainty associated with the TWVIA  $\delta D$ - and  $\delta^{18}O$ - $H_2O_v$  dependence corrections is determined from the calibration residuals shown in Fig. S2.1b and Fig. S2.2b. We note that the calibration residuals do include a small instrument precision component, as the calibration values are the average of 200 s sampling periods. The absolute value of the  $\delta D$  and  $\delta^{18}O$  residuals from all five reference waters tested were filtered into bins defined by 100 ppmv  $H_2O_v$  mole fraction increments. Averages of the absolute  $\delta D$  and  $\delta^{18}O$  residuals were calculated for each bin. For relatively dry conditions (i.e. below 3500

ppmv H<sub>2</sub>O<sub>v</sub>), the bin-averaged calibration residuals increase as H<sub>2</sub>O<sub>v</sub> mole fractions decrease. A best-fit linear regression was determined for the bin-averaged residuals as a function of H<sub>2</sub>O<sub>v</sub> mole fraction (from 550 – 3500 ppmv for δD and 550 – 3700 ppmv for δ<sup>18</sup>O). Bin-averaged residuals were relatively constant for H<sub>2</sub>O<sub>v</sub> mole fractions greater than 3500 ppmv for δD and 3700 ppmv for δ<sup>18</sup>O. Average H<sub>2</sub>O<sub>v</sub> dependence calibration uncertainties of 1.8‰ for δD and 0.9‰ for δ<sup>18</sup>O were calculated from the bin-averaged residuals from 3500 – 14000 ppmv for δD and 3700 – 14000 ppmv for δ<sup>18</sup>O. Higher uncertainties in the δ values at low H<sub>2</sub>O<sub>v</sub> mole fractions is not surprising, as the manufacturer suggests the TWVIA be used for sampling air ranging from 4,000 – 60,000 ppmv H<sub>2</sub>O<sub>v</sub>.

**Total uncertainty:**

Total δD and δ<sup>18</sup>O uncertainty is calculated by propagating the error resulting from instrument precision,  $S_{precision}$ , and from the H<sub>2</sub>O<sub>v</sub> concentration-dependence calibration,  $S_{calibration}$ , as in eq. (S3.1):

