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*Supplement of*

## **The dynamical core of the Aeolus 1.0 statistical–dynamical atmosphere model: validation and parameter optimization**

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# 1 Supplementary Information

2

## 3 S1 Planetary Waves

### 4 S1.1 Calculation of planetary waves at tropospheric levels excluding EBL-level

5 At other tropospheric levels than the EBL, the components are calculated by

$$\langle u^*(z) \rangle = -\frac{1}{f\rho_0} \nabla_\phi \langle p_z^* \rangle \quad (\text{S1})$$

$$\langle v^*(z) \rangle = \frac{1}{f\rho_0} \nabla_\lambda \langle p_z^* \rangle, \quad (\text{S2})$$

6

7 The azonal component is computed assuming isothermal expansion of air parcels in planetary waves

$$\langle p_z^* \rangle = \langle p_{EBL}^* \rangle \exp[(z - z_{EBL})/H_0] + \frac{p_* g}{\Gamma R} \exp[-z/H_0] \left\{ \ln \left[ \frac{T(z)}{T(z_{EBL})} \right] - \ln \left[ \frac{T(z)}{T(z_{EBL})} \right] \right\} \quad (\text{S3})$$

8 and

$$\langle p_{EBL}^* \rangle = \rho \left\{ \overline{\langle u_{EBL} \rangle} \right\} \nabla_\phi \langle \psi_{EBL}^* \rangle + 2 \left( \frac{\overline{\langle u_{EBL} \rangle}}{a \cos(\phi)} + \Omega \right) \sin(\phi) \langle \psi_{EBL}^* \rangle \quad (\text{S4})$$

9

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### 12 S1.2 Orographically induced stream function

13 For the waves excited by the orography, the stream function is calculated by

$$\beta \nabla_\lambda \langle \psi_{or,0,EBL}^* \rangle = -\frac{f}{H_0} \langle w_{or} \rangle + \frac{f^2}{g} \frac{\partial \langle u'v' \rangle^*}{\partial z} \quad (\text{S5})$$

14

15 where  $f$  is the Coriolis parameter and  $\beta = \nabla_\phi f$  and

16

$$w_{or} = \langle u \rangle \nabla_{\phi} h_{or} + \langle v \rangle \nabla_{\lambda} h_{or} + a_{std} (\langle u \rangle^2 + \langle v \rangle^2 + \langle u' \rangle^2 + \langle v' \rangle^2)^{1/2} h_{std}. \quad (S6)$$

- 1  
2 The variable  $h_{or}$  describes the grid cell averaged orography height  $h_{std}$  the subgrid scale standard deviation of the  
3 height of mountains, and  $a_{std}$  is an additional tuning parameter.  
4 The azonal component describes quasi-stationary planetary waves and is subdivided into a geostrophic and  
5 ageostrophic term:

$$u^* = u_{geos}^* + u_{ageos}^*$$

$$v^* = v_{geos}^* + v_{ageos}^*$$

### 6 **S1.3 Zeroth order solution of the thermally induced waves of the barotropic vorticity equation at the EBL**

- 7 We start from the z-projection of the baroclinic vorticity equation, which can be derived from the simplified Navier-  
8 Stokes-equation :

$$\bar{u} \frac{\partial}{\partial x} \left( \frac{\partial^2 \langle \Psi_{EBL}^* \rangle}{\partial x^2} + \frac{\partial^2 \langle \Psi_{EBL}^* \rangle}{\partial y^2} \right) + \beta \frac{\partial \langle \psi^* \rangle}{\partial x} = - \frac{\rho}{T_0} \frac{\partial \langle T_{EBL}^* \rangle}{\partial x} \frac{\partial \bar{p}}{\partial y} \frac{1}{\rho_0^2} \quad (S7)$$

- 9  
10 with  $= \frac{2\Omega}{a} \cos \phi$ , and  $\Omega$  is the earth's rotation angular velocity,  $a$  is the earth's radius and  $\phi$  the latitude.

- 11 In Eq. (S7)  $\langle \Psi_{EBL}^* \rangle$  is the stream function of the azonal large-scale component at the equivalent barotropic level  
12  $z_{EBL}$ ,  $x$  and  $y$  are the horizontal and vertical direction,  $T_0$  is the constant reference temperature and  $\langle T_{EBL}^* \rangle$  is the  
13 large-scale long-term azonal temperature at the EBL. The variable  $\bar{u}$  is the zonal mean zonal wind velocity,  $\rho_0$   
14 stands for the density near surface and  $\bar{p}$  is the zonal mean pressure.

