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Supplement of

Interpretation of $NO_3-N_2O_5$ observation via steady state in high-aerosol air mass: the impact of equilibrium coefficient in ambient conditions

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S1. Ambient case invalid for NO₃-N₂O₅ steady state analysis

Take two typical cases in winter and summer respectively for example to illustrate the conditions under which steady state analysis is invalid for interpreting NO_3 - N_2O_5 observation and deriving $\gamma(N_2O_5)$. Over the period of wintertime case shown in Figure S1, the NOx and Sa concentration were low, indicating a clean episode. The $\gamma(N_2O_5)$ and kNO_3 can be determined from the intercept and slope respectively by linear fit based on steady state equation Eq. (5). The details and derivation of this approach are provided in introduction and method section. Albeit the correlation coefficient for deriving $\gamma(N_2O_5)$ by steady state approximation appears to be high, an unreasonably negative kNO_3 value derived during this analysis period (Figure S1d) indicates that the steady state in this case still requires much longer induction time due to low strength of NO_3 - N_2O_5 sink. In summertime case, although large sink rate contributed to fast approach of steady state, frequent injection of NO_3 emission could significantly modify the air mass condition. The time for mixing and reacting was still less than enough as emissions deviates the air mass from steady state (Figure S1e-S1g), leading to weak correlation factors (Figure S1h).

S2. Observation datasets from field campaigns 2017PKU and 2018TZ

The datasets used for analysis in this study were obtained from two field campaigns with different ambient conditions. The PKU2017 winter campaign took place from mid-November to late-December 2017 in the campus of Peking University, which is at urban area of Beijing, China. And the other one TZ2018 summer campaign took place from late-May to mid-June 2018 at a suburban supersite, Taizhou, China. More specific information about these two campaigns can be referred to our previous studies (Ma et al., 2019; Wang et al., 2020), while only basic background of site location and analysis-relevant instrumentation are provided below.

During the PKU2017 campaign, all instruments were applied on the roof of building in the campus of Peking University, which was about 100 m west to the major roads with strong influence of vehicle emissions. Each sampling inlet was distributed at least 20 m above the ground. The strong northerly winds with dry and clean air mass during the winter would periodically transport to this site, bring in fresh O₃ at night. The TZ2018 site is surrounded by agricultural land and fishponds, resulted in strong influence of biogenic emissions and occasional biomass burning. Each sampling inlet was distributed about 5 m above the ground. It should be noted that low concentration level of NO was frequently observed at this site due to a major highway within 0.5 km.

Same instrumentation was implemented in these two campaigns, and the related information are given in Table S1. We adjusted the nighttime NO concentration near the detection limit to zero during the periods with O3 concentration higher than 25 ppbv, as the lifetime of NO would be extremely short at night under this condition and the NO measurement at the low level usually has large uncertainty.

S3. Characteristic of nighttime NO₃-N₂O₅ loss pathway in half-artificial dataset

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The validity of NO₃-N₂O₅ steady state depends on their atmospheric lifetime, in other words their loss rate constants (Brown et al., 2003). In different seasons or areas, variations of emission, temperature, and other relevant factors can sufficiently change the sink strength of ambient NO₃ and N₂O₅ and thus relative occupations of these pathways. As half-artificial datasets (detailed in Methods) indicated, the average nighttime loss rate of NO₃ and N₂O₅ at PKU site in winter were 41 pptv h⁻¹ and 195 pptv h⁻¹, whereas much higher rates were obtained at TZ2018 campaign with 451 pptv h⁻¹ for NO₃ and 390 pptv h⁻¹ for N₂O₅. Distinguished from a dominant sink rate of N₂O₅ in winter, total sink rate attribution shifted to NO₃ side in summer with significant larger sink strength than that in winter. The average proportions of NO₃ and N₂O₅ removal in each night is shown in Figure S2, where the nights with missing data represents that there is less than 15% valid data. Under the condition of approximate steady state, the sink flux contributed through N₂O₅ reaches up to 55~95% in wintertime campaign 2017PKU with an average higher than 80%, whilst it turns out to be less than 50%, even 5%, in 2018TZ summer campaign. Besides the different emission compositions at these two sites leading to significant distinction of removal attribution (strong biogenic emission at TZ site and high anthropogenic emission at PKU site), high temperature during summer facilitates the equilibrium in reactions R1 shifting to NO₃, further increasing the sink flux of NO₃. The attribution of removal pathways among NO₃ and N₂O₅ directly determines the weights of two terms on the right side of steady state expressions Eq. (4) and Eq. (5), contributing to assessing the impacts of several variables on steady state fitting among different reactivity conditions. Taking two typical cases from these two datasets for example, the N₂O₅ lifetime was about 20 minutes in winter (Figure S3(a)), while was largely reduced to 100 seconds for summertime case (Figure S3(c)). The steady state lifetime of N₂O₅ ($\tau_{SS}(N_2O_5) = \frac{[N_2O_5]}{k_{R1}[NO_2][O_3]}$) and calculated lifetime of N₂O₅ ($\tau_{calc}(N_2O_5) = (k_{N_2O_5} + \frac{k_{NO_3}}{K_{eq}[NO_2]})^{-1}$) were used for determine whether the situation had satisfied steady state (see details in methods section). Significantly different atmospheric lifetime for these two cases was majorly resulted from varying uptake