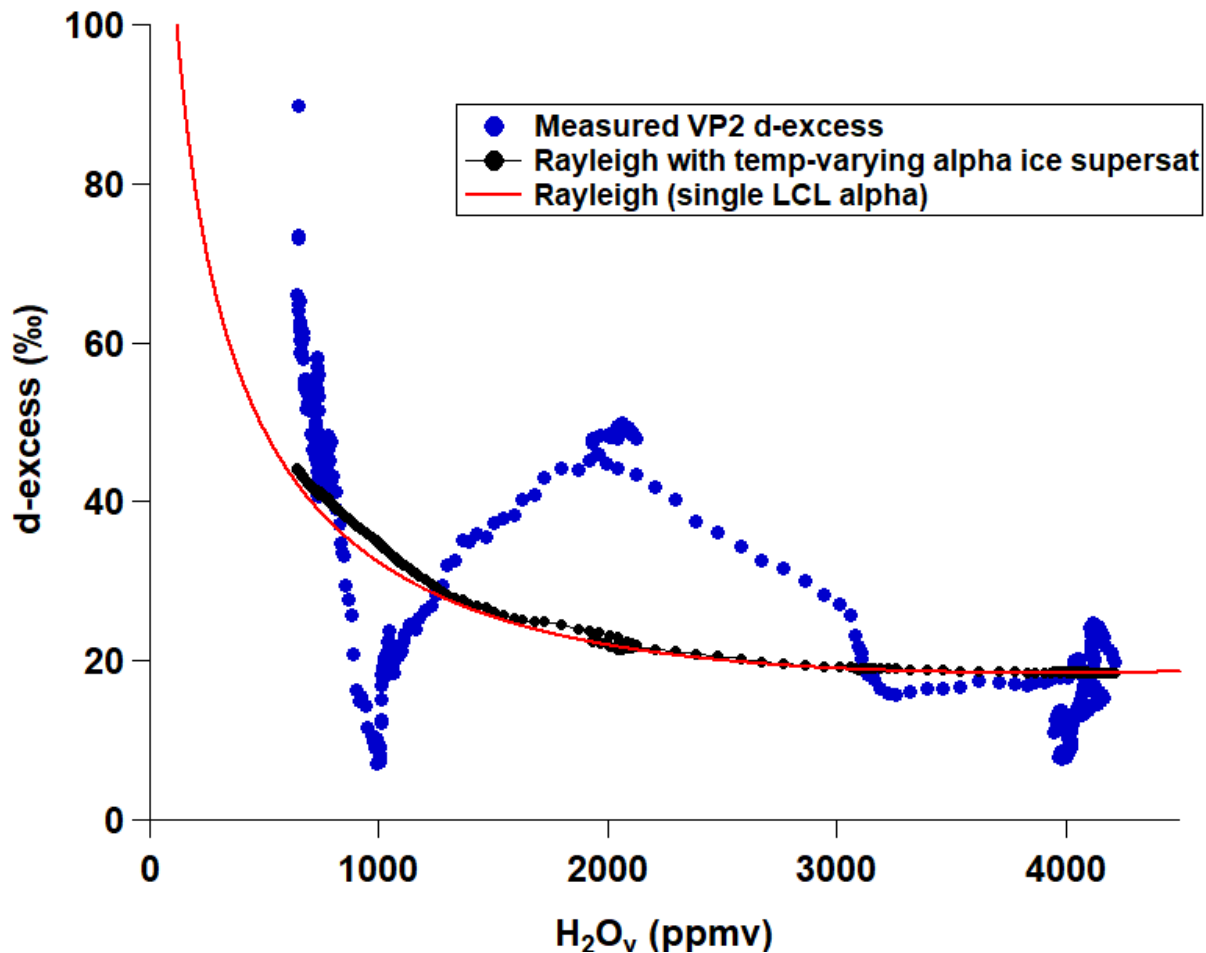
$$S_{total} = \sqrt{S_{precision}^2 + S_{calibration}^2}. \quad (S3.1)$$

The total d-excess uncertainty is determined according to eq. (S3.2):

$$S_{total,d-excess} = \sqrt{S_{total,\delta D}^2 + 8 \times (S_{total,\delta^{18}O}^2)}, \quad (S3.2)$$

