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THE RESOLUTION FUNCTION
FOR THE ROTATING-CRYSTAL SPECTROMETER

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THE RESOLUTION FUNCTION
FOR THE ROTATING-CRYSTAL SPECTROMETER

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The resolution function in the (\vec{Q}, ω) space for the rotating-crystal time-of-flight spectrometer is defined. All the instrumental components bringing a contribution to the uncertainties in the measured energy and momentum transfers are taken into account. A detailed analysis of the monochromator unit transmission, including the Doppler effect influence, is presented. An analytic expression is derived for the resolution function in the Gaussian approximation.

1. INTRODUCTION

During the last years, the resolution function of the thermal neutron spectrometers used in condensed matter studies has been considered by a number of authors. Its analytical expression for a triple axis neutron spectrometer and for a twin-rotor time-of-flight spectrometer was calculated in refs. /1,2,3/ and in /4/, respectively. For the case of the rotating-crystal spectrometer /5/, a time-of-flight resolution function has been discussed by Furrer/6/. This function depends on the measured cross-section, hence it is not defined exclusively by the instrument.

The present paper contains an analytical treatment of the resolution function in the (\vec{Q}, ω) space for the rotating-crystal

spectrometer. All the sources of the uncertainties in the measured momentum and energy transfers have been considered for a particular channel of the time analyser and a given setting. These sources are: the dimensions and the shape of the monochromator crystal, sample and detector, the Doppler effect, the width of the analyser channel, the collimators angular divergences and the monochromator mosaic spread.

The resolution function is defined in sec.2 and the necessary approximations for obtaining an analytical form are given. In sec.3 the transmission function of the monochromator unit is derived. Unlike the equivalent function calculated in ref. /2/, this function depends on the crystal coordinates and on the time also. This dependence is due to the Doppler effect and to the rotation respectively. The Gaussian expression for the resolution function is given in sec.4 in a form suitable for a simple computer program.

2. DEFINITION OF THE RESOLUTION FUNCTION

The layout of a rotating-crystal spectrometer is presented in fig.1. The horizontal and vertical angular divergences of the i -th collimator C_i ($i=1,2,3$) are α_i and β_i respectively. The collimators axes are contained in the horizontal plane. The monochromator crystal, of cylindrical shape with radius r_0 and height z_0 , rotates around a vertical axis contained in a reflecting plane belonging to the most probable mosaic block. Let the coordinate system $(M, \hat{I}, \hat{J}, \hat{K})$ be connected with the crystal in such a way, that the \hat{I} axis is vertical and the \hat{J} axis is normal to the above mentioned reflecting plane. Let $t=0$ be the moment when \hat{I} becom...

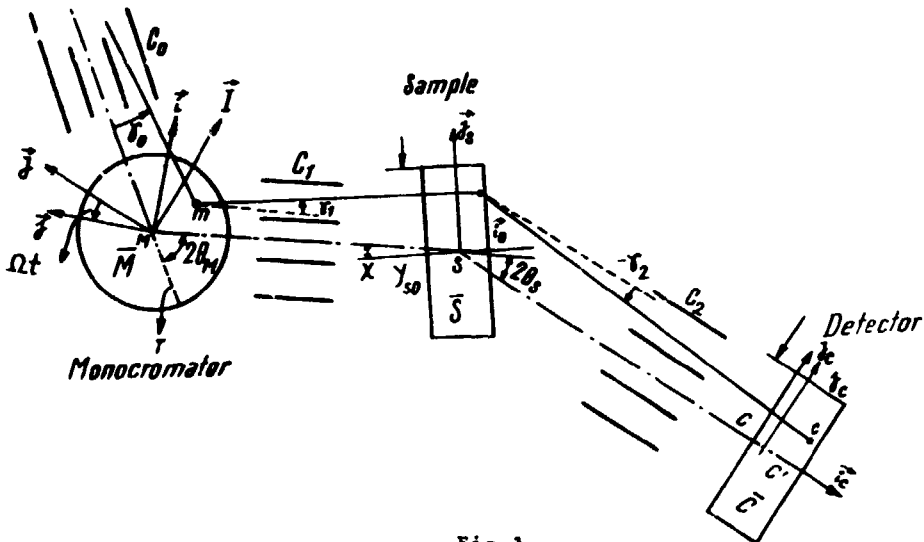


Fig.1.
Layout of the rotating-crystal spectrometer.