removal pathways instead of kNO₃ from gas-phase reactions. Higher humidity at TZ site during nights facilitated hygroscopic growth of particles, the Sa concentration of which usually increased up to thousands of µm² cm⁻³ promoting the uptake reactions of NO₃ and N₂O₅, whereas Sa in the PKU site case become lower than 500 µm² cm⁻³ under the impact of clean and dry air mass. The steady state lifetime denoted by blue dash line in Figure S3(a)&(c), shows good agreement with atmospheric lifetime in both of cases, indicating that the NO₃-N₂O₅ chemical system simulated by steady state model is validated to be approximate steady state (deviation <5%). However, even in these cases, the derived uptake coefficient of N₂O₅, $\gamma_{ss}(N_2O_5)$, through steady state fitting (Figure S3(b)&(d)) still have a significant bias (>20%) from the setting values 0.02. Furthermore, we found that unexpected difference between $\gamma_{ss}(N_2O_5)$ fitting results and $\gamma(N_2O_5)$ setting values is common for all selected steady state periods in datasets. Since the influence of covariance of Sa and $Keq \times [NO_2]$ has been avoided by applying Eq. (5) (Brown et al., 2009), the bias of $\gamma_{ss}(N_2O_5)$ presented in the above fitting calculation could be produced by interaction between equilibrium and steady state, variation of relevant parameters in the fitting equations (such as kNO_3 , kN_2O_5 , etc), which are discussed in the main text.

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S4. Parameterization of Keg coefficient in different databases

Keq of NO₃-N₂O₅ system is a temperature dependent parameter, which has been extensively quantified in the laboratory (Pritchard, 1994). According to simultaneous measurements of N₂O₅, NO₃ and NO₂ concentration in a reaction chamber, the Keq can be directly calculated (Cantrell et al., 1988;Graham and Johnston, 1978;Osthoff et al., 2007), while the measurements of k_{R1a} and k_{R1b} or other accompanied parameters provides indirect ways to quantify Keq (Cantrell et al., 1993;Kircher et al., 1984;Smith and Ravishankara, 1985). However, distinct differences arise from these Keq results, which might be ascribed to the calibration uncertainty of absorption cross sections of NO₃ and NO₂ molecule (Osthoff et al., 2007). Jet Propulsion Laboratory (JPL) database provides an empirical formula, similar with Arenius formula, to calculate Keq in a simple way:

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$$K_{eq}(JPL) = A \times \exp(B/T),$$
 (S1)

Here T denotes ambient temperature, and coefficients A and B are empirical parameter derived from laboratory works. Nevertheless, only parameterizations of k_{R1a} and k_{R1b} based on fall-off curve are described in IUPAC database and most of chemical mechanisms, without a direct formula to estimate Keq value. To our best knowledge, only one previous study compared two of these parameterizations in terms of temperature dependence (Chang et al., 2011).