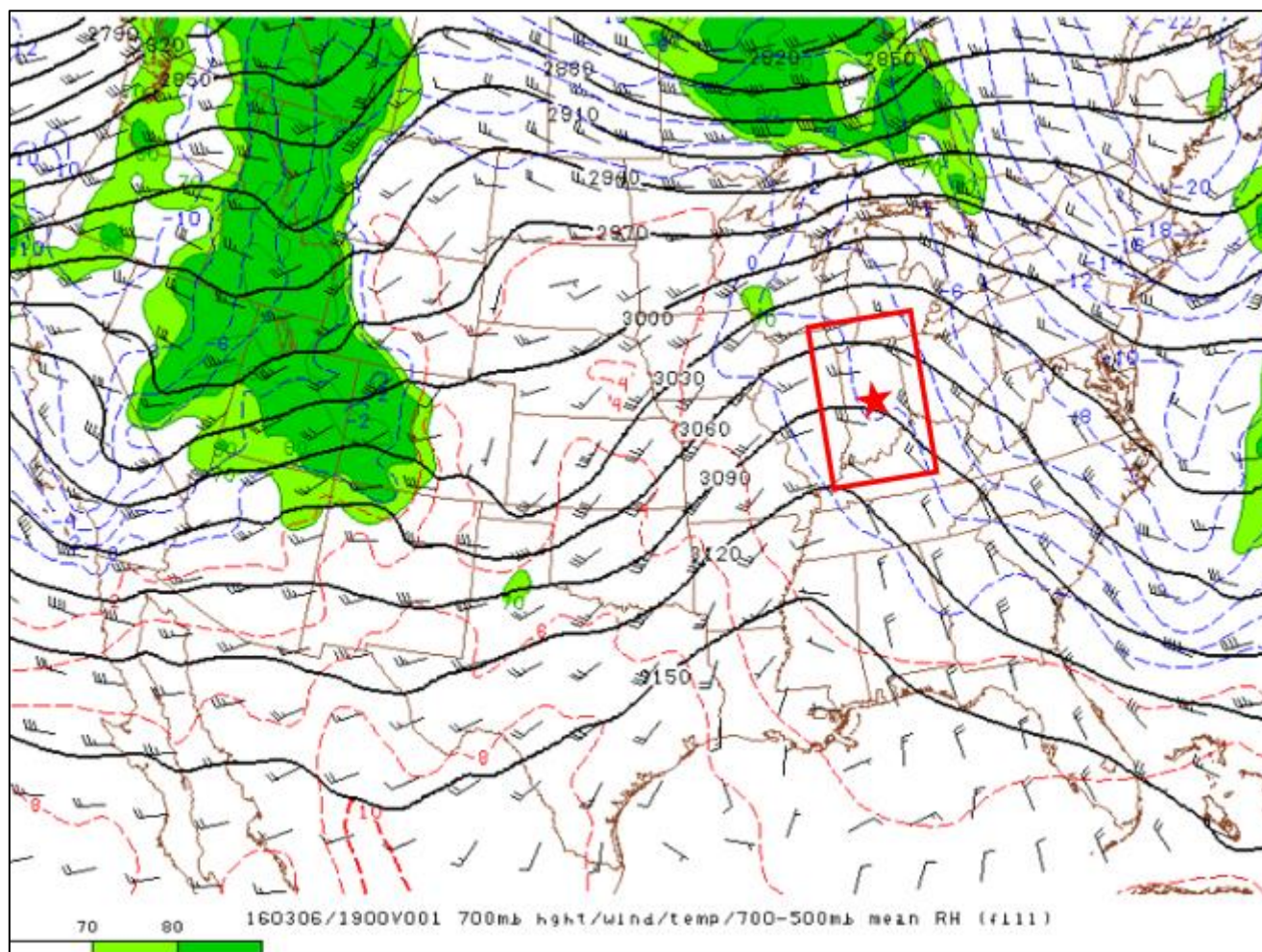
where  $S_{total,\delta D}$  and  $S_{total,\delta^{18}O}$  are the total δD and δ<sup>18</sup>O uncertainties (given by eq. (S3.1)). The total uncertainty for δD, δ<sup>18</sup>O, and d-excess as functions of H<sub>2</sub>O<sub>v</sub> mole fraction are presented in Fig. 1.

Section S4. Rayleigh distillation equilibrium fractionation factor method comparison



