



45

50

5.6

6.3

7.1

8.0

9.2

10

11



2.8

3.2

3.6

4.0

4.4

4.8

5.2

5.6

6.0

6.4

6.8

7.2

7.6

8.0

8.4

8.8

9.2

9.6

10.0

10.4

10.8

11.2

11.6

12.0

12.4

12.8

13.2

13.6

14.0

14.4

14.8

15.2

15.6

16.0

16.4

16.8

17.2

17.6

18.0



MICROCOPY RESOLUTION TEST CHART

NATIONAL BUREAU OF STANDARDS - 1963

Comitato Nazionale Energia Nucleare

## METHOD OF ANALYSIS OF NEUTRON CAPTURE GAMMA-RAY SPECTRA

*A. Fubini, A. Napoli, D. Prosperi, F. Terrasi*

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CNEN - RT/FI(70)47

A. Fubini, A. Napoli, D. Prosperi, F. Terrasi (CNEN, Laboratorio Fisica Nucleare Applicata)

METHOD OF ANALYSIS OF NEUTRON CAPTURE GAMMA-RAY SPECTRA

**RIASSUNTO** - Vengono descritte le tecniche utilizzate per tarare gli spettri di cattura dei rivelatori al Ge(Li). Viene proposto un metodo di calcolo che dall'energia dei gamma permette di ottenere uno schema di decadimento col metodo di Ritz. Il metodo è applicato alla reazione  $\text{Cl}^{35}(n, \gamma)$ .

# METHOD OF ANALYSIS OF NEUTRON CAPTURE GAMMA-RAY SPECTRA

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METHOD OF ANALYSIS OF NEUTRON CAPTURE GAMMA-RAY SPECTRA

**SUMMARY** - The method used to calibrate the neutron capture gamma-ray spectra of a Ge(Li) detector is described in detail. The procedure used to obtain from the gamma-ray energy a decay scheme is reported. The method is applied to the  $\text{Cl}^{35}(n, \gamma)$  reaction.

*Tesio pervenuto il 19 novembre 1970*

### 1 - Introduction

One of the most suitable methods for investigating the nuclear level structure is the analysis of the  $\gamma$ -ray spectra arising from reaction such as  $(n, \gamma)$  or from the decay of radioactive isotopes. In spite of the complexity usually shown by these spectra it is possible to observe and analyse correctly a large number of  $\gamma$ -ray lines (typically  $>100$ ) with increasing precision, due to the development of high resolution Ge(Li) spectrometers, precise calibration curve determination, and methods of analysis of line shapes.

With such a number of transitions it would be very long and difficult to perform a complete analysis of the level scheme inserting in it more than a small number of transitions by means of coincidence experiments.

Then, starting from the knowledge of the energies of a small number of levels and of a large number of transitions one can try to construct a decay scheme by the Ritz combination principle. In the present paper such a method is described in detail and some results obtained for the reaction  $^{35}\text{Cl}(n, \gamma)$  are reported.

The computer programs arranged for this purpose are described in section 2. In section 3 we report the method used for obtaining precise energy measurements. The application of

the Ritz method to the construction of the  $^{36}\text{Cl}$  level scheme is described in section 4.

## 2 - Computer codes

The computation are carried out by the programs PLOT and PROB. The procedure starts from some known levels of energy  $E_L + \delta E_L$  and from the  $\gamma$ -ray energy  $E_\gamma + \delta E_\gamma$ . The program PLOT calculate for some discrete values of energy  $E$  how many times combinations  $(E_L, E_\gamma)$  such that  $\left[|E-E_L| - E_\gamma\right]^2 < (\delta E_L^2 + \delta E_\gamma^2)$  are obtained.

The energy values  $E$  should vary in the chosed interval by steps of lenght smaller than the smallest value of  $(\delta E_L^2 + \delta E_\gamma^2)$ . If more than a preset number of combinations is found for one of these values that energies is considered as a possible new level.

Because of the condition imposed to the lenght of the steps this will usually occur for several neighbouring values. The plot of the number of combinations vs. energy, provided by the program will thus show a number of peaks corresponding to the possible levels on a continuous background: this is due to the finite errors of the energy measurements that give rise to accidental combinations. If the spin  $I_i$  and  $I_f$  parities  $\pi_i$  and  $\pi_f$  of initial and final states are known as well as the multipolarity  $L$  of the transitions the program check if the relationship

$$I_i + L \geq I_f \geq (I_i - L)$$

$$\text{are } \pi_i \cdot \pi_f = \pi_f$$

are satisfied. The combinations not satisfying these selection rules may be disregarded thus reducing the number of accidental combinations.

The probability of obtaining such accidental combinations depends strongly on the magnitude of the energy errors. It is therefore very important to measure with good accuracy the transition energies; section 3 is devoted to this problem. A computer code, PROB, was developed in order to calculate by means of a self consistent procedure, the energy of the levels as a weighted mean of the single values provided by pair  $(E_L, E_\gamma)$  where  $E_L$  is a known level connected to the new level by the transition  $E_\gamma$ .

The program calculates also the probability of the level candidate being purely accidental. The method is similar to that proposed in Ref. 1) and will not be described in detail here.

A list of PROB an PLOT program are reported in Appendix.

## 3 - Analysis of $\gamma$ spectra

In the sample treated the capture  $\gamma$ -ray spectrum measurement in  $^{35}\text{Cl}$  was performed by means of a  $\text{Ge}(\text{Li})^{(2)}$  spectrometer. The resolution was  $\sim 4$  Kev at 1.3 MeV and  $\sim 10$  Kev at 7 MeV. The measurement of the energies was carried out in the following manner. Below 2 MeV a spectrum was recorded with a Chlorine target and some calibration sources ( $\text{Cs}^{137}$ ,  $\text{Y}^{88}$ ,  $\text{Na}^{22}$ ): from 2 to 8 MeV the Sodium lines at 2516.0, 3588.10, 3981.69, 5617.91, 6396.93 Kev were used for calibration purposes by irradiating a mixed target of Cl+Na.

The energy of the most intense lines of  $^{36}\text{Cl}$  was calculated by

means of best fit with a fourth order polinomials.

The estimates of error  $\delta E_{\gamma}$  attributes to each energy value  $E_{\gamma}$  was calculated evaluating the error in the peak position and the quality of the fit. The energies of the weaker lines were obtained in a similar manner from the single target spectra using the strong lines as calibration.

Moreover the existence of some cascade was used for calibration purpose: in fact if we known the  $\gamma$  ray populating and depopulating some level, we can obtain several estimate of Q value. After a test of the statistical distribution of these estimates we calculate the high energy  $\gamma$  ray as the difference between the weighted mean of the Q value estimate and the corresponding low energy values and added them to the other calibration point for a new fitting. This procedure was repeated until the Q value converged to a fixed value. The calibration curve thus obtained is reported in fig. 1.