Here, a set of uniform formulas are applied to describing k_{R1a} and k_{R1b}, capable of reproducing the preferred values given by several popular atmospheric chemistry mechanisms (Mozart, CB05, Saprc07, RACM2 and kinetic databases JPL2015 as well as IUPAC2017) and finally calculating *K*eq. As shown in Eq. (S2) and Eq. (S3):

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$$k_{R1a}([M], T) = \left(\frac{k_o(T)[M]}{1 + \frac{k_o(T)[M]}{k_\infty(T)}}\right) \times F^{\left\{1 + \left[\frac{\log_{10}\left(\frac{k_o(T)[M]}{k_\infty(T)}\right)}{g}\right]^2\right\}^{-1}},$$
 (S2)

$$124 k_{R1b}([M],T) = \left(\frac{\frac{k_{o}(T)[M]e^{\frac{-B1}{T}}}{A}}{1 + \frac{k_{o}(T)[M]e^{\frac{-B1}{T}}}{k_{\infty}(T)e^{\frac{-B2}{T}}}}\right) \times F^{\left\{1 + \left[\frac{\log_{10}\left(\frac{k_{o}(T)[M]e^{\frac{-B1}{T}}}{-\frac{B2}{T}}\right)}{g}\right]^{2}\right\}^{-1}}, (S3)$$

The parameter [M] represent molecular density in ambient air. $k_o(T)$ and $k_\infty(T)$ are rate coefficients of third-body reactions under low and high pressure respectively, which over different temperatures can be extrapolated by Eq. (S4) and Eq. (S5) based on 300 K measurement or simulation results:

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$$k_o(T) = k_o^{300} \left(\frac{T}{300}\right)^{-n}$$
, (S4)

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$$k_{\infty}(T) = k_{\infty}^{300} \left(\frac{T}{300}\right)^{-m},$$
 (S5)

All parameters in the above formulas are summarized in Table S3 and Table S4, which can be applied to calculating Keq coefficient via k_{R1a}/k_{R1b} . We found that there are significant differences among the parameters from these chemical mechanisms and databases, with a maximum discrepancy of 63% propagating to Keq at 298 K.

S5. Sensitivity tests of time to approach steady state

In Figure S8 and Figure S9, a series of sensitivity test provide an assessment of the time a valid steady state needs under several conditions. The most sensitive variables to the time to reach a valid steady state are kN_2O_5 , kNO_3 and T, the enhancement of which reduces the induction time, facilitating the approach to valid steady state of NO_3 - N_2O_5 system. The time for a simulation of a particular case, starting from initialized conditions to meet the steady state criterion (detailed in the methods section), is defined as the time to reach a valid steady state. In the case of increasing kN_2O_5 and kNO_3 , the fast approaching to stead state is accounted by lower concentration of NO_3 and N_2O_5 when the steady state is valid. By comparing the sensitivity tests based on summertime (Figure S8(a)) and wintertime (Figure S8(b)) conditions, the impacts of kN_2O_5 on approaching steady state is found to be more efficient than that of kNO_3 in winter, while both contribute similarly in summer.

The different sensitivities to their reactivity in different seasons could be determined by the weights of loss pathways (Text S3). During the winter, such as the condition of PKU2017, the N₂O₅ usually accounted by over 80% of the overall loss frequency of NO₃-N₂O₅ system, leading to high sensitivity to kN_2O_5 , while comparable loss frequency was occupied by both of NO₃ and N₂O₅ during the summer. As for the temperature, lower temperature shifts the equilibrium in R1 to N₂O₅ side, which delay the time for developing equilibrium. By contrast, enhanced loss through NO₃ with higher ambient temperature decreases the influence of equilibrium, boosting the approach to steady state. Moreover, Figure S9 shows relatively weak sensitivity of NO₂ and O₃ concentration to steady state approach. While changing O₃ concentration barely contribute to promote a valid steady state in the scenario of this analysis, the NO₂ concentration shows a positive sensitivity in some cases. Like the ambient temperature, changing NO₂ concentration could shift the ratio of N₂O₅/NO₃ when steady state is valid and thus the time it requires. Especially under the condition of low ratio of NO₂ to O₃, like that in TZ2018, the enhancement of NO₂ concentration shift NO₃ to N₂O₅ production and amplify the influence of equilibrium reactions. Instead, with a sufficiently high ratio of NO₂/O₃, the loss associated with NO₃-N₂O₅ system has been already dominated by N₂O₅ removal,

eliminating the influence of NO₂ increase on delaying steady state. Previous research has also found similar trends of time to develop steady state according to simple scenarios simulated by box model (Brown et al., 2003).