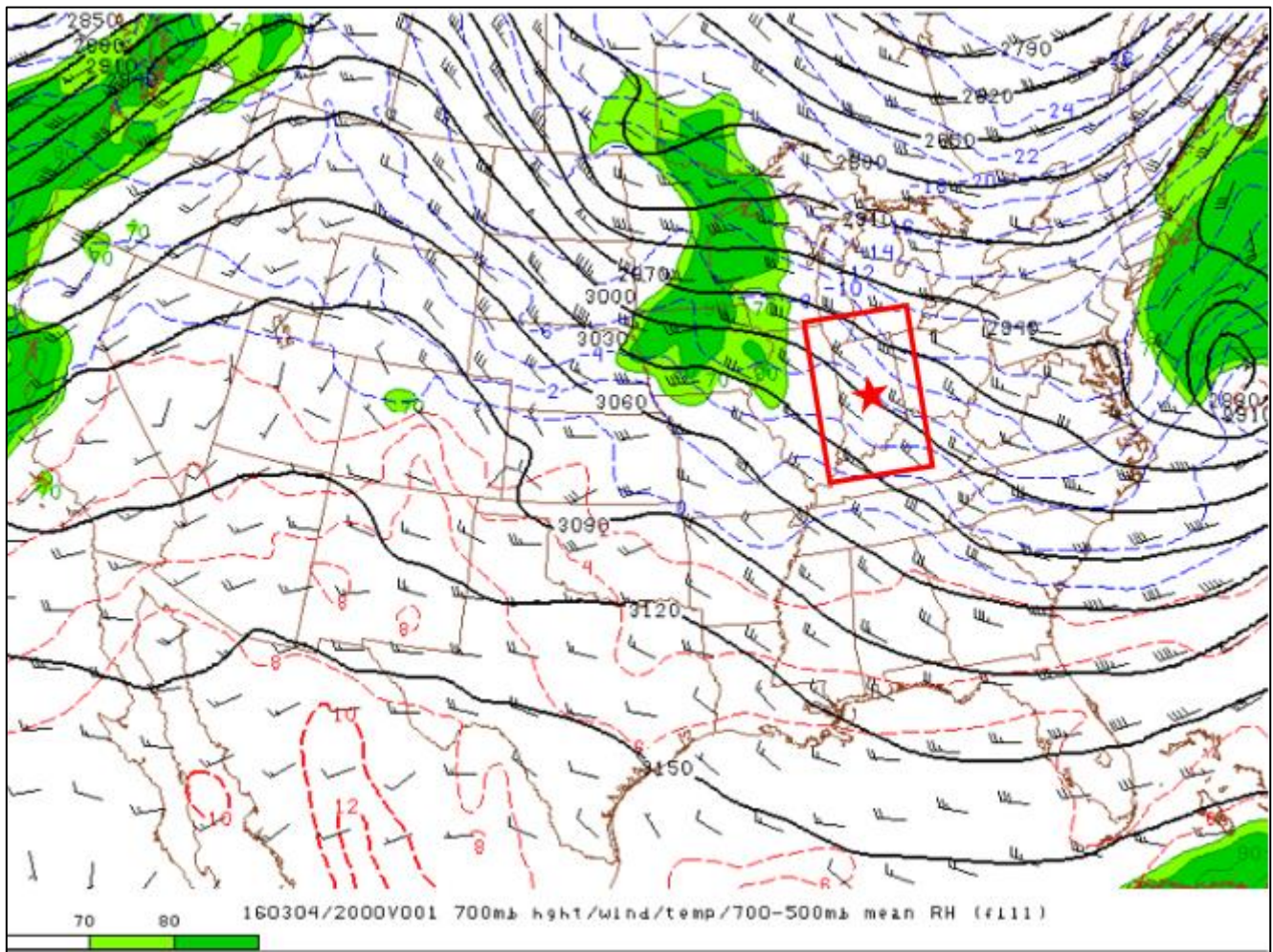
**Figure S4.** Comparison of Rayleigh distillation curves calculated using a single fractionation factor ( $\alpha$ ) defined by the temperature at the lifting condensation level (LCL =  $-6.0^{\circ}\text{C}$ ) and temperature-varying  $\alpha$  values. The Rayleigh curve comparison is shown for altitude-varying temperatures, ranging from  $-0.9^{\circ}\text{C}$  –  $4.1^{\circ}\text{C}$ , measured along the second vertical profile (VP2) conducted on the stratocumulus cloud (STC) case study.