#### 4 - Construction of a decay scheme

To construct the decay scheme of  $\text{Cl}^{36}$  a iterative procedure was used. From coincidence measurement and (d, p) studies<sup>(3)</sup> it has been possible to obtain the levels scheme shown in fig. 2. We use this decay scheme and the  $\gamma$  ray listed in Tab. 1 as the basis for the search of new levels. The most probable levels obtained was at 3633.6, 3964.5, 4497.6, 5958.6 KeV. The probability that one of these levels was random was less than 35% and as the intensity balance was roughly correct they are added to the previous one. This procedure was repeated until no new level will be found with probability higher than 65%.

The decay scheme obtained is reported in fig. 3. All the

levels have probability to be true higher than 65% : as an exception the level at 4139.2 was accepted for his strong agreement with the (d, p) experiment. Moreover the intensity balance is roughly correct as shown in Tab. 2. Finally as estimate of the spin of the new level was obtained assuming than all the transitions inserted in fig. 3 are E1, M1 or E2. This assumptions will be justified observing that all the transitions inserted in the scheme of fig. 2 are of those multipolarity.

The value of the spin obtained are reported in fig. 3: this results was obtained taking also into account the restriction imposed by the angular momentum conservation for the levels for which the  $l_n$  values are known for (d,p) relation.

Tables caption

Table I - Summary of energy and intensity results for the gamma radiation following neutron capture in natural chlorine.

Table II - Intensity balance for the lowest lying levels. correction for electron losses have been neglected.

Table 1

| transitio<br>n | $E_eV$     | $H^-/100 cap$ | $H^-$ | $(eV)$     | transitio<br>n | $H^-/100 cap$ | $H^-$ | $(eV)$ |
|----------------|------------|---------------|-------|------------|----------------|---------------|-------|--------|
| 1              | 8580.5±0.7 | 3.12          | 23    | 5586.5±1.2 | 0.50           |               |       |        |
| 2              | 7792.1±0.7 | 8.51          | 24    | 5544.0±1.5 | 0.21           |               |       |        |
| 3              | 7415.2±0.6 | 10.30         | 25    | 5519.1±1.1 | 1.67           |               |       |        |
| 4              | 7320.3±2.1 | 0.05          | 26    | 5473.4±1.5 | 0.11           |               |       |        |
| 5              | 6979.8±0.5 | 2.21          | 27    | 5405.3±1.5 | 0.10.          |               |       |        |
| 6              | 6954.9±1.1 | 0.15          | 28    | 5374.5±1.4 | 0.10           |               |       |        |
| 7              | 6892.6±2.6 | 0.90          | 28'   | 5261.9±1.5 | 0.10           |               |       |        |
| 8              | 6869.9±2.9 | 0.90          | 29    | 5248.0±1.2 | 0.60           |               |       |        |
| 9              | 6628.9±1.0 | 5.00          | 30    | 5206.0±1.8 | 0.25           |               |       |        |
| 10             | 6620.9±1.0 | 8.50          | 31    | 5150.1±1.3 | 0.26           |               |       |        |
| 11             | 6552.8±1.8 | 0.17          | 32    | 5114.0±1.5 | 0.10           |               |       |        |
| 12             | 6491.5±0.9 | 0.18          | 33    | 5079.3±1.6 | 0.16           |               |       |        |
| 13             | 6423.2±1.2 | 0.28          | 34    | 5019.1±1.2 | 0.45           |               |       |        |
| 14             | 6383.5±1.2 | 0.10          | 35    | 4982.0±1.1 | 3.70           |               |       |        |
| 15             | 6346.3±2.3 | 0.16          | 36    | 4946.6±1.0 | 1.00           |               |       |        |
| 16             | 6269.8±0.9 | 0.41          | 36'   | 4881.8±2.8 | 0.12           |               |       |        |
| 17             | 6113.0±0.9 | 20.80         | 36"   | 4854.3±1.5 | 0.07           |               |       |        |
| 17'            | 6004.5±3.4 | 0.10          | 37    | 4829.8±1.5 | 0.16           |               |       |        |
| 18             | 5957.0±1.1 | 0.24          | 38    | 4816.7±1.5 | 0.15           |               |       |        |
| 19             | 5905.4±1.0 | 0.12          | 39    | 4793.4±1.5 | 0.09           |               |       |        |
| 19'            | 5735.8±1.5 | 0.15          | 40    | 4757.4±1.2 | 0..            |               |       |        |
| 20             | 5716.9±1.1 | 5.86          | 41    | 4730.2±1.1 | 0.83           |               |       |        |
| 21             | 5640.1±1.4 | 0.13          | 41'   | 4713.0±1.5 | 0.09           |               |       |        |
| 22             | 5607.7±1.6 | 0.37          | 42    | 4707.9±1.4 | 0.45           |               |       |        |

Table 1 (continued)

| $\gamma$<br>transition | $E_\gamma$<br>(keV) | $I_\gamma$<br>( $\gamma/100$ cap) | $\gamma$<br>transition | $E_\gamma$<br>(keV) | $I_\gamma$<br>( $\gamma/100$ cap) |
|------------------------|---------------------|-----------------------------------|------------------------|---------------------|-----------------------------------|
| 43                     | 4685.1±1.4          | 0.06                              | 63                     | 3858.7±1.6          | 0.22                              |
| 44                     | 4617.0±1.0          | 0.55                              | 64                     | 3823.4±0.7          | 1.56                              |
| 45                     | 4589.6±1.2          | 0.24                              | 65                     | 3775.2±1.3          | 0.25                              |
| 46                     | 4548.6±1.2          | 0.49                              | 66                     | 3756.4±1.2          | 0.10                              |
| 47                     | 4525.3±1.1          | 0.40                              | 67                     | 3748.0±1.2          | 0.22                              |
| 48                     | 4441.8±1.0          | 0.91                              | 68                     | 3737.6±1.2          | 0.27                              |
| 49                     | 4416.9±1.3          | 0.33                              | 69                     | 3707.2±1.6          | 0.23                              |
| 50                     | 4378.6±1.0          | 0.10                              | 70                     | 3662.2±0.8          | 0.26                              |
| 51                     | 4337.5±1.4          | 0.19                              | 70'                    | 3650.2±1.1          | 0.13                              |
| 52                     | 4299.6±1.0          | 0.46                              | 71                     | 3636.8±1.1          | 0.28                              |
| 53                     | 4207.4±1.8          | 0.15                              | 72                     | 3628.8±1.1          | 0.28                              |
| 54                     | 4140.1±1.3          | 0.16                              | 72'                    | 3616.8±1.1          | 0.16                              |
| 55                     | 4128.7±1.3          | 0.05                              | 73                     | 3601.4±1.2          | 0.93                              |
| 56                     | 4114.8±1.3          | 0.04                              | 74                     | 3585.6±1.1          | 0.82                              |
| 57                     | 4083.6±0.8          | 0.50                              | 75                     | 3562.5±1.1          | 1.04                              |
| 58                     | 4057.4±1.2          | 0.75                              | 76                     | 3548.0±1.1          | 0.10                              |
| 58'                    | 4047.2±1.5          | 0.11                              | 77                     | 3525.5±1.1          | 0.05                              |
| 59                     | 4033.1±2.4          | 0.15                              | 78                     | 3511.8±1.1          | 0.18                              |
| 60                     | 3999.6±1.2          | 0.12                              | 79                     | 3500.4±1.1          | 0.31                              |
| 61                     | 3981.4±1.2          | 1.10                              | 80                     | 3465.3±1.2          | 0.10                              |
| 62                     | 3965.7±1.2          | 0.43                              | 80'                    | 3445.5±1.5          | 0.10                              |
| 62'                    | 3914.5±1.5          | 0.13                              | 81                     | 3429.1±0.6          | 0.89                              |
| 62"                    | 3883.8±1.5          | 0.09                              | 82                     | 3371.4±0.6          | 0.47                              |