external bisectrix of the angle $2\theta_M$ between the axes of the collimators C_0 and C_1 . At $t=0$ the laboratory coordinate system $(M, \vec{I}, \vec{J}, \vec{L})$ coincides with $(M, \vec{i}, \vec{j}, \vec{l})$. The coordinate system for the sample is chosen as in fig.1. The sample is either a rectangular prism of x_{OS}, y_{OS}, z_{OS} dimensions or a cylinder of r_{OS} radius and z_{OS} height. The detector (which consists usually of two rows of cylindrical counters of ρ_0 radius and a total window of dimensions y_{OC}, z_{OC}) is considered, for the sake of simplicity, to be a rectangular prism of effective thickness $x_{OC} = \pi\rho_0$. The detector coordinate systems are $(C, \vec{I}_C, \vec{J}_C, \vec{L}_C)$ and $(C', \vec{I}'_C, \vec{J}'_C, \vec{L}'_C)$, the \vec{I}_C and \vec{I}'_C axes being the same, and the segment $C'C$ being defined by the weight center of the absorption function $\langle x_C \rangle = C'C$. The value of $\langle x_C \rangle$ depends on the mean wavelength corresponding to each time channel. Let us denote MS with L_I and SC with L_{FO} . The segments L_I and $L_p = L_{FO} + \langle x_C \rangle$ are the mean flight paths of the neutrons

before and after the scattering, respectively.

For a given interplanar distance d of the monochromator, and given angles $2\theta_M$ and $2\theta_S$, in the analyser time channel T_0 neutrons will be detected corresponding to the mean scattering process :

$$\vec{Q}_0 = \vec{k}_P - \vec{k}_I \quad (2.1.1)$$

$$\hbar\omega_0 = (\hbar^2/2m)(k_I^2 - k_P^2) \quad (2.1.2)$$

where m is the neutrons mass and

$$k_I = \pi/(d \sin\theta_M) \quad (2.2.1)$$

$$k_P = L_P k_I \sqrt{\hbar k_I T_0 / m - L_I} \quad (2.2.2)$$

The intensity detected in the T_0 channel will be :

$$I(T_0) = I(\vec{Q}_0, \omega_0) = \int R(\vec{Q} - \vec{Q}_0, \omega - \omega_0) \sigma(\vec{Q}, \omega) d\vec{Q} d\omega \quad (2.3)$$

where $\sigma(\vec{Q}, \omega)$ is the cross section of the sample. $R(\Delta\vec{Q}, \Delta\omega)$ is the resolution function of the instrument for a particular time channel $/4/$. It is defined as the probability of detecting neutrons corresponding to the scattering process associated with the particular point $(\vec{Q}_c + \Delta\vec{Q}, \omega_c + \Delta\omega)$ in the (\vec{Q}, ω) space.

Let us assume that a neutron is reflected at the moment t at the point (x, y, z) with a wave-vector $\vec{k}_I + \Delta\vec{k}_I$, is scattered at (x_s, y_s, z_s) with a wave-vector $\vec{k}_P + \Delta\vec{k}_P$ and absorbed at (x'_c, y'_c, z'_c) . The resolution function will be then :

$$R(\Delta\vec{Q}, \Delta\omega) = \frac{1}{|\bar{M}||\bar{S}||\bar{C}|} \int_{\bar{M}} dx dy \int_{\bar{S}} dx_s dy_s \int_{\bar{C}} dx'_c dy'_c \int_{-\infty}^{\infty} dt$$

$$\int d(\Delta\vec{k}_1) d(\Delta\vec{k}_f) P_M(\Delta\vec{k}_1, \vec{r}, t) T_2(\Delta\vec{k}_f) P_C(x'_c, y'_c) P_T(\Delta T) \quad (2.4)$$

$$\delta(\Delta\vec{Q} - \Delta\vec{k}_f + \Delta\vec{k}_1) \delta(k_f \Delta k_f - k_I \Delta k_I + (\hbar/m)\Delta\omega) \delta(y_s - \varphi_1) \delta(y'_c - \varphi_2)$$