## Section S5. Case study weather maps

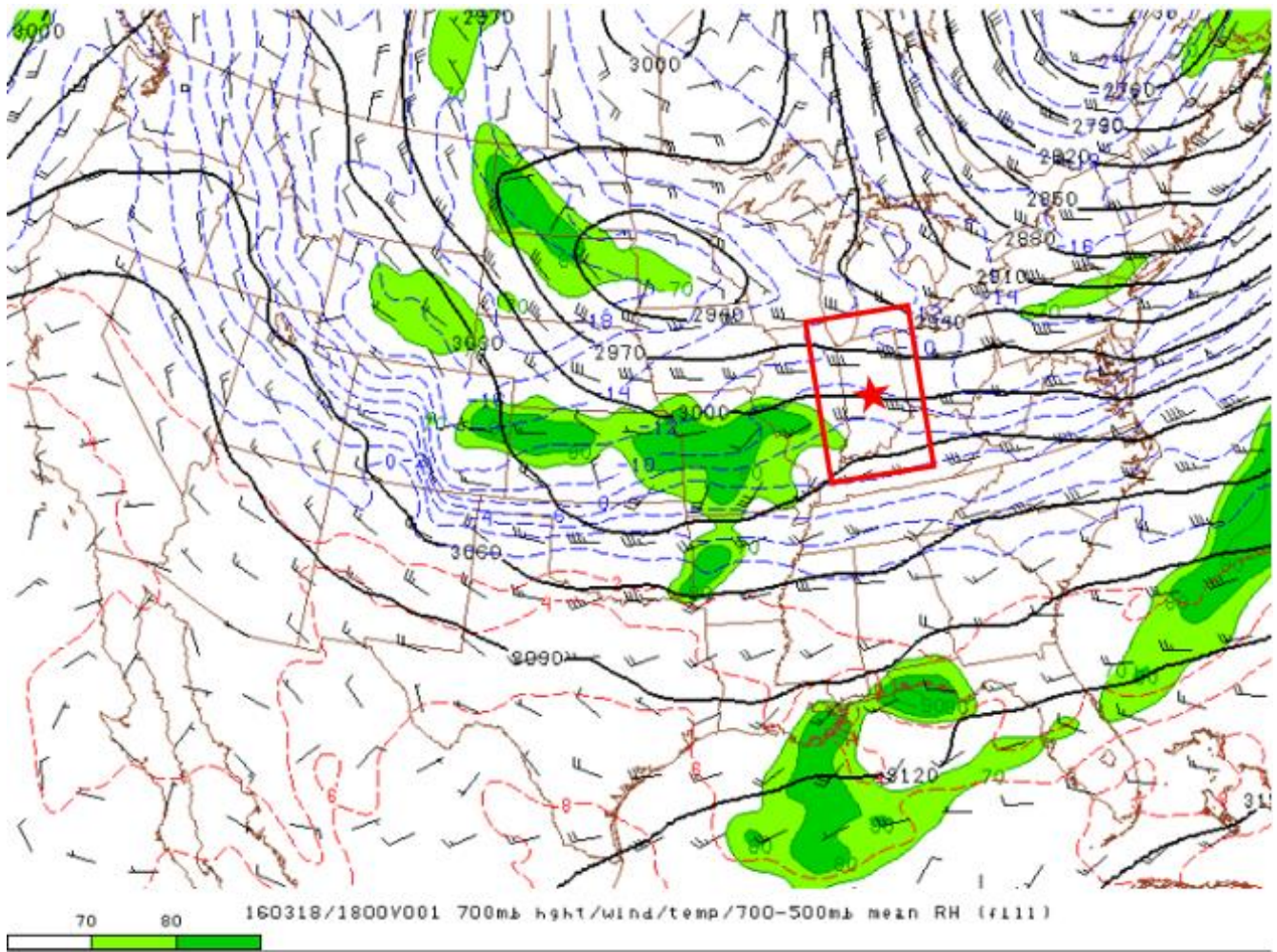


**Figure S5.1.** Weather map of mid-troposphere (3-5.5 km) relative humidity on the CLR case study day (6 March 2016) at 14:00 local time (EST). Figure S5.1 shows that the mid-troposphere was relatively dry directly upwind of the Indianapolis study site. Indiana is outlined by a red box, and Indianapolis is indicated with a star. This weather map represents atmospheric conditions approximately halfway through the CLR flight. Map source:

[https://www.spc.noaa.gov/exper/ma\\_archive/](https://www.spc.noaa.gov/exper/ma_archive/).