Table 1 (continued)

| $\gamma$<br>transition | $E_\gamma$<br>(keV) | $I_\gamma$<br>( $\gamma/100$ cap) | $\gamma$<br>transition | $E_\gamma$<br>(keV) | $I_\gamma$<br>( $\gamma/100$ cap) |
|------------------------|---------------------|-----------------------------------|------------------------|---------------------|-----------------------------------|
| 83                     | 3350.1±1.1          | 0.14                              | 105                    | 2705.7±1.0          | 0.36                              |
| 84                     | 3332.3±0.6          | 0.52                              | 106                    | 2676.5±0.4          | 1.30                              |
| 85                     | 3310.8±1.1          | 0.16                              | 107                    | 2649.5±1.1          | 0.18                              |
| 86                     | 3287.6±1.1          | 0.13                              | 108                    | 2622.5±0.5          | 0.22                              |
| 87                     | 3267.9±1.1          | 0.13                              | 109                    | 2592.3±1.0          | 0.11                              |
| 88                     | 3248.2±3.3          | 0.23                              | 110                    | 2578.6±1.0          | 0.11                              |
| 89                     | 3214.6±1.1          | 0.18                              | 110'                   | 2557.1±1.0          | 0.15                              |
| 90                     | 3199.9±1.4          | 0.21                              | 111                    | 2534.3±0.6          | 0.46                              |
| 91                     | 3161.0±2.6          | 0.12                              | 111'                   | 2517.5±1.0          | 0.08                              |
| 92                     | 3135.1±1.1          | 0.14                              | 112                    | 2491.0±0.4          | 0.51                              |
| 93                     | 3114.6±0.5          | 0.75                              | 113                    | 2468.4±0.3          | 0.68                              |
| 93'                    | 3088.3±1.1          | 0.10                              | 114                    | 2418.3±0.4          | 0.41                              |
| 94                     | 3061.0±0.5          | 3.07                              | 114'                   | 2384.3±1.0          | 0.14                              |
| 95                     | 3015.5±0.5          | 0.86                              | 115                    | 2362.5±1.0          | 0.12                              |
| 96                     | 2996.6±0.5          | 1.03                              | 116                    | 2346.5±1.5          | 0.15                              |
| 97                     | 2973.1±0.5          | 0.97                              | 117                    | 2323.7±1.0          | 0.24                              |
| 98                     | 2922.5±1.1          | 0.80                              | 118                    | 2309.7±0.6          | 0.50                              |
| 99                     | 2896.5±0.7          | 0.34                              | 119                    | 2287.6±2.5          | 0.14                              |
| 100                    | 2863.4±0.4          | 0.73                              | 120                    | 2270.0±1.0          | 0.13                              |
| 101                    | 2843.9±0.9          | 0.54                              | 121                    | 2247.0±1.0          | 0.29                              |
| 102                    | 2808.2±1.5          | 0.51                              | 122                    | 2199.3±0.6          | 1.85                              |
| 103                    | 2799.5±1.5          | 0.51                              | 123                    | 2179.0±1.0          | 0.30                              |
| 104                    | 2755.4±1.2          | 0.19                              | 124                    | 2157.6±0.5          | 0.39                              |

Table 1 (continued)

| $\gamma$<br>transition | $E_\gamma$<br>(keV) | $I_\gamma$          | $\gamma$<br>transition | $E_\gamma$<br>(keV) | $I_\gamma$          |
|------------------------|---------------------|---------------------|------------------------|---------------------|---------------------|
|                        |                     | ( $\gamma/100$ cap) |                        |                     | ( $\gamma/100$ cap) |
| 125                    | $2076.0 \pm 0.6$    | 0.40                | 139                    | $1716.8 \pm 1.5$    | 0.22                |
| 126                    | $2039.2 \pm 0.9$    | 0.40                | 140                    | $1641.2 \pm 0.7$    | 0.51                |
| 127                    | $1959.5 \pm 0.2$    | 9.60                | 141                    | $1601.1 \pm 0.2$    | 3.00                |
| 128                    | $1951.5 \pm 0.2$    | 14.70               | 142                    | $1327.3 \pm 0.4$    | 1.06                |
| 129                    | $1903.8 \pm 1.0$    | 0.18                | 143                    | $1266.5 \pm 0.5$    | 0.10                |
| 130                    | $1889.4 \pm 1.4$    | 0.14                | 144                    | $1164.9 \pm 0.2$    | 23.90               |
| 131                    | $1875.4 \pm 1.4$    | 0.11                | 145                    | $1131.4 \pm 0.3$    | 1.66                |
| 132                    | $1860.9 \pm 1.1$    | 0.36                | 146                    | $789.3 \pm 0.3$     | 10.80               |
| 133                    | $1847.8 \pm 1.5$    | 0.18                | 147                    | $786.5 \pm 0.3$     | 13.00               |
| 134                    | $1833.3 \pm 0.9$    | 0.40                | 148                    | $632.5 \pm 0.4$     | 0.19                |
| 135                    | $1814.3 \pm 1.5$    | 0.27                | 149                    | $517.0 \pm 0.2$     | 21.90               |
| 136                    | $1791.2 \pm 1.5$    | 0.30                | 150                    | $436.4 \pm 0.3$     | 0.83                |
| 136'                   | $1774.8 \pm 2.0$    | 0.10                | 151                    | $358.5 \pm 0.4$     | 0.18                |
| 137                    | $1748.6 \pm 1.6$    | 0.15                | 152                    | $291.9 \pm 0.3$     | 0.21                |
| 138                    | $1733.0 \pm 1.5$    | 0.22                |                        |                     |                     |