S6. The impacts of kNO_3 and kN_2O_5 levels on $\gamma_{ss}(N_2O_5)$

In order to demonstrate the impacts of kNO₃ level on deriving $\gamma_{ss}(N_2O_5)$, another three half artificial data set are formulated through steady state model also based on the same observational constraints with kNO₃ levels increased to 3 times (Mod1), 6 times (Mod2) and 10 times (Mod3) respectively, while other parameters remained unchanged. Similarly, the steady state fitting is used to obtain $\gamma_{ss}(N_2O_5)$ for each 2-hour time-period as Mod0. The mean discrepancy from complete steady state of these time periods and the median deviation of derived $\gamma_{ss}(N_2O_5)$ from pre-set $\gamma(N_2O_5)$ are shown as solid circles and triangles in Figure S9. With the enhancement of kNO₃ constraints, $\gamma_{ss}(N_2O_5)$ deviation from true value increase dramatically, though the NO₃-N₂O₅ system behave generally closer to steady state. A larger deviation of $\gamma_{ss}(N_2O_5)$ will be yielded from linear fit at a higher kNO₃ level, while the relative varieties of kNO_3 stay the same. It indicates that the region with strong biogenic emissions is not suited to steady state fitting, such as TZ site, neither are the time periods with NO injection due to the resulted high reactivity and fast variation. Therefore, air mass with medium to low level of kNO₃ is required to produce accurate $\gamma_{ss}(N_2O_5)$ when applying stead state to analysis, like data sets of airborne or residual measurements (Brown et al., 2009; Brown et al., 2006; Morgan et al., 2015). Similarly, the influence of different levels of kN_2O_5 is also explored by adjusting the preset $\gamma(N_2O_5)$ or the Sa concentration constraint in the steady state model, as presented in the Figure S10(c)&(d). With the enhancement of kN_2O_5 level up to 5 times (Mod4), 12.5 times (Mod5) and 25 times (Mod6) of that in Mod0, the steady state approach can provide more reliable results of $\gamma_{ss}(N_2O_5)$, especially in the summer data set. This is because a large kN_2O_5

level contributes to approaching steady state, which instinctively attenuates the deviation of

fitting results produced by the small difference between both sides of Eq. (5).

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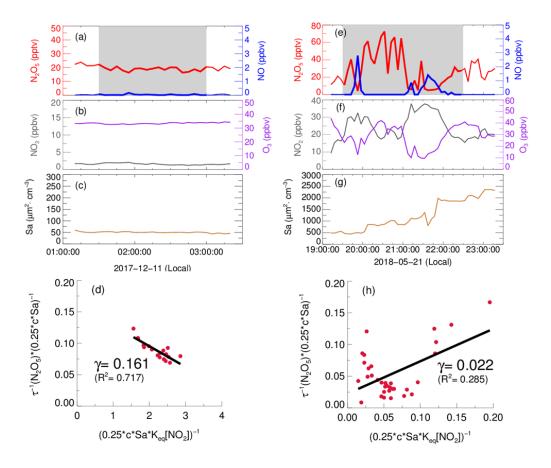


Figure S1. Exemplary steady state fit and the variations of relevant parameters in ambient conditions of (a)&(b)&(c)&(d) PKU site and (e)&(f)&(g)&(h) TZ site. The red dots in (d)&(h) represent the correlation plot between $(0.25cS_a\tau_{ss}(N_2O_5))^{-1}$ and $(0.25cS_aK_{eq}[NO_2])^{-1}$ used for deriving $\gamma(N_2O_5)$ and kNO_3 as illustrated in the method. The text on the plot gives the best fit results of $\gamma(N_2O_5)$ and correlation coefficient.