**Figure S5.2.** Weather map of mid-troposphere (3-5.5 km) relative humidity on the STC case study day (4 March 2016) at 15:00 local time (EST). Figure S5.2 shows an atmosphere of >80% relative humidity (dark green coloring) upwind of the Indianapolis study site. Indiana is outlined by a red box, and Indianapolis is indicated with a star. This weather map represents atmospheric conditions approximately halfway through the STC flight. Map source: [https://www.spc.noaa.gov/exper/ma\\_archive/](https://www.spc.noaa.gov/exper/ma_archive/).



**Figure S5.3.** Weather map of mid-troposphere (3-5.5 km) relative humidity on the DBL case study day (18 March 2016) at 14:00 local time (EDT). Figure S5.3 shows moistening ahead of a shortwave trough. Indiana is outlined by a red box, and Indianapolis is indicated with a star. The dark green coloring shows relative humidity greater than 80%. This weather map supports observations of elevated  $\text{H}_2\text{O}_v$  mole fraction in the free troposphere during the fourth vertical profile (VP4) on DBL. Map source: [https://www.spc.noaa.gov/exper/ma\\_archive/](https://www.spc.noaa.gov/exper/ma_archive/).

## Section S6. Fractionation of water vapor in ice supersaturated conditions

$\text{H}_2\text{O}_v$  undergoing deposition on ice crystals is impacted by equilibrium and kinetic fractionation. The kinetic fractionation factor is calculated via Galewsky (2015) eq. (S6.1):

$$\alpha_{ice,k} = \frac{S_i}{\alpha_e \frac{D}{D'} (S_i - 1) + 1}, \quad (\text{S6.1})$$

where  $S_i$  is saturation with respect to ice, expressed as a fraction. The equilibrium fractionation factor,  $\alpha_e$ , is calculated for the temperature at the lifting condensation level (LCL) and is discussed in Methods 2.5. The ratio of the molecular diffusivity of the light to heavy isotopologue,  $\frac{D}{D'}$ , is 1.02849 for  $^{18}\text{O}$  and 1.02512 for D (Merlivat, 1978).

The isotopic signature of an air parcel in ice supersaturated conditions ( $R_{S_i}$ ) can be calculated according to eq. (S6.2):

$$R_{S_i} = R_o \left( \frac{H_2O_v}{H_2O_{v_o}} \right)^{\alpha_{ice,k} \alpha_e^{-1}} \quad (\text{S6.2})$$

$R_o$  is the heavy to light isotopologue ratio ( $\frac{HDO_v}{H_2O_v}$  or  $\frac{H_2^{18}O_v}{H_2O_v}$ ) of the parcel prior to the ascent. The remaining fraction of  $\text{H}_2\text{O}_v$  left in the ascending parcel relative to initial conditions is given by  $\frac{H_2O_v}{H_2O_{v_o}}$ .

Figure S6 shows the STC VP d-excess observations along with Rayleigh vapor calculated from  $\text{RH} = 100\%$  (Methods 2.5) and vapor in ice supersaturated conditions (eq. (S6.2)). To match the most negative d-excess value observed at the top of the INV on STC, a supersaturation ( $S_i$ ) of 1.17 ( $\text{RH}_i = 117\%$  in Fig. S6) was used but does not necessarily reflect reality for the temperature or altitude of the observations. The Rayleigh curve is presented for reference.