The expression (2.4) implies that in a first approximation the resolution function is not affected by the vertical dimensions of the instrumental elements, and that y_s and y'_c are not independent variables. The quantities $|\bar{M}|, |\bar{S}|, |\bar{C}|$ are the areas of the horizontal sections \bar{M}, \bar{S} , and \bar{C} in the monochromator, sample and detector respectively.

The quantity ΔT is given by :

$$\Delta T = T - T_0 \quad (2.5.1)$$

where

$$T_0 = (m/\hbar) (L_I/k_I + L_F/k_F) \quad (2.5.2)$$

T_0 is the moment of detection of a mean neutron reflected at $t=0$ at the point M with a wavevector \vec{k}_I , scattered at S with a wavevector \vec{k}_F and absorbed in C' . The quantity T is given by

$$T = t + (m/\hbar) (L_I/k_I + L_F/k_F) \quad (2.5.3)$$

and represents the moment of detection in the same channel of the neutron under consideration in (2.4).

One can write

$$\Delta T = t + (m/n) (\Delta L_1/L_I + \Delta L_f/L_f - L_I \Delta k_1/k_I^2 - L_f \Delta k_f/k_f^2) \quad (2.6)$$

It is easily found that

$$\Delta L_1 = L_1 - L_I = -\zeta_1 X + \zeta_2 Y + x_s / \cos \chi - \gamma_1 L_I \operatorname{tg} \chi \quad (2.7.1)$$

$$\Delta L_f = L_f - L_P = \xi_1 \cos \theta_M X + \xi_1 \sin \theta_M Y + \xi_1 L_I \gamma_1 - \beta x_s / \cos \chi + x'_c \quad (2.7.2)$$

and also that

$$y_s = \varphi_1 = (\cos \theta_M / \cos \chi) X + (\sin \theta_M / \cos \chi) Y + \gamma_1 L_I \cos \chi - x_s \operatorname{tg} \chi \quad (2.8.1)$$

$$y'_c = \varphi_2 = \xi_2 \cos \theta_M X + \xi_2 \sin \theta_M Y + \gamma_1 L_I \xi_2 + x_s \alpha / \cos \chi + \gamma_2 L_P$$

where

$$\zeta_1 = \sin \theta_M + \operatorname{tg} \chi \cos \theta_M \quad (2.9)$$

$$\zeta_2 = \cos \theta_M - \operatorname{tg} \chi \sin \theta_M$$

$$\alpha = \sin 2\theta_s ; \quad \beta = \cos 2\theta_s \quad (2.10)$$

$$\xi_1 = \alpha + \beta \operatorname{tg} \chi ; \quad \xi_2 = \alpha - \beta \operatorname{tg} \chi \quad (2.11)$$

χ is the angle between the normal to the sample and the incoming beam ($\chi = 0$ when the sample is a cylinder). X, Y are the coordinates of a point (x, y) of the monochromator in the laboratory system. The laboratory system $(M, \vec{I}, \vec{J}, \vec{L})$ is connected with the system $(M, \vec{I}, \vec{J}, \vec{L})$ by the relations :

$$\begin{aligned} X &= x \cos \Omega t - y \sin \Omega t = x \\ Y &= y \cos \Omega t + x \sin \Omega t = y \end{aligned} \tag{2.12}$$

Here was taken into account the fact that the instrument transmits only for small Ωt , due to the existence of the collimators C_0 and C_1 . The quantity $\Omega/2\pi$ is the frequency of the monochromator rotation.