Table 2

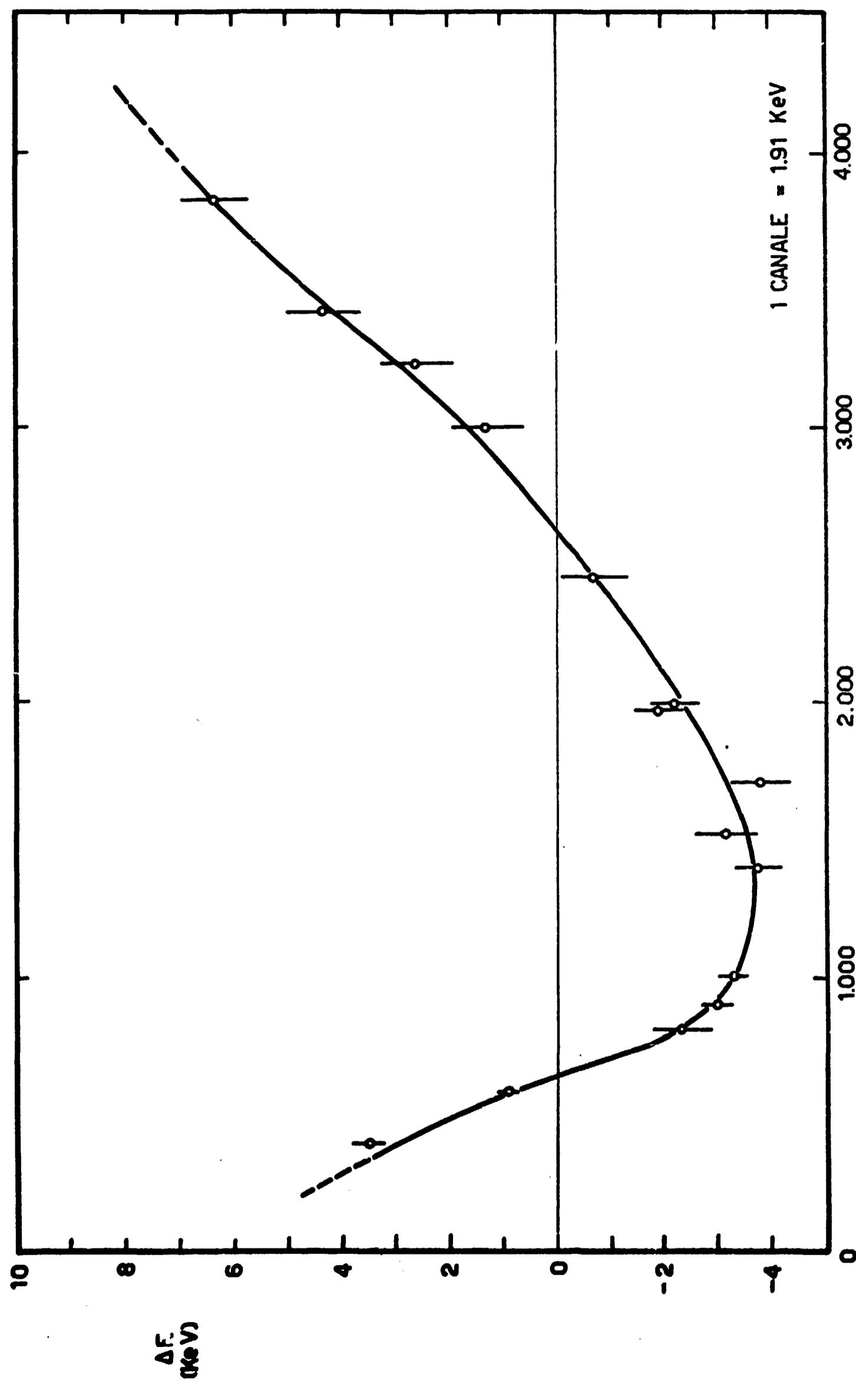
| $E_{\gamma 1} + \delta E_{\gamma 1}$<br>(keV) | $E_{\gamma 2} + \delta E_{\gamma 2}$<br>(keV) | $Q \pm \delta Q$<br>(keV) |
|---|---|---------------------------|
| $2622.6 \pm 0.5$                              | $5958.6 \pm 0.4$                              | $8581.2 \pm 0.6$          |
| $4442.1 \pm 1.0$                              | $4139.3 \pm 0.3$                              | $8581.4 \pm 1.0$          |
| $4617.3 \pm 1.1$                              | $3964.9 \pm 0.4$                              | $8582.3 \pm 1.1$          |
| $6113.6 \pm 0.9$                              | $2468.6 \pm 0.2$                              | $8582.2 \pm 0.9$          |
| $6621.4 \pm 0.8$                              | $1959.6 \pm 0.2$                              | $8581.0 \pm 0.8$          |
| $6980.5 \pm 0.5$                              | $1601.2 \pm 0.2$                              | $8581.7 \pm 0.5$          |
| $7416.4 \pm 0.5$                              | $1164.9 \pm 0.2$                              | $8581.3 \pm 0.5$          |
| $7792.7 \pm 0.5$                              | $789.3 \pm 0.2$                               | $8582.0 \pm 0.5$          |
| $8581.9 \pm 0.7$                              |   | $8581.9 \pm 0.7$          |

Figures caption

Fig. 1 - Calibration curve for the Ge(Li) detector.

Fig. 2 - Decay scheme obtained from coincidence measurement  
and (d,p) studies.

Fig. 3 - Decay scheme obtained by the Ritz combination  
principle. The relative probability of the existence  
of the levels, spin and parity are also reported.



$E_x$  (KeV)