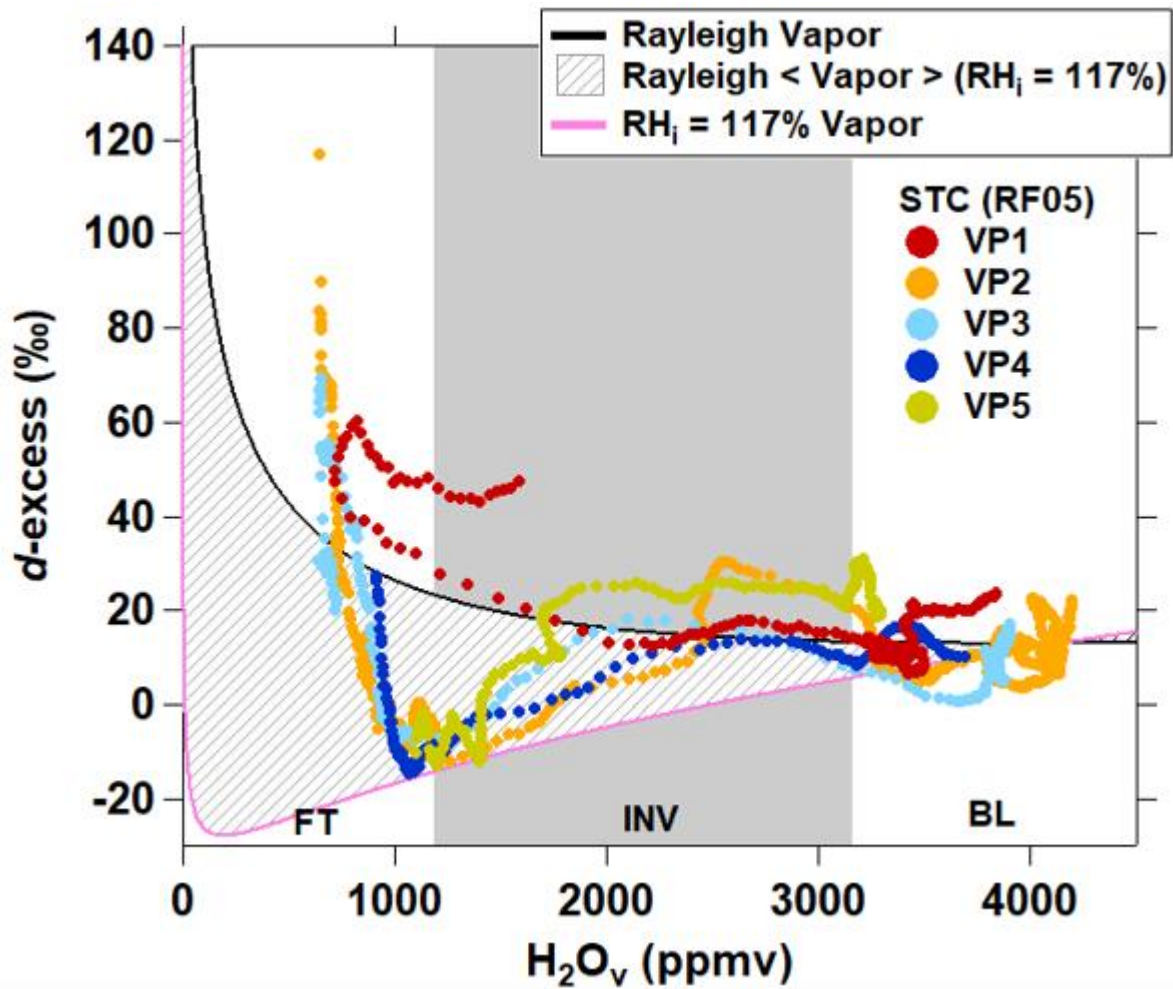
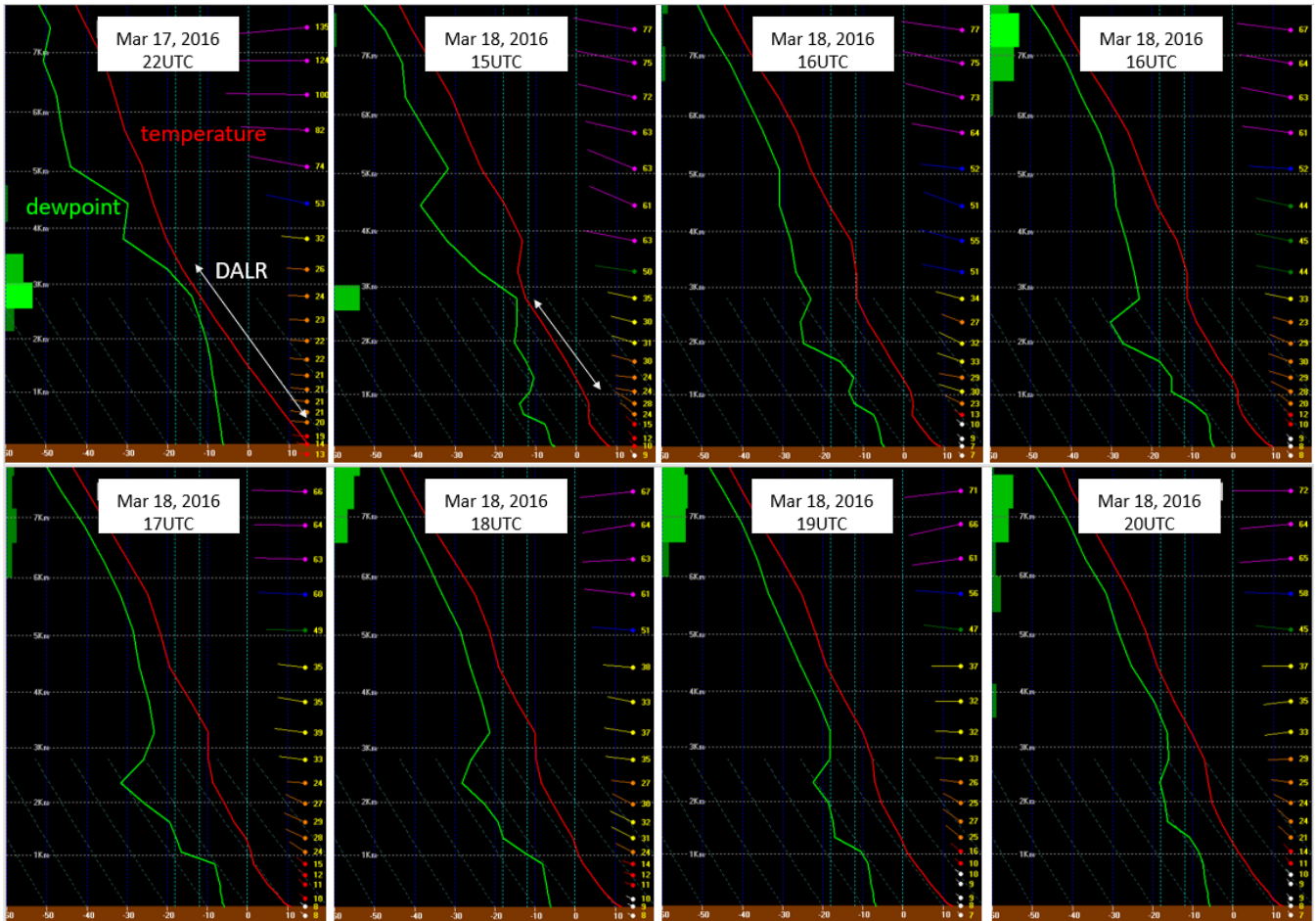


Figure S6: STC VP d-excess observations, Rayleigh vapor d-excess, and calculated d-excess of vapor in ice supersaturated ( $RH_i$ ) conditions up to  $RH_i = 117\%$ . Ice supersaturated conditions were chosen merely to match the INV-FT interface d-excess observations, and do not necessarily reflect a realistic  $RH_i$  for the STC flight day. The region indicated by the slanted lines describes the Rayleigh-predicted d-excess values under conditions spanning 100% RH over liquid to 117%  $RH_i$  over ice.



**Section S7. Indianapolis International Airport (KIND) temperature and dewpoint profiles preceding and during DBL observations**



**Figure S7. Rapid Refresh (RAP) Model ambient temperature and dewpoint profiles for the Indianapolis International Airport (KIND) from 22:00 EDT on 17 March 2018 (MAR17; Table 1) and 11:00 – 17:00 EDT on 18 March 2016 (MAR18-DBL; Table 1). The progression of figures shows a near dry adiabatic lapse rate (DALR; white line) persisted from 17 March 2018 into the afternoon of 18 March 2018. With time, the 17 March 2018 residual layer (with nearly a DALR) is incorporated into the 18 March 2018 boundary layer.**