- 15 For the stream function of the azonal large-scale component of motion at the equivalent barotropic level  $z_{EBL}$  we use  
16 the ansatz

$$\langle \Psi_{EBL}^* \rangle = \langle \Psi_{0,EBL}^* \rangle + \epsilon \langle \Psi_{1,EBL}^* \rangle + \dots$$

- 17 For the zeroth order approximation, we can neglect higher order derivations of  $\Psi$ :

$$\beta \frac{\partial \langle \Psi_{0,EBL}^* \rangle}{\partial x} = - \frac{1}{\rho T_0} \frac{\partial \langle T_{EBL}^* \rangle}{\partial x} \frac{\partial}{\partial y} \int_0^{\infty} \frac{\rho \langle [T(z)] \rangle dz}{H_0} \quad (S8)$$

- 18 In eq. (S8), we replaced  $\bar{p} = \int_0^{\infty} R \rho \langle [T(z)] \rangle dz / H_0$  and  $H_0 = RT_0 / g$  and  $\rho = \rho_0 \exp(-z/H_0)$ ,  $R$  is the gas  
19 constant,  $\rho$  is the air density,  $T$  is the temperature,  $H_0$  is the atmospheric scale height, and  $g$  the gravity  
20 acceleration. Per definition, one can replace the term with

$$\frac{\int_0^\infty p dz}{H_0} = \frac{gR}{RT_0} 2 \int_0^{z_{EBL}} \rho \langle [T(z)] \rangle dz$$

1 Such that

$$\frac{\partial \langle \psi_{0,EBL}^* \rangle}{\partial x} = - \frac{agR}{2\Omega RT_0^2 \rho_0 \cos \phi} 2 \frac{\partial}{\partial y} \int_0^{z_{EBL}} \rho \langle [T(z)] \rangle dz \frac{\partial \langle T_{EBL}^* \rangle}{\partial x}$$

2

3 With latter equation and  $\frac{1}{a} \nabla_\phi = \partial/\partial y$ , we can then derive

$$\langle \psi_{0,EBL}^* \rangle = - \langle T_{EBL}^* \rangle \frac{g}{\Omega \rho_0 T_0^2 \cos \phi} \nabla_\phi \int_0^{z_{EBL}} \rho \langle [T(z)] \rangle dz$$

4

5

## 6 S2 Derivation of the zonal mean meridional wind velocity

7 The zonal mean meridional wind velocity  $\overline{\langle v(z, \phi) \rangle}$  which also accounts for convective contribution is calculated by

$$\overline{\langle v(z, \phi) \rangle} =$$

$$\frac{d_1 \cdot (-2 \tan(\phi) (\overline{\langle u^* v^* \rangle} + \overline{\langle u' v' \rangle})) + d_2 \cdot \left( \frac{\partial}{\partial \phi} (\overline{\langle u^* v^* \rangle} + \overline{\langle u' v' \rangle}) \right) + d_3 \cdot \left( \left( -\frac{dK_z}{z} + \frac{K_z}{H_0} \right) \frac{\partial \overline{\langle u \rangle}}{\partial z} a \right) + d_4 \cdot (A)}{n_1 * (\tan(\phi) \overline{\langle u \rangle}) + n_2 * \left( -\frac{\partial \overline{\langle u \rangle}}{\partial \phi} \right) + n_3 * (2\Omega a \sin(\phi))}$$

(S9)

8 With  $K_z = 0.005 z$  and

$$A = \frac{\mathcal{L} \overline{\langle P_{co} \rangle}}{H_0} \frac{\overline{\langle u_{sf} \rangle}}{\Gamma_a - \Gamma_0 - \Gamma_1 (T_a - T_0) (1 - a_q q_s^2) + \Gamma_2 n_c}$$

9 whereby the parameters are given in **Table 1**. We roughly approximate  $\overline{\langle u_{sf} \rangle}$  by constant profile for this experiment

$$\overline{\langle u_{sf} \rangle} = \begin{cases} 2, & |\phi| > 40 \\ -2 \cos\left(\phi \frac{\pi}{40^\circ}\right), & \text{otherwise} \end{cases} \quad (\text{S10})$$