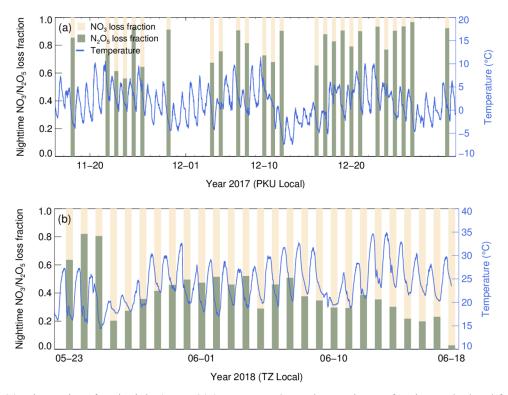


Figure S2. Timeseries of each night (SZA>90°) mean NO₃/N₂O₅ loss pathways fractions calculated from steady state model and ambient temperature in (a) PKU2017 winter campaign and (b) TZ2018 summer campaign.

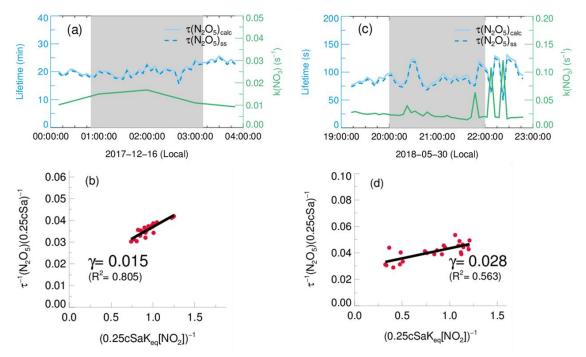


Figure S3. Example analysis of N₂O₅ lifetime and $\gamma_{ss}(N_2O_5)$ derivation through steady state fitting for (a)&(b) PKU2017 case in winter and (c)&(d) TZ2018 case in summer. The steady state lifetime and calculated atmospheric lifetime are shown as blue dash line and full line respectively. The green line is lumped NO₃ loss frequency. The red dots in (b)&(d) represent data points in the shadow area, used for steady state fit (black line) by the plot of $(0.25cS_a\tau_{ss}(N_2O_5))^{-1}$ against $(0.25cS_aK_{eq}[NO_2])^{-1}$. The text on the plot gives the best fit results of $\gamma_{ss}(N_2O_5)$ and correlation coefficient.

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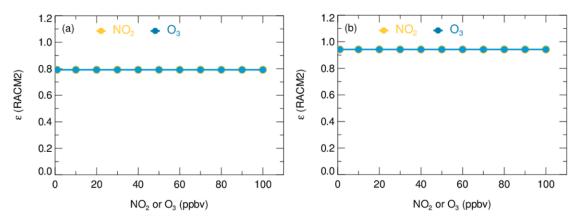


Figure S4. Sensitivity plot of NO₂ and O₃ concentration against coefficient ε calculated based on rate constants from RACM2. (a) Initial model constraint is according to winter condition of PKU2017; (b) Initial model constraint is according to summer condition of TZ2018.

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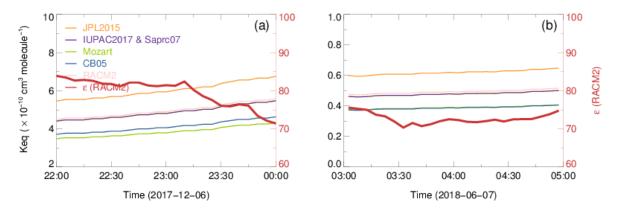


Figure S5. Exemplary comparison of Keq parameterization in (a) 2017-12-06 of PKU2017 dataset and (b) 2018-06-07 of TZ2018 dataset, using parameters from JPL2015 (orange), IUPAC2017&Saprc07 (purple), Mozart (green), CB05 (blue) and RACM2 (pink). It should be noted that the databases of Saprc07 and IUPAC2017 have the exactly same parameters, Keq derived from which are thus both denoted as purple line. The ε value calculated based on RACM2 is shown as red line.

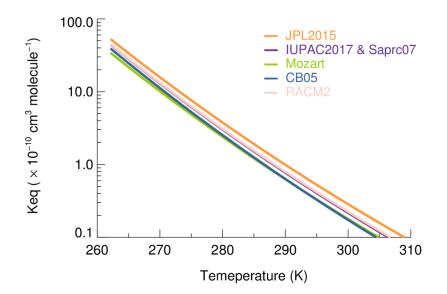


Figure S6. The dependence of different *K*eq parameterizations on temperature.