The functions under the integral sign in (2.4) are probability functions, with the following meanings : P_M is the transmission of the monochromator unit (collimators C_0, C_1 and monochromating crystal) T_2 - the transmission of the collimator C_2 , P_C is the probability of absorption in the detector, P_T is the acceptance of the analyser channel. P_M is a convolution between the crystal reflectivity function with the transmission functions of the collimators C_0 and C_1 . These functions have different forms (the crystal reflectivity has a shape given by the mosaic crystal theory, the collimator transmissions are triangular functions, P_T is rectangular with a width $\Delta\tau$, P_C is of the form $\exp(-\mu x_C)$ in the $(0, x_{OC})$ range and zero otherwise). It is reasonable to make use of the Gaussian approximation for each of them, on the grounds that the folding of a large number of functions having arbitrary forms gives a nearly Gaussian.

The Gaussian approximation of the resolution function is obtained by replacing each of the above mentioned functions by a Gaussian of the same dispersion :

$$f_G(x) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left[-\frac{1}{2}\left(\frac{x}{\sigma}\right)^2\right] \tag{2.13}$$

where $\langle x \rangle = 0$ was assumed.

For a triangle of half width at half maximum a one has $a^* = a/\sqrt{6}$, and for a rectangle of width a , $a^* = a/\sqrt{12}$. In the integrals of the following type :

$$I(\dots) = \frac{1}{|\bar{D}|} \int_{\bar{D}} du dv F(u,v,\dots) = \int_{-\infty}^{\infty} du \int_{-\infty}^{\infty} dv \psi(u,v) F(u,v,\dots) \quad (2.14.1)$$

where

$$\psi(u,v) = \begin{cases} \frac{1}{|\bar{D}|} & \text{for } (u,v) \in \bar{D} \\ 0 & \text{otherwise} \end{cases}$$

the function ψ has to be replaced by the Gaussian function having the same covariance matrix :

$$\psi_G = \frac{1}{2\pi a_1^* a_2^*} e^{-\frac{1}{2}(u^2/a_1^{*2} + v^2/a_2^{*2})} \quad (2.14.2)$$

where $\langle u \rangle = \langle v \rangle = 0$ is assumed, and also $\langle uv \rangle = 0$.

If \bar{D} is the circle of radius a , then $a_1^* = a_2^* = a/2$.
 If \bar{D} is a rectangle of sides a_1 and a_2 , then $a_1^* = a_1/\sqrt{12}$ and $a_2^* = a_2/\sqrt{12}$.

3. THE FUNCTIONS P_M AND P_C

Let the vertical and horizontal mosaic spread of the crystal be η . Let be $\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$ the position vector in a

point of the crystal. In the approximation of a weak extinction, after having performed the approximations mentioned in sec.2 for the collimators, for the transmission function of the monochromator unit (for the unity volume of the crystal) one obtains:

$$dP_M = \frac{Q(\vec{r})}{(2\pi)^3 \alpha_0^* \alpha_1^* \beta_0^* \beta_1^*} \exp\left[-\frac{1}{2} \left[\left(\frac{\gamma_0}{\alpha_0}\right)^2 + \left(\frac{\delta_0}{\beta_0}\right)^2 + \left(\frac{\Delta_h}{\eta}\right)^2 + \left(\frac{\Delta_v}{\eta}\right)^2 + \left(\frac{\gamma_1}{\alpha_1}\right)^2 + \left(\frac{\delta_1}{\beta_1}\right)^2 \right]\right] d\delta_0 \quad (3.1)$$

where $Q(\vec{r})$ is the reflectivity of the unit volume and $\alpha_1^* = \alpha_1/\sqrt{6}$ and $\beta_1^* = \beta_1/\sqrt{6}$.