$J^\pi$

8583.0 —  $2^+$

2467.2 —  $3^-$

1956.8 —  $2^-$

1950.4 —  $2^+$

1600.4 —  $(1,2)^0$

1163.0 —  $1^+$

780.0 —  $3^+$

0 —  $2^+$

$\text{Cl}^{36}$

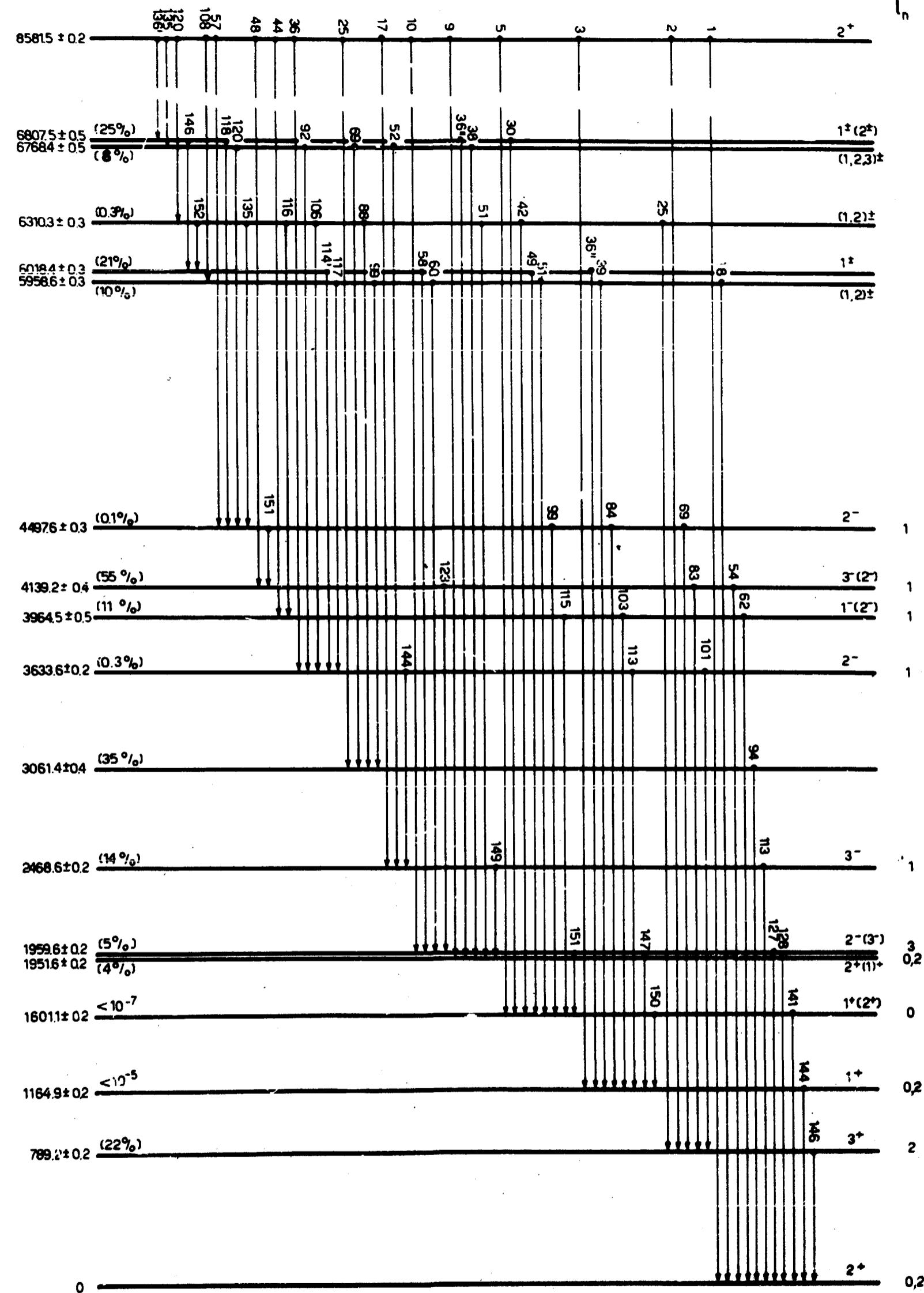


Fig. 3

## Appendix

The computer programs PLOT and PROB have been written in a IBM 7094 FORTRAN language.

The following date are needed for the PLOT program, as shown in fig. 1A.

### First card

Number of levels, numbers of gamma rays, number of regions analysed, multipolarity of  $\gamma$  rays accepted

Format 16 I 5

### Second card

Energy levels with their errors and spin. One level for card

Format 2F 8.3, 7 I 4

### Third card

Gamma rays energy and error. One gamma for card Format 2F 10.3

### Fourth card

Boundary limits of the energy region analysed, step width, spin and parity of probe level.

Format 3F 7.2, 29 X, 7 I 4

We need the same first three cards for the PROB program. The fourth card must contain: boundary limits of the energy region analysed, step width, number of combinations with the

probe level E, number of levels in the energy region  
E-G +E+G, number of steps in G, spin and parity of the probe  
level

Format 2F 7.2, F 6.3, 3 I 10, 7 I 4

The interval G should be large enough to include many  
combinations, so that it gives a good average value.

The FORTRAN of the program PLOT is reported in fig. 2A.

The FORTRAN of the main program of PROB is reported in  
fig. 3A: in fig. 4A and 5A are reported the subroutine PROB  
and POISON.