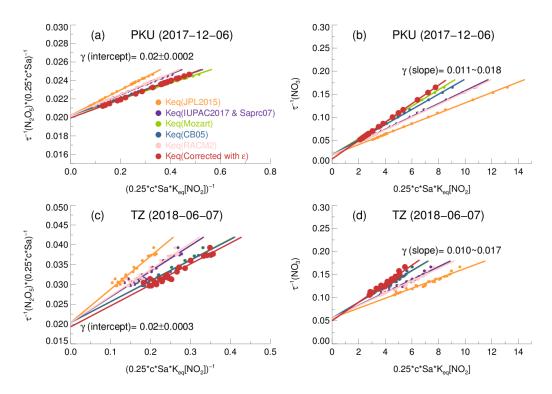


Figure S7. Exemplary fitting plot according to steady state approximation Eq. (1) (a)&(c) and Eq. (2) (b)&(d), using Keq parameterization of JPL2015 (orange), IUPAC2017&Saprc07 (purple), Mozart (green), CB05 (blue) and RACM2 (pink). The Keq (corrected by ε) is derived from output of steady state model coupled with RACM2. The values of derived $\gamma(N_2O_5)$ by intercept or slope are shown in text in the figures.

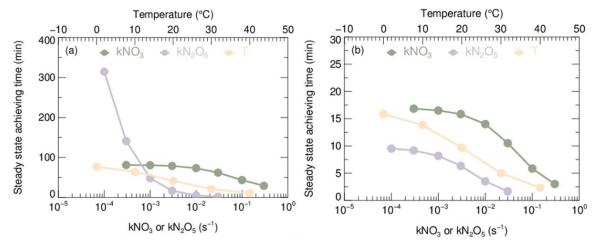


Figure S8. Sensitivity plot of kNO_3 , kN_2O_5 and T against steady state achieving time of NO_3 - N_2O_5 system. The trace of T is plotted against the upper horizontal axis and the traces of the other two parameters are plotted against the lower horizontal axis. (a) Initial model constraint is according to winter condition of PKU2017; (b) Initial model constraint is according to summer condition of TZ2018.

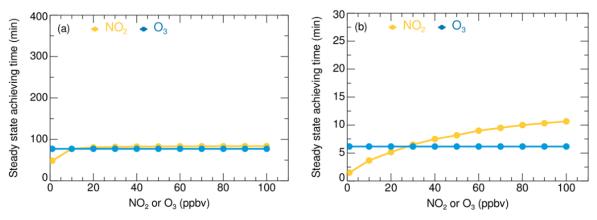


Figure S9. Sensitivity plot of NO₂ and O₃ concentration against steady state achieving time of NO₃-N₂O₅ system. (a) Initial model constraint is according to winter condition of PKU2017; (b) Initial model constraint is according to summer condition of TZ2018.

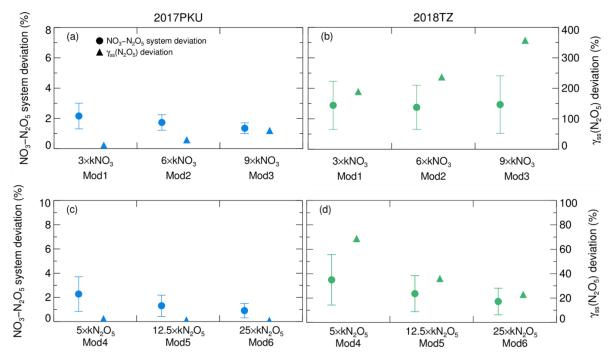


Figure S10. The average of NO₃-N₂O₅ system deviating from steady state and the median value of $\gamma_{ss}(N_2O_5)$ deviating from true value determined from different model constraints based on (a)&(c) PKU2017 dataset in blue and (b)&(d) TZ2018 dataset in green. The full circles represent the average of NO₃-N₂O₅ system deviating from steady state and the triangles represent the median deviation of $\gamma_{ss}(N_2O_5)$. As indicated in the text, the kNO₃ of Mod1, Mod2 and Mod3 are multiplied by 3,6 and 10 respectively against Mod0, and the kN₂O₅ of Mod4, Mod5 and Mod6 are multiplied by 5, 12.5 and 25 respectively against Mod0.

Table S1. Principal parameters and performance of related instruments.