10

- 1 The additional calculation of  $\overline{\langle u_{sf} \rangle}$  instead of the calculated surface zonal velocity is done to avoid instabilities.  
 2 Instabilities can emerge due to the strong positive feedback between the meridional temperature and vertical wind  
 3 velocity, which lead to high latent heat. In nature these would be damped out but due to fixed troposphere height, we  
 4 parameterize it in the above described way.  
 5 For the derivation we start with the differential equation of the zonal wind component

$$\frac{du}{dt} = \frac{\tan \phi}{a} uv + fv - \frac{1}{\rho} \Delta_\lambda p + F_u \quad (\text{S11})$$

- 6 Whereby  $a$  is the Earth radius,  $f$  is the Coriolis factor and  $F_u$  is the frictional force in  $u$ -direction. Multiplying the  
 7 equation with  $\rho$  and using that  $\rho \frac{du}{dt} = \frac{d(\rho u)}{dt} - u \frac{d\rho}{dt}$ ,  $\frac{d(\rho u)}{dt} = \frac{\partial(\rho u)}{\partial t} + \mathbf{V} \cdot \Delta(\rho u)$  and  $\mathbf{V} \cdot \Delta(\rho u) = \Delta(\rho u \mathbf{V}) - (\rho u) \Delta \cdot$   
 8  $\mathbf{V}$ , we get

$$\frac{\partial(\rho u)}{\partial t} + \Delta(\rho u \mathbf{V}) - u \left( \frac{d\rho}{dt} + (\rho u) \Delta \cdot \mathbf{V} \right) = \frac{\tan \phi}{a} \rho uv + f \rho v - \Delta_\lambda p + \rho F_u$$

- 9 With the continuity equation and using spherical coordinates, the equation simplifies to

$$\begin{aligned} \frac{\partial(\rho u)}{\partial t} + \frac{1}{a \cos \phi} \frac{\partial(\rho u^2)}{\partial \lambda} + \frac{1}{a \cos \phi} \frac{\partial(\rho \cos \phi uv)}{\partial \phi} + \frac{\partial(\rho w u)}{\partial z} \\ = \frac{\tan \phi}{a} \rho uv + f \rho v - \frac{1}{a \cos \phi} \frac{\partial p}{\partial \lambda} + \rho F_u \end{aligned} \quad (\text{S12})$$

10

11

- 12 We calculate the zonal average  $(\overline{\dots})$ , take into account that  $\frac{\partial \bar{x}}{\partial \lambda} = 0$  and assume a vertical dependence of  
 13 the density ( $\rho = \rho_0(z)$ ):

$$\frac{\partial(\overline{\rho_0 u})}{\partial t} + \frac{1}{a} \frac{\partial(\overline{\rho_0 uv})}{\partial \phi} + \frac{\partial(\overline{\rho_0 w u})}{\partial z} = 2 \frac{\tan \phi}{a} \rho \overline{uv} + f \rho \bar{v} + \rho_0 \bar{F}_u$$

14

- 15 We split the wind variables into an synoptic scale waves, planetary waves and zonal mean wind ( $u = \bar{u} + u^* + u'$ ).  
 16 Under the assumption that  $\bar{u}$  and  $v^*$  are independent, the result of the zonal mean over the azonal component is zero:

$$\begin{aligned} \overline{uv} &= \overline{\bar{u}\bar{v}} + \overline{\bar{u}v^*} + \overline{\bar{u}v'} + \overline{u^*\bar{v}} + \overline{u^*v^*} + \overline{u^*v'} + \overline{u'\bar{v}} + \overline{u'v^*} + \overline{u'v'} \\ &= \overline{\bar{u}\bar{v}} + \overline{\bar{u}v'} + \overline{u^*v^*} + \overline{u'\bar{v}} + \overline{u'v'} \end{aligned}$$