By using relations (9,10,11) from the Appendix one obtains :

$$\gamma_0 = 2(\Delta k_1/k_1) \text{tg}\theta_M + \gamma_1 - 4(m/\eta) \text{tg}\theta_M \sin^2\theta_M \vec{v}\vec{t}_p/\tau^2 \quad (3.2.1)$$

$$\Delta_h = (\Delta k_1/k_1) \text{tg}\theta_M + \gamma_1 - \omega^* - 2(m/\eta) \text{tg}\theta_M \vec{v}\vec{t}_p/\tau^2 \quad (3.2.2)$$

$$\Delta_v = (\delta_1 - \delta_0)/(2 \sin\theta_M) \quad (3.2.3)$$

For Ωt of the order of collimator divergences one can write :

$$\vec{t}_p/\tau = \vec{I} + \Omega t \vec{J} \quad (3.3)$$

$$\vec{v} = -\Omega(\gamma + x\Omega t) \vec{I} + \Omega(x - \gamma\Omega t) \vec{J} \quad (3.4)$$

so that .

$$\omega^* = \Omega t \quad (3.5)$$

$$2(m/\hbar)\vec{v}\vec{r}_p/\tau^2 = -2(m/\hbar)(\Omega y/\tau) \quad (3.6)$$

Putting all these expressions into (3.1) and integrating over δ_0 , one obtains :

$$F_M(\Delta\vec{k}_1, \vec{r}, t) = P_0 \exp \left\{ -\frac{1}{2} \left[\left(\frac{2\Delta k_1/k_I \text{tg}\theta_M + \gamma_1 + 4m\Omega y/(\hbar\tau) \text{tg}\theta_M \sin^2\theta_M}{\alpha_0^*} \right)^2 + \left(\frac{\Delta k_1/k_I \text{tg}\theta_M + \gamma_1 + 2m\Omega y/(\hbar\tau) \text{tg}\theta_M}{\eta} \right)^2 - \Omega t^2 + \left(\frac{\gamma_1}{\alpha_1} \right)^2 + \left(\frac{\delta_1}{\beta_1} \right)^2 + \frac{\delta_1^2}{\beta_0^{*2} + 4\eta^2 \sin^2\theta_M} \right] \right\} \quad (3.7)$$

where

$$P_0 = \frac{Q(\vec{r}) \sin\theta_M}{(2\pi)^{5/2} \eta \alpha_0^* \alpha_1^* \beta_1^* \sqrt{\beta_0^{*2} + 4\eta^2 \sin^2\theta_M}} \quad (3.8)$$

It can be shown that for small enough frequencies one has :

$$Q(\vec{r}) = Q(0) \left(1 + v \frac{m}{\hbar} \frac{\Omega y}{\tau} \right) \quad (3.9)$$

where v depends on θ_M . The second term in (3.9) is of the order of 10^{-2} and therefore may be neglected.

In a first approximation the absorption function will depend only on x_c :

$$P_C(x_c) dx_c = e^{-\mu x_c} (1 - e^{-\mu dx_c}) = \mu e^{-\mu x_c} dx_c \quad (3.10)$$

The function $\tilde{P}_C(x_C) = x_{OC}^{-1} P_C(x_C)$ appearing in the relation (2.4) becomes, when normalized :

$$\tilde{P}_C(x_C) = \mu e^{-\mu x_C} / (1 - e^{-\mu x_{OC}}) \quad (3.11)$$

The quantity μ is the absorption coefficient of the detector. It has a weak and linear dependence on the wavelength of the detected neutron :

$$\mu = ck_f^{-1} = ck_P^{-1} = ck_{FO}^{-1} = c(\hbar k_f T_0 / m - L_I) / L_{FO} \quad (3.12)$$

where c is a constant characterizing the absorbant). The quantities $\langle x_C \rangle$ and $\langle x_C^2 \rangle$ have the following expressions :

$$\langle x_C \rangle = \frac{1}{\mu} - x_{OC} / (e^{\mu x_{OC}} - 1) \quad (3.13.1)$$

$$\langle x_C^2 \rangle = (2/\mu) \langle x_C \rangle - x_{OC}^2 / (\mu^2 x_{OC} - 1) \quad (3.13.2)$$

