Supplementary Materials

Hydrologic-Land Surface Modelling of a Complex System under Precipitation

Uncertainty: A Case Study of the Saskatchewan River Basin, Canada

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1.0 MESH new features

In order to enable MESH to model complex and highly managed basins (e.g. SaskRB), new water management features (irrigation, reservoir operation, and diversion) have been integrated recently into the MESH framework.

The irrigation algorithm is based on the soil moisture deficit approach, similar to that of Pokhrel et al. (2016). The net irrigation

5 water demand is estimated as the difference between target soil moisture content (θ_T) and the simulated actual soil moisture (θ_k) .

$$
IR = \frac{\rho_w}{\Delta t} \sum_{k=1}^{n} \{ \max[(\theta_T - \theta_k), 0] * D_k \}
$$
\n(S1)

where IR [kg m⁻² s] is the net irrigation demand, ρ_w [kg m⁻³] is the density of water; Δt is model time step; θ_T is given as $\alpha *$ θ_{FC} ; θ_{FC} and θ_k [m³ m⁻³] are the field capacity and simulated actual volumetric soil moisture content, respectively; α [-] is the

- 10 parameter that defines the upper soil moisture limit which has been used varyingly from 0.5 to 1; and D_k [m] is the thickness of κ^{th} soil layer, *n* represents the number of soil layers considered in the calculation. In order to represent irrigation effects, the standard CLASS three soil layer configuration has been changed to four soil layers so that the bottom of the third soil layer is set to around 1m. The thickness of each soil layer is 0.1, 0.25, 0.7, and 3.05 m. The top three layers are considered for irrigation with a crop root depth of 1.0m. The estimated irrigation demand is applied to the soil as rain between 0600 and 1000
- 15 local time each day in a similar approach as Ozdogan et al., (2010) and Pokhrel et al., (2016). The excess irrigation water (return flow) is assumed to join the nearest river system in the form of interflow and bottom-layer soil drainage. Reservoir regulation is represented by the Dynamically Zoned Target Release (DZTR) scheme which uses a parametric piecewise-linear function to approximate actual reservoir release rules (Yassin et al., 2019). The DZTR scheme divides reservoir storage into five zones, dead storage (Zone 0), critical storage (Zone 1), normal storage (Zone 2), flood storage (Zone
- 20 3) and emergency storage (Zone 4). Whenever storage is below full supply storage zone, the release only occurs at the bottom outlet, but when storage is within flood storage, the release happens from both outflow outlet and spillway. The dead storage (Zone 0) amount is assumed 10 % of the maximum storage or a dead storage value from the reservoir characteristics data. In general, where no operational information is available, the other storage zones is estimated from historical time series of storage by defining some non-exceedance probability value for each zone or by optimizing these zones to reproduce the observed
- 25 storage and release time series. Target releases for each zone are obtained in a similar fashion. These target storages and releases are allowed to vary each month (or on any other arbitrarily selected time step) to allow a better representation of the seasonality of reservoir operation.

Zone 0	$Q_t = 0$	$[S_t < 0.1S_{max}]$	(S2)	
Zone 1	$Q_t = min\left(Q_{ci}, \frac{S_t - 0.1S_{max}}{\Delta t}\right)$	$[0.1S_{max} < S_t \le S_{ci}]$	(S3)	
30	Zone 2	$Q_t = Q_{ci} + (Q_{ni} - Q_{ci}) \frac{(S_t - S_{ci})}{(S_{ni} - S_{ci})}$	$[S_{ci} < S_t \le S_{ni}]$	(S4)
Zone 3A	$Q_t = Q_{ni} + (Q_{mi} - Q_{ni}) \frac{(S_t - S_{ni})}{(S_{mi} - S_{ni})}$	$[S_{ni} < S_t \le S_{mi}]$	(S5A)	

zone 3B
$$
Q_t = Q_{ni} + max\{(I_t - Q_{ni}), (Q_{mi} - Q_{ni})\}\frac{(S_t - S_{ni})}{(S_{mi} - S_{ni})}
$$
 $[S_{ni} < S_t \le S_{mi}]$ (5B)
\n**zone 4** $Q_t = min(\left[max\left(\frac{(S_t - S_{mi})}{\Delta t}, Q_{mi}\right)\right], Q_{mc})$ $[S_{mi} < S_t]$ (56)

where I_t , Q_t and S_t are inflow, release and storage at time step t. S_{ci} , S_{ni} and S_{mi} are critical, normal and maximum storage targets for month *i*. Q_{ci} , Q_{ni} and Q_{mi} are critical, normal and maximum release targets for month *i*. Q_{mc} is maximum channel 5 capacity parameter.

We also developed a flow diversion process within MESH to represent water transfer across the basin via engineered works, for various purposes including irrigation. Flow diversion is the water transfers within-basin from one river node to another, water transfers from outside basin to within-basin river node, and water withdrawals from river node to irrigated areas. The flow diversion implementation in MESH is divided into two types depending on the location of source and sink of diverted

10 water: type 1 has either a water source or sink located outside the whole basin; type 2 has both sources and sink located within the basin. To divert water from one point to another, the locations of source and sink and the amount to be diverted at each time step are provided as input to the model. However, in the case of flow diversion for irrigation, the amount of water for diversion is estimated using the irrigation demand algorithm discussed above.

Table S1: Summary of major reservoirs in Saskatchewan River Basin that are accounted for in the modelling

Main purpose: **WS**-Water Supply, **HP**-Hydropower **IR**-Irrigation **FC**-Flood Control

Table S2: Summary of irrigation districts in Alberta and reservoirs in Saskatchewan

Table S3: Streamflow stations for calibration and validation of the model

Table S4: Climate stations with Adjusted and Homogenized Canadian Climate Data (AHCCD)

Figure S1: Simulated (light red) and observed (black) streamflow of selected stations in SaskRB. The calibration and validation period is separated by a vertical line at the end of 2008.

References

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