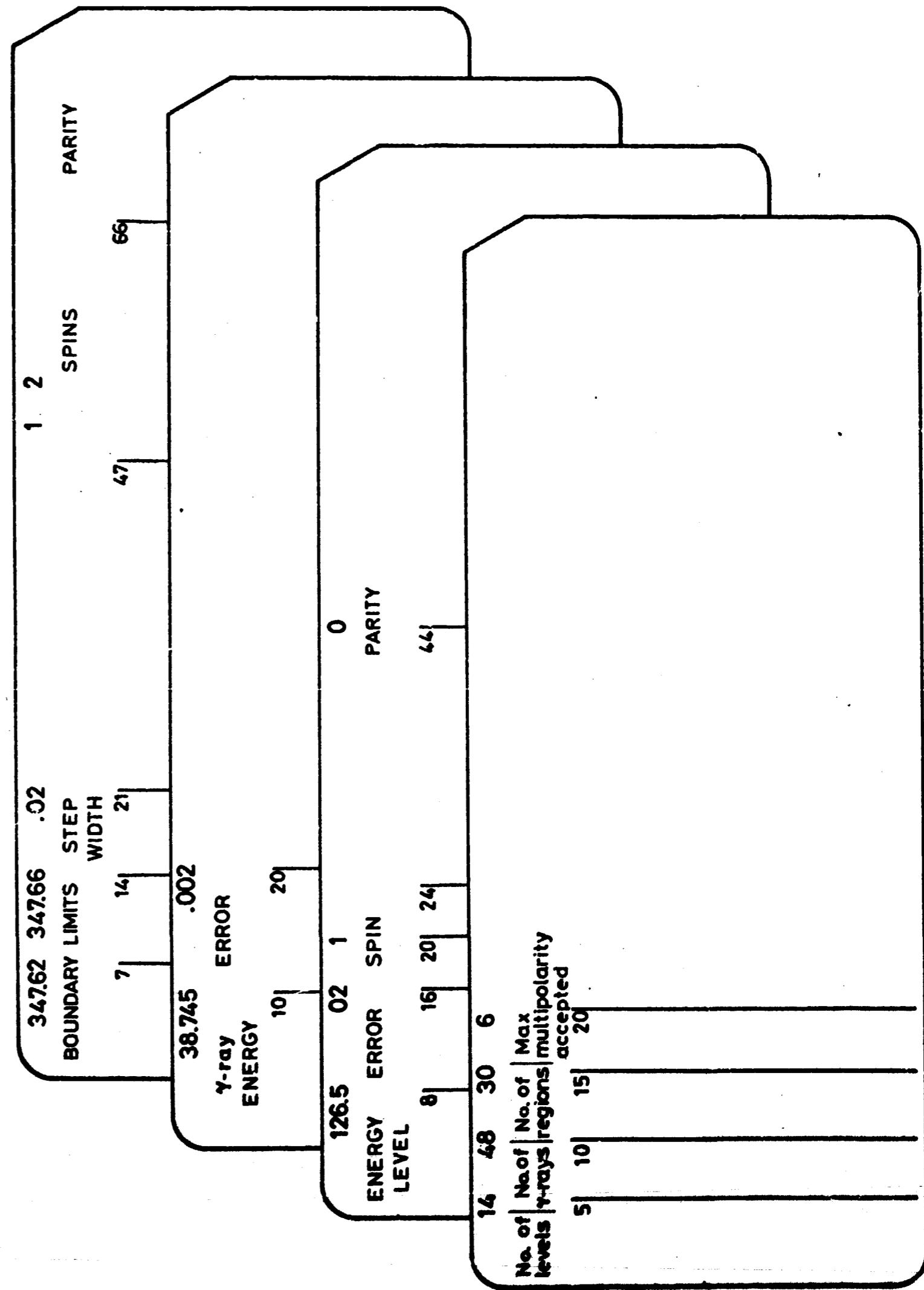


Fig. 1.a

04/01/70

FUTAT - EFN SOURCE STATEMENT - IFN(S) -

```

C GRAFICO NUMERO INCASTRI VS ENERGIA LIVELLO
DIMENSION EN(90),DEN(90),E(250),DE(250),EINF(99),ESUP(99),PASS(99)
DIMENSION IPAR(100),JPAR(100),ISPIN(100,6),JSPIN(100,6)
DIMENSION INK(5000),EEP(5000),KNIF(100),SPA2(30)
READ(5,1111) AST,(SPA2(L),L=1,30)
READ(5,1000) IMAX,KMAX,JMAX,JJ,INDICE,JDELTA,INRINC
READ(5,1002)(EN(I),DEN(I),(ISPIN(I,L),L=1,6),IPAR(I),I=1,IMAX)
READ(5,3001)(E(K),DE(K),K=1,KMAX)
READ(5,1004)(EINF(J),ESUP(J),PASS(J),(JSPIN(J,L),L=1,6),JPAR(J),J=
11,JMAX)
IF(INRINC.NE.0) READ(5,1003) VALRIN
IF(INRINC.EQ.0) GO TO 2
DO 499 K=1,KMAX
499 E(K)=E(K)&E(K)/VALRIN
2 WRITE(6,222) IMAX,JMAX,KMAX
WRITE(6,1005)
WRITE(6,333)(EN(I),DEN(I),(ISPIN(I,L),L=1,6),IPAR(I),I=1,IMAX)
WRITE(6,444)
WRITE(6,1008)(E(K),DE(K),K=1,KMAX)
WRITE(6,1005)
WRITE(6,555)(EINF(J),PASS(J),ESUP(J),(JSPIN(J,L),L=1,6),JPAR(J),J=
11,JMAX)
WRITE(6,7777) INDICE
WRITE(6,100)
100 FORMAT(//8X,7HLIVELLO,9X,88H1 2 3 4 5 6 7 8 9 10 11 12 13
114 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30//)
222 FORMAT(//2X,5HIMAX=,I3,5X,5HJMAX=,I3,5X,5HKMAX=,I3)
333 FORMAT(3(1X,3HLV=,F8.3,4H ER=,F4.2,4H 2I=,6I2,5H PAR=,I1))
444 FORMAT(//2X,22HTRANS GAMMA CON ERRORI)
555 FORMAT(2(1X,8HLIM INF=,F7.2,7H PASSO=,F4.2,5H SUP=,F7.2,6H SPIN=,6
I12,5H PAR=,I2))
1000 FORMAT(16(5)
1001 FORMAT(10F8.3)
1002 FORMAT(2F8.3,7I4)
1003 FORMAT(5F15.3)
1004 FORMAT(3F7.2,29X,7I4)
1005 FORMAT(//)
1008 FORMAT(14F9.3)
1009 FORMAT(12F10.3)
1111 FORMAT(26A3)
2222 FORMAT(3X,F12.3,I4,31A3)
3001 FORMAT(2F10.3)
3333 FORMAT(5X,48HPASSO TROPPO PICCOLO OD INTERVALLO TROPPO GRANDE)
7777 FORMAT(//5X,24HCODICE REGOLA SELEZIONE=,I2)
J=1
5 CONTINUF
LMAX=INT((ESUP(J)-EINF(J))/PASS(J)*1.)
IF(LMAX.GT.9000) WRITE(6,3333)
IND=0
NE=0
IPR=1
DO 234 LF=1,LMAX
EP=EINF(J)&PASS(J)*FLOAT(LF)
41 I=1
49 DELTA=EP-EN(I)

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INDC=0
GO TO 153,50,53,51,53,55,INDICE
50 IF(IPAR(I)&JPAR(J).NE.1) INDC=1
GO TO 53
51 IF(IPAR(I)&JPAR(J).GT.3.OR. IPAR(I)&JPAR(J).EQ.1) INDC=1
53 IF(INDC.EQ.1) JDELT=JDELT+82
DO 54 L=1,10
IFI(JSPIN(I,L)).EQ.0) GO TO 210
DO 54 LG=1,10
IFI(ISPIN(I,LG)).EQ.0) GO TO 54
IFI(ABS(ISPIN(I,LG))-JSPIN(J,L)).LE.JDELT) GO TO 55
54 CONTINUE
55 ABSDEL=ABS(DELTA)
IFI(IND1500,71,75
71 K=1
GO TO 91
75 K=KMF(I)
91 D=ABSDEL-E(K)
F=SQRT(DEN(I)*DEN(I)+DE(K)*DE(K))
C=ABS(D)-F
IFI(C) 140,132,132
132 IF(D)160,160,133
133 K=K81
IFI(K-KMAX)91,91,210
140 NE=NE+1
160 KMF(I)=K-1
IFI(KMF(I))205,205,210
205 KMF(I)=1
210 I=I81
IFI(INDC.EQ.1) JDELT=JDELT-2
IFI(I-IMAX)49,49,230
230 IND=1
232 INK(IPR)=NE
EEP(IPR)=EP
IPR=IPR&1
233 NE=0
234 CONTINUE
IJ=IPR-1
IFI(IJ.LE.?) GO TO 237
DO 236 NU=1,IJ
NNE=INK(NU)
IFI(NNE.LT.JJ.AND.INK(NU81).GE.JJ) GO TO 235
IFI(NNE.LT.JJ.OR.NNE.GT.30) GO TO 236
WRITE(6,2222) EEP(NU),NNE,(SPAZ(K),K=1,NNE),AST
GO TO 236
235 WRITE(6,1005)
236 CONTINUE
237 IPR=1
260 J=J81
WRITE(6,1005)
DO 261 M=1,IMAX
261 KMF(M)=1
IFI(J.LE.JMAX) GO TO 5
400 WRITE(6,100)
500 CONTINUE
STOP

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PROB - EFN SOURCE STATEMENT - IFN(S) -

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C RICERCA NUOVI LIVELLI METODO INCASTRI E CALCOLO PROBABILITA' CHE IL LIVELLO
C SIA CASUALE
COMMON IMAX,KMAX,INKMIN(50),ELV(70),ERRLV(70),EGAM(250),ERRGAM(250)
11,EINF(50),ESUP(50),NUMLV(50),NUMPAS(50)
DIMENSION W(202),INK(202),EEP(202),KLIV(70),KDUP(7C),VV(202,30)
DIMENSION ISPIN(70,6),IPAR(70),JSPIN(50,6),JPAR(50),PASS(50)
DIMENSION KK(202,30),IT(202,30)
READ(5,111) IMAX,KMAX,JMAX,ICODE,JDELT,INRINC
111 FORMAT(16I5)
READ(5,222) (ELV(I),ERRLV(I),(ISPIN(I,L),L=1,6),IPAR(I),I=1,IMAX)
222 FORMAT(F8.3,F8.3,7I6)
READ(5,333) (EGAM(K),ERRGAM(K),K=1,KMAX)
333 FORMAT(2F10.3)
READ(5,444) (EINF(J),ESUP(J),PASS(J),INKMIN(J),NUMLV(J),NUMPAS(J),