In order to keep the Gaussian approximation one has to put:

$$\tilde{P}_C(x_C) = \frac{1}{\sqrt{2\pi}\epsilon} \exp\left[-\frac{1}{2}(x_C - x_C')^2 / \epsilon^2\right] = \frac{1}{\sqrt{2\pi}\epsilon} \exp\left[-\frac{1}{2}(x_C' / \epsilon)^2\right] = \tilde{P}_C(x_C') \quad (3.14.1)$$

where

$$\epsilon^2 = \langle x_C^2 \rangle - \langle x_C \rangle^2 \quad (3.14.2)$$

4. DERIVATION OF THE RESOLUTION FUNCTION

Within the approximations of sec.2 and . the resolution function has the expression :

$$R(\Delta\vec{Q}, \Delta\omega) = R'_0 \int d(\Delta\vec{k}_1) d(\Delta\vec{k}_2) \delta(\Delta\vec{Q} - \Delta\vec{k}_2 + \Delta\vec{k}_1) \delta(k_F \Delta k_F - k_T \Delta k_1) + \\ + \pi \Delta\omega / \hbar \exp \left[-\frac{1}{2}(E_1 + E_2) \right] \int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} du_1 du_2 du_3 du_4 du_5 \exp(-E_3/2) \quad (4.1)$$

where

$$R'_0 = \frac{36\sqrt{2}}{5/2} \frac{\chi_{oc}}{c\Delta\tau} \frac{P_0}{|\vec{M}| |\vec{S}| |\vec{C}|} \quad (4.2)$$

(for cylindrical samples $R'_0 \pi \Rightarrow R'_0/3$), and

$$E_1 = a_{73}^2 v_3^2 + a_{11}^2 v_4^2 \quad (4.3.1)$$

$$E_2 = a_{13}^2 \delta_1^2 + a_{14}^2 \delta_2^2 \quad (4.3.2)$$

$$E_3 = \sum_{i,j=1}^5 N_{ij} u_i u_j + 2 \sum_{i=1}^5 c_i u_i + \sum_{i=1}^5 d_i^2 = U' N U + 2C' U + D' E D \quad (4.3.3)$$

$$C = K D ; \quad D = J V \quad (4.4)$$

The quantities a_i ($i=1, 2, \dots, 32$) are given in table I, and the matrices N, K, J in tables II and III. E is the unity matrix, and the vectors U and V are :

$$U = \begin{pmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \end{pmatrix} \equiv \begin{pmatrix} t \\ x \\ y \\ x_B \\ x'_C \end{pmatrix} \quad V = \begin{pmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{pmatrix} \equiv \begin{pmatrix} \Delta k_1 \\ \Delta k_f \\ \gamma_1 \\ \gamma_2 \end{pmatrix} \quad (4.5)$$

Making use of the translation :

$$U = W - N^{-1}C \quad (4.6)$$

one obtains for E_3 :

$$E_3 = W'NW - C'N^{-1}C + D'ED = W'NW + F_4 \quad (4.7)$$

and the last five integrals in (4.1) may be written as (see ref.7) :

$$\int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} du_1 \dots du_5 \exp(-E_3/2) = \exp(-E_4/2) \int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} dv_1 \dots dv_5 \exp\left(-\frac{1}{2} \sum_{i,j=1}^5 N_{ij} v_i v_j\right) = (2\pi)^{5/2} \exp(-E_4/2) / |N|^{1/2} \quad (4.8)$$

where $|N|$ is the determinant of the matrix N .

By using (4.4) one gets for E_4 :

$$E_4 = D'(E - K'N^{-1}K)D = V'FV \quad (4.9)$$

where

$$F = J'(E - K'N^{-1}K)J \quad (4.10)$$

Now, one has to rewrite the elements F_{33} and F_{44} of the matrix F with the aid of E_1 from (4.3) :

$$F_{33}(\text{new}) = F_{33}(\text{old}) + a_7^2 \quad (4.11)$$

$$F_{44}(\text{new}) = F_{44}(\text{old}) + a_{11}^2$$

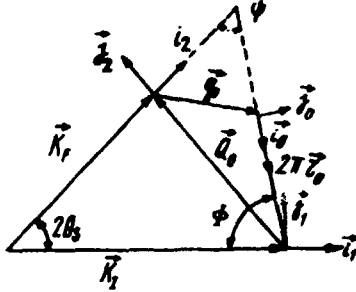


Fig. 2.
Geometry of the scattering process in the reciprocal space.