Parameter	Technique	Time resolution	Detection Limit(1σ)	Accuracy
NO	Chemiluminescence ^a	1 min	200 pptv	±20%
NO_2	Chemiluminescence	1 min	1 min 300 pptv	
O_3	UV photometry	1 min	500 pptv	±5%
VOCs	GC-MS/FID ^b	60 min	20-300 pptv	±15%
Monoterpene	PTR-MS ^c	10 s	20 ppyv	±15%
Sa	Nano SMPS, SMPS, APS	5 min	-	±10%

^a Photolytic conversion to NO through blue light before detection; ^b Gas chromatography equipped with a mass spectrometer and a flame ionization detector; ^c Monoterpene was only measured in TZ2018.

Table S2. Parameters of initial model constraint for sensitivity test.

Parameters	NO ₂ /ppbv	NO ₂ /ppbv O ₃ /ppbv		Sa/µm ² ·cm ⁻³	$\gamma (N_2 O_5)^a$	kNO ₃ /s ⁻¹
Winter case	10	23	276	540	0.02	9×10 ⁻³
Summer case	27	49	300	2670	0.02	9×10 ⁻²

^{a.} With the Sa, T and $\gamma(N_2O_5)$, the constraint of kN_2O_5 can be calculated as $6\times10^{-4}\,\mathrm{s}^{-1}$ for winter case and $3\times10^{-3}\,\mathrm{s}^{-1}$ for summer case.

Table S3. Summary of parameters for calculating rate constant of k_{R1a} .

Source	k_0^{300}	n	$k_{_{\infty}}^{300}$	m	F	g
JPL2015	2.4×10 ⁻³⁰	3.0	1.6×10 ⁻¹²	-0.1	0.6	1.0
Mozart	2.0×10 ⁻³⁰	4.4	1.4×10 ⁻¹²	0.7	0.6	1.0
CB05	2.0×10 ⁻³⁰	4.4	1.4×10 ⁻¹²	0.7	0.6	1.0
Saprc07	3.6×10 ⁻³⁰	4.1	1.9×10 ⁻¹²	-0.2	0.35	$0.75\text{-}1.27 \times log_{10}0.35$
RACM2	2.0×10 ⁻³⁰	4.4	1.4×10 ⁻¹²	0.7	0.6	1.0
IUPAC2017	3.6×10 ⁻³⁰	4.1	1.9×10 ⁻¹²	-0.2	0.35	$0.75\text{-}1.27 \times \log_{10} 0.35$

Table S4. Summary of parameters for calculating rate constant of k_{R1b} .

Source	k_0^{300}	n	$k_{_{\infty}}^{300}$	m	F	g	A	B_1	B_2
JPL2015 ^a	2.4×10 ⁻³⁰	3.0	1.6×10 ⁻¹²	-0.1	0.6	1.0	5.8×10 ⁻²⁷	10840	10840
Mozart	2.2×10 ⁻³⁰	4.4	1.4×10 ⁻¹²	0.7	0.6	1.0	3.0×10 ⁻²⁷	10900	10900
CB05 ^b	$k_0^{300}/A = 1.0 \times 10^{-3}$	3.5	$k_{\infty}^{300}/\mathrm{A}=$	-0.1	0.45	1.0	-	11000	11080
			9.7×10^{14}						
Sapre07 ^b	$k_0^{300}/A=$ 1.3×10 ⁻³	3.5	$k_{\infty}^{300}/A=$ 9.7×10^{14}	-0.1	0.35	0.75- 1.27×log ₁₀ 0.35	-	11000	11080
RACM2	2.2×10 ⁻³⁰	4.4	1.4×10 ⁻¹²	0.7	0.6	1.0	2.7×10 ⁻²⁷	11000	11000
IUPAC20 17 ^b	$k_0^{300}/A=$ 1.3×10 ⁻³	3.5	$k_{\infty}^{300}/A=$ 9.7×10^{14}	-0.1	0.35	0.75- 1.27×log ₁₀ 0.35	-	11000	11080

a. This rate constant expression is reformed from k_{R1a}/Keq as defined in JPL2015, where the k_{R1a} and Keq are calculated with values recommended by JPL2015;

b. The k_0^{300}/A and k_{∞}^{300}/A are given in the form of ratio instead of separately.

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