1(JSPIN(J,L),L=1,6),JPAR(J),J=1,JMAX)
444 FORMAT(2F7.2,F6.3,3I10,7I4)
IFI(INRINC.EQ.0) GO TO 2
READ(5,555) VALRIN
555 FORMAT(5F15.3)
DO 1 K=1,KMAX
1 EGAM(K)=EGAM(K)+EGAM(K)/VALRIN
2 WRITE(6,666) IMAX,KMAX,JMAX,ICODE,JDELT,INRINC
666 FORMAT(/10X,7HNUM LV=I3,9H NUM GAM=I3,9H NUM INT=I3,14H CODE REG
1SEL=I2,22H INIZ GAM DA TOGLIFRE=I3,9H RINCULD=I2//)
WRITE(6,777) (ELV(I),ERRLV(I),(ISPIN(I,L),L=1,6),IPAR(I),I=1,IMAX)
777 FORMAT(3I1X,3HLV=F8.3,4H ER=F4.2,4H 2I=,6I2,5H PAR=,II)
WRITE(6,888)
888 FORMAT(/2X,28HTRANSIZIONI GAMMA CON ERRORI)
WRITE(6,999) (EGAM(K),ERRGAM(K),K=1,KMAX)
999 FORMAT(14F9.3)
WRITE(6,2222)
2222 FORMAT(/)
WRITE(6,1111) (EINF(J),ESUP(J),PASS(J),INKMIN(J),NUMLV(J),NUMPAS(J),
1,(JSPIN(J,L),L=1,6),JPAR(J),J=1,JMAX)
1111 FORMAT(2X,8HLIM INF=F7.2,9H LIM SUP=F7.2,7H PASSO=F5.3,13H NUM I
INK MIN=I2,21H NUM LIV NELL'INTERV=I2,11H NUM PASSI=I6,4H 2I=6I3,5H
1 PAR=I2)
WRITE(6,2222)
JINF=1
NUMEVN=0
INNLVL=0
J=1
5 CONTINUE
DO 10 M=1,IMAX
10 KLIV(M)=1
KINC=0
LMAX=INT((ESUP(J)-EINF(J))/PASS(J))1.
IFI(LMAX.GT.202) WRITE(6,3333)
3333 FORMAT(10X,48HPASSO TROPPO PICCOLO OD INTERVALLO TROPPO GRANDE)
NE=0
IPR=1
W(1)=0.
15 CONTINUE
DO 120 LF=1,LMAX
EP=FINF(J)*PASS(J)*FLOAT(LF)

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PROB - EFN SOURCE STATEMENT - IFN(S) -
20 i=1
DO 25 M=1,IMAX
25 KDUPI(M)=0
30 DIFF=EP-ELV(I)
INDC=0
GO TO 45,35,45,40,45,55,ICODE
35 IF(IPAR(I)&JPAR(J).NE.1) INDC=1
GO TO 45
40 IF(IPAR(I)&JPAR(J).GT.3.OR.IPAR(I)&JPAR(J).EQ.1) INDC=1
45 IF(INDC.EQ.1) JDELT=JDELT&2
DO 50 M=1,6
IF(JSPIN(J,M).EQ.0) GO TO 80
DO 50 MG=1,6
IF(ISPIN(I,MG).EQ.0) GO TO 50
IF(TABS(ISPIN(I,MG)-JSPIN(J,M)).LE.JDELT) GO TO 55
50 CONTINUE
55 ABSDF=ABS(DIFF)
IF(KIND.EQ.0) GO TO 60
K=1
GO TO 65
60 K=KLIV(I)
AMEZER=ERRLV(I)*ERRLV(I)
65 D=APSDF-EGAM(K)
F=SQRT(AMEZER*ERRGAM(K)*ERRGAM(K))
IF(ABS(D).LT.F) GO TO 85
IF(D) 75,75,70
70 K=K&1
IF(K-KMAX) 65,65,80
75 KLIV(I)=K-1
IF(KLIV(I).LE.0) KLIV(I)=1
80 I=I+1
IF(INDC.EQ.1) JDELT=JDELT-2
IF(I.LE.1MAX) GO TO 30
GO TO 110
85 NE=NE&1
KDUPI(I)=KDUPI(I)&1
V=C*D/(F*F)
IF(KDUP(I).EQ.1) GO TO 90
IF(V.GT.RR) GO TO 100
W(IPR)=W(IPR)&V-RR
NE=NE-1
GO TO 95
90 W(IPR)=W(IPR)&V
95 VV(IPR,NE)=V
RR=V
KK(IPR,NE)=K
II(IPR,NE)=I
GO TO 105
100 NE=NE-1
105 IF(NE.GT.30) WRITE(6,4444) EP
4444 FORMAT(3X,14H PER IL VALORE F9.3,49H TROPPI INCASTRI AUMENTARE DIM
IENSTON DI VV,KK,II)
IF(D.LT.0.01) GO TO 75
KLIV(I)=K
K=K&1
IF(K-KMAX) 65,65,80

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PROB - EFN SOURCE STATEMENT - IFN(S) -
110 KIND=1
INK(IPR)=NE
EEP(IPR)=EP
IPR=IPR&1
115 NE=0
W(IPR)=0.
IF(IPR.GT.202) GO TO 125
120 CONTINUE
125 IJ=IPR-1
NUM=0
WRITE(6,2222)
INCAB=1
DO 130 NU=1,IJ
IF(INK(NU).LT.INKMIN(J)) GO TO 126
NUM=NUM&1
126 CONTINUE
GO TO 127,128,129,INDAB
127 WRITE(6,5555) EEP(NU)
5555 FORMAT(3X,11H DA ENERGIA=F9.3)
INDAB=2
128 IF(INK(NU).NE.INK(NU&1)) INDAB=3
IF(NU.EQ.IJ) GO TO 129
IF(INDAB.EQ.2) GO TO 130
129 WRITE(6,6666) EEP(NU),INK(NU)
6666 FORMAT(26X,16HFIND AD ENERGIA=F9.3,11H INCASTRI=I3)
INDAB=1
130 CONTINUE
IJM=1
MAX=INK(I)
MAXI=0
DO 137 M=2,IJ
IF(INK(M)-MAX) 137,133,131
131 MAX=INK(M)
IJM=M
GO TO 136
133 NNE=INK(M)
DO 135 MU=1,NNE
IF(IT(M,MU).NE.IT(IJM,MU)) MAXI=INK(M)
IJMM=M
135 CONTINUE
GO TO 137
136 IF(INK(M).GT.MAXI) MAXI=0
137 CONTINUE
138 WM=W(IJM)/FLDAT(INK(IJM))
WRITE(6,7777) EEP(IJM),MAX,W(IJM),WM,J
7777 FORMAT(//10X,8HFNRGIA=F9.3,10H INCASTRI=I3,17H SCMMA DF1 DD/FF=F7
1.4,22H (DD/FF)/NUM INCASTRI=F7.4,12H NELL*INT J=I3/)
EARIC=0.
SIGMA=0.
DO 150 MU=1,MAY
III=IT(IJM,MU)
KKK=KK(IJM,MU)
VVV=VV(IJM,VU)
D=ABS(EEP(IJM)-ELV(III))-EGAM(KKK)
F=ERRLV(III)*ERRLV(III)*ERRGAM(KKK)*ERRGAM(KKK)
IF(ELV(III).GT.EEP(IJM)) GO TO 140

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PROB - EFN SOURCE STATEMENT - IFN(S) -

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BARIC=BARIC8(ELV(III)&EGAM(KKK))/F