1

2 We average eq. (S12) over time and phase speed ( $\langle \dots \rangle$ ). Due to a “gap” in the three-dimensional (period-wavelength-  
3 phase velocity) spectrum of atmospheric processes (see, e.g., Fraedrich & Böttger 1978, Coumou et al. 2011), the  
4 synoptic-scale component in its interaction with the large-scale long-term component of the atmospheric fields on the  
5 time scales about 10-20 days and longer could be, to a first approximation, represented (described) in terms of its  
6 ensemble (statistical) characteristics (the second and higher-order moments), and not as the individual eddies  
7 (Saltzman, 1978). We can simplify the terms  $\langle \bar{u}v' \rangle = \langle u'v \rangle = 0$ . In addition, it is  $\overline{\bar{u}\bar{v}} = \bar{u}\bar{v}$  due to quasi stationarity  
8 of both terms. It is also  $\langle \frac{dx}{dt} \rangle = 0$  and  $\langle \bar{u}\bar{v} \rangle = \langle \bar{u} \rangle \langle \bar{v} \rangle$  since the oscillations of  $\bar{u}$  and  $\bar{v}$  are very small and independent  
9 of each other. By using the continuity equation  $\frac{\rho_0}{a} \frac{\partial \langle \bar{v} \rangle}{\partial \phi} - \frac{\tan \phi}{a} \rho_0 \bar{v} + \frac{\partial(\rho_0 \langle \bar{w} \rangle)}{\partial z} = 0$ , we can simplify eq. (S12) to

$$\begin{aligned} \frac{1}{a} \rho_0 \langle \bar{v} \rangle \frac{\partial \langle \bar{u} \rangle}{\partial \phi} + \frac{\rho_0}{a} \frac{\partial (\langle v^* u^* \rangle + \langle v' u' \rangle)}{\partial \phi} + \rho_0 \langle \bar{w} \rangle \frac{\partial \langle \bar{u} \rangle}{\partial z} + \frac{\partial (\rho_0 \langle \bar{w}^* u^* \rangle + \langle \bar{w}' u' \rangle)}{\partial z} \\ = \frac{\tan \phi}{a} \rho_0 \langle \bar{u} \rangle \langle \bar{v} \rangle + 2 \frac{\tan \phi}{a} (\langle v^* u^* \rangle + \langle v' u' \rangle) + f \rho \bar{v} + \rho_0 \bar{F}_u \end{aligned} \quad (\text{S13})$$

10 With the assumption that  $\rho_0 = e^{-z/H_0}$  and  $\rho_0 \bar{F}_u = \frac{\partial \bar{\tau}}{\partial z} = \frac{\partial}{\partial z} \left( \kappa \rho_0 \frac{\partial \langle \bar{u} \rangle}{\partial z} \right) = \kappa \frac{\partial \rho_0}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \frac{\partial \kappa}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \kappa \frac{\partial^2 \langle \bar{u} \rangle}{\partial z^2} =$   
11  $-\kappa \frac{\rho_0}{H_0} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \frac{\partial \kappa}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z}$ , we obtain

$$\begin{aligned} \rho_0 \langle \bar{v} \rangle \left( \frac{1}{a} \frac{\partial \langle \bar{u} \rangle}{\partial \phi} - \frac{\tan \phi}{a} \langle \bar{u} \rangle - f \right) = 2 \frac{\tan \phi}{a} (\langle v^* u^* \rangle + \langle v' u' \rangle) - \frac{\rho_0}{a} \frac{\partial (\langle v^* u^* \rangle + \langle v' u' \rangle)}{\partial \phi} - \rho_0 \langle \bar{w} \rangle \frac{\partial \langle \bar{u} \rangle}{\partial z} - \\ \frac{\partial (\rho_0 \langle \bar{w}^* u^* \rangle + \langle \bar{w}' u' \rangle)}{\partial z} - \kappa \frac{\rho_0}{H_0} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \frac{\partial \kappa}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z} \end{aligned} \quad (\text{S14})$$

12 The contribution to the vertical exchange of the atmospheric momentum from stationary eddies described in our case  
13 by zonally averaged  $\langle \bar{w}^* u^* \rangle$  is shown negligibly small (Hantel and Hacker, 1978). Also, the scale analysis attests  
14 that  $\langle \bar{w} \rangle \frac{\partial \langle \bar{u} \rangle}{\partial z}$  are small (Petoukhov et al., 2003):

$$-\rho_0 \langle \bar{w} \rangle \frac{\partial \langle \bar{u} \rangle}{\partial z} - \frac{\partial (\rho_0 \langle \bar{w}^* u^* \rangle + \langle \bar{w}' u' \rangle)}{\partial z} - \kappa \frac{\rho_0}{H_0} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \frac{\partial \kappa}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z} \approx - \frac{\partial (\rho_0 \langle \bar{w}' u' \rangle)}{\partial z} - \kappa \frac{\rho_0}{H_0} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \frac{\partial \kappa}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z}$$