GO TO 145
140 BARIC=BARIC8(ELV(III)-EGAM(KKK))/F
145 SIGMA=SIGMA81./F
R=SQRT(F)
WRITE(6,8888) III,ELV(III),KKK,EGAM(KKK),D,R,VVV
8888 FORMAT(5X,2H=I3,12H LIV NOTO=F9.3,5H K=I3,14H TRANS GAMMAF9
1.3,5H D=F8.3,5H F=F8.3,9H DD/FF=F8.3)
150 CONTINUE
BARIC=BARIC/SIGMA
SQM=SQRT(1./SIGMA)
WRITE(6,9999) BARIC,SQM
9999 FORMAT(1/20X,19HENERGIA BARICENTRO=F12.4,22H SCARTO QUADRO MEDIO=F
19.4)
IF(MAX1.EQ.C) GO TO 160
MAX=MAX1
IJM=IJMM
MAX1=0
GO TO 138
160 INNULV=INNULV81
NUMEVN=NUMEVNANUM
IF(INNULV.LT.NUMLV(J)) GO TO 165
CALL PROBINUMEVN,JINF,J)
NUMEVN=0
INNULV=0
JINF=J81
165 J=J81
IF(J.LE.JMAX) GO TO 5
STOP
END
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FIT - EFN SOURCE STATEMENT - IFN(S) -

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SUBROUTINE PROB(M,JMIN,JFIN)
COMMON IMAX,KMAX,INKMIN(50),ELV(70),ERRLV(70),EGAM(250),ERRGAM(250
!),EINF(50),ESUP(50),NUMLV(50),NUMPAS(50)
DIMENSION S(70),T(70),LMIN(70),LMAX(70),INE(70),LZ(70)
J=JMIN
G=(EGAM(KMAX)-EGAM(1))/FLOAT(KMAX)
PROBMD=0.
EINCR=25.
ENERG=(EINF(J)&ESUP(J))/2.-25.
NENERG=0
5 I=1
10 S(I)=0.
DELTA=ABS(ENERG-ELV(I))
K=1
IND=0
IF(DELTA-EGAM(K)-G) 15,20,20
15 IF(DELTA-EGAM(K).LT.0.) GO TO 20
IND=1
20 D1=FGAM(K)-DELTA
D2=ABS(D1)
IF(D2-G) 30,30,25
25 IF(D1) 35,35,40
30 S(I)=S(I)&ERRGAM(K)&ERRLV(I)
35 K=K+1
IF(K.LE.KMAX) GO TO 20
40 IF(IND.EQ.0) GO TO 45
GI=(G+DELTA-FGAM(1))/2.
GO TO 55
45 IF(DELTA.GT.EGAM(KMAX)) GO TO 60
IF(DELTA&G.GT.EGAM(KMAX)) GO TO 50
GI=G
GO TO 55
50 GI=(G+D1)/2.
55 S(I)=S(I)/GI
GO TO 65
60 S(I)=0.
65 T(I)=1.-S(I)
I=I+1
IF(I.LE.IMAX) GO TO 10
RUA=1.
DO 70 I=1,IMAX
70 RUA=RUA*T(I)
N=INKMIN(J)
75 SUM=0.
LMIN(1)=1
LMAX(1)=IMAX-N+1
PI=RUA
DO 80 M=1,N
80 INE(M)=0
MU=2
85 LMIN(MU)=LMIN(MU-1)+1
LMAX(MU)=LMAX(MU-1)+1
LL=LMIN(MU-1)
IF(S(LL)) 95,95,90
90 PI=PI*S(LL)/T(LL)
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MAT - EFN SOURCE STATEMENT - IFN(S) -

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GO TO 100
95 INE(MU-1)=2
100 MU=MU81
IF(MU.LE.N) GO TO 85
DO 105 M=1,N
105 LZ(M)=LMIN(M)
INDA=0
DC 110 M=1,N
110 INDA=INDA&INE(M)
IF(INDA.GT.0) GO TO 115
P=PI
MU=N
LL=LZ(MU)
P=P*S(LL)/T(LL)
SUM=SUM+P
115 MU=N
120 IF(LZ(MU).GE.LMAX(MU)) GO TO 125
LMIN(MU)=LMIN(MU)&1
GO TO 100
125 MU=MU-1
IF(MU.LE.0) GO TO 135
LL=LMIN(MU)
IF(S(LL).GT.0.) GO TO 130
INE(MU)=0
GO TO 120
130 PI=PI*T(LL)/S(LL)
GO TO 120
135 WRITE(6,111) ENERG,N,J,SUM
111 FORMAT( /10X,11HALL'ENERGIAF8.2,4H CON12,21H INCASTRI NELL'INT J=1
12,19H LA PROBABILITA' E'E12.7//)
NENERG=NENERG81
PRORMD=PROBMD&SUM
ENERG=ENERG&INCR
IFI(ENERG.LT.ESUP(J)>25.1 GO TO 5
IFI(J.EQ.JFIN) GO TO 140
J=J+1
GO TO 5
140 PROBMD=PROBMD/FLOAT(NENERG)
WRITE(6,222) PROBMD,EINF(JMIN),ESUP(JFIN),NENERG
222 FORMAT( //5X,18HPROBABILITA MEDIA=E12.7,15H FRA LE ENERGIE2F9.3,11H
1 MEDIATA SU13,7H VALORI//)
CALL POISON(PROBMD,M,JMIN)
RETURN
END

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SUBROUTINE POISON(P,NU,J)
COMMON IMAX,KMAX,INKMIN(50),ELV(70),ERRLV(70),EGAM(250),ERRGM(250
1),EINF(50),ESUP(50),NUMLV(50),NUMPAS(50)
ENNE=P*FLOAT(NUMPAS(J))
ENU=ENNE*FLOAT(NUMLV(J))/FLOAT(NU)
PROBFN=0.
PROBNY=0.
EMME=1.
EXPNU=EXP(ENU)
DO 10 M=1,20
FNME=EMME*FLOAT(M)
PR=(ENU**M)/(EXPNU*EMME)
PROBNY=PROBNY+PR
IF(M.LT.NUMLV(J)) GO TO 10
PROBFN=PROBFN+PR
PR=PR*1000.
IF(PR.LT.PROBNY) GO TO 20
10 CONTINUE
20 WRITE(6,111) NU,INKMIN(J),J,FNME,ENU
111 FORMAT( //3X,3HCONT4,18H VGLTE CHE VI SONO12,28H O PIU' INCASTRI NE
ILL'INT J=I3,7H CON N=F9.4,13H NU=N*NU/EMMEF10.7/)
PROBNY=PROBNY*100.
PROBFN=PROBFN*100.
WRITE(6,222) PROBNY
222 FORMAT(3X,49FLA PROBABILITA' CHE UN LIVELLO SIA CASUALE E° DELFI0.
15,10H PER CENTO//)
WRITE(6,333) NUMLV(J),PROBFN
333 FORMAT(3X,20HE QUELLA CHE TUTTI E13,31H I LIVELLI SIANO CASUALI E°
1 DELFI0.5,10H PER CENTO///)
RETURN
END

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