15

16 Hence the eq. (S14) can be rewritten into

$$\begin{aligned} \rho_0 \langle \bar{v} \rangle \left( \frac{1}{a} \frac{\partial \langle \bar{u} \rangle}{\partial \phi} - \frac{\tan \phi}{a} \langle \bar{u} \rangle - f \right) = 2 \frac{\tan \phi}{a} (\langle v^* u^* \rangle + \langle v' u' \rangle) - \frac{\rho_0}{a} \frac{\partial (\langle v^* u^* \rangle + \langle v' u' \rangle)}{\partial \phi} - \rho_0 \langle \bar{w} \rangle \frac{\partial \langle \bar{u} \rangle}{\partial z} - \\ \frac{\partial (\rho_0 \langle \bar{w}^* u^* \rangle + \langle \bar{w}' u' \rangle)}{\partial z} - \kappa \frac{\rho_0}{H_0} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \frac{\partial \kappa}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z} \end{aligned} \quad (\text{S15})$$

- 1 With  $\langle u'w' \rangle = -\kappa' \frac{\partial \langle \bar{u} \rangle}{\partial z}$ , whereby  $\kappa'$  is the coefficient of large-scale turbulent exchange for the momentum due to  
 2 transient synoptic eddies (Williams and Davies, 1965), we get

$$\begin{aligned} \rho_0 \langle \bar{v} \rangle \left( \frac{1}{a} \frac{\partial \langle \bar{u} \rangle}{\partial \phi} - \frac{\tan \phi}{a} \langle \bar{u} \rangle - f \right) \\ = 2 \frac{\tan \phi}{a} (\langle \overline{v^* u^*} \rangle + \langle \overline{v' u'} \rangle) - \frac{\rho_0}{a} \frac{\partial (\langle \overline{v^* u^*} \rangle + \langle \overline{v' u'} \rangle)}{\partial \phi} - (\kappa + \kappa') \frac{\rho_0}{H_0} \frac{\partial \langle \bar{u} \rangle}{\partial z} + \rho_0 \frac{\partial (\kappa + \kappa')}{\partial z} \frac{\partial \langle \bar{u} \rangle}{\partial z} \end{aligned}$$

- 3 With  $K_z = \kappa + \kappa'$  we can simplify the equation to

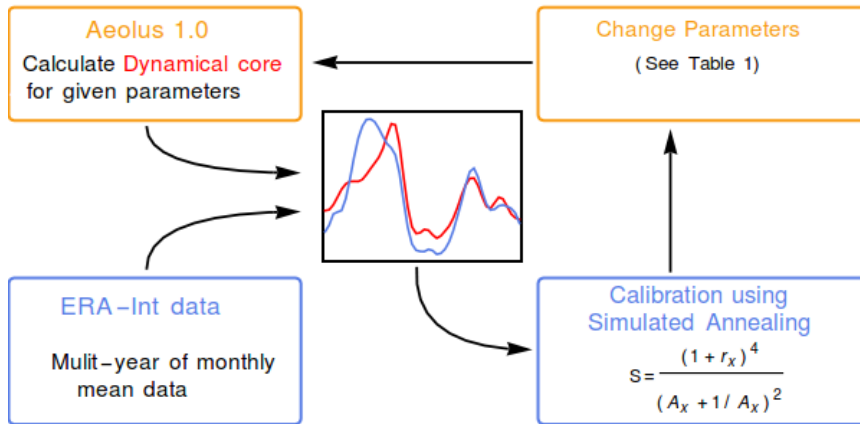
$$\langle \overline{v(z, \phi)} \rangle = \frac{-2 \tan(\phi) (\langle \overline{u^* v^*} \rangle + \langle \overline{u' v'} \rangle) + \frac{\partial}{\partial \phi} (\langle \overline{u^* v^*} \rangle + \langle \overline{u' v'} \rangle) + (-\frac{dK_z}{dz} + \frac{K_z}{H_0}) \frac{\partial \langle \bar{u} \rangle}{\partial z} a}{\tan(\phi) \langle \bar{u} \rangle - \frac{\partial \langle \bar{u} \rangle}{\partial \phi} + 2\Omega a \sin(\phi)}$$

(S16)

- 4 The derived equation for the meridional velocity does not account for latent heat release associated with  
 5 convective precipitation. To capture this additional term we include convective precipitation and finally  
 6 introduce tuning parameters, which have values close to 1.  
 7

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### 9 S3 Schematic plot of the optimization process



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