It remains to carry out the integrals over $\Delta \vec{k}_1$ and $\Delta \vec{k}_F$.
According to fig. 2, one has :

$$\Delta \vec{k}_1 = \Delta k_1 \vec{i}_1 + k_1 \gamma_1 \vec{j}_1 + k_1 \delta_1 \vec{k}_1 = (b \Delta k_1 - a k_1 \gamma_1) \vec{i}_0 + (a \Delta k_1 + b k_1 \gamma_1) \vec{j}_0 + k_1 \delta_1 \vec{k}_0 \quad (4.12.1)$$

$$\Delta \vec{k}_F = \Delta k_F \vec{i}_2 + k_F \gamma_2 \vec{j}_2 + k_F \delta_2 \vec{k}_2 = (-B \Delta k_F - A k_F \gamma_2) \vec{i}_0 + (A \Delta k_F - B k_F \gamma_2) \vec{j}_0 + k_F \delta_2 \vec{k}_0 \quad (4.12.2)$$

$$\Delta \vec{Q} = \Delta Q_x \vec{i}_0 + \Delta Q_y \vec{j}_0 + \Delta Q_z \vec{k}_0 \quad (4.12.3)$$

where $a = \sin \phi$; $b = \cos \phi$; $A = \sin \psi$; $B = \cos \psi$ (4.13)

By taking into account that

$$d(\Delta \vec{k}_1) d(\Delta \vec{k}_F) = k_1^2 k_F^2 d(\Delta k_1) d(\Delta k_F) d\gamma_1 d\gamma_2 d\delta_1 d\delta_2 = k_1^2 k_F^2 dv_1 dv_2 dv_3 dv_4 d\delta_1 d\delta_2 \quad (4.14)$$

and by setting :

$$\Delta Q_x = X_1; \quad \Delta Q_y = X_2; \quad \Delta \omega = X_4 \quad \text{and} \quad \Delta k_{1-v_1} = X_3 \quad (4.15)$$

one obtains for the resolution function :

$$R(\Delta \vec{Q}, \Delta \omega) = \frac{(2\pi)^{5/2} \rho_0 k_I}{|M|^{1/2} k_P} \int_{-\infty}^{\infty} d\delta_1 \int_{-\infty}^{\infty} d\delta_2 e^{-E_2/2} \delta(\delta_2 - \delta_1 - \Delta Q_2/k_P) \\ \int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} dv_1 dv_2 dv_3 dv_4 \left[\prod_{j=1}^4 \delta(v_j - \sum_{j=1}^4 I_{1j} X_j) \right] \exp\left(-\frac{1}{2} \sum_{i,j=1}^4 P_{ij} v_i v_j\right) \quad (4.16)$$

where $\lambda = k_I/k_P$ and :

$$I = \begin{pmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & \lambda & -m/(\pi k_P) \\ B/(ak_I) & -A/(ak_I) & (\lambda - \beta)/(ak_I) & -m/(\pi ak_I k_P) \\ -b/(ak_P) & -A/(ak_P) & (\lambda \beta - 1)/k_P & -m\beta/(\pi ak_P^2) \end{pmatrix} \quad (4.17)$$

The integral over δ_1 and δ_2 from (4.16) becomes :

$$I_1 = (2\pi / (k_P^2 a_{13}^2 + k_I^2 a_{14}^2))^{1/2} k_P \exp - \frac{1}{2} \frac{a_{13}^2 a_{14}^2}{k_P^2 a_{13}^2 + k_I^2 a_{14}^2} (\Delta Q_x)^2 \quad (4.18)$$

and the integrals over v_1, v_2, v_3, v_4

$$I_2 = \int_{-\infty}^{\infty} dx_3 \exp\left(-\frac{1}{2} \sum_{i,j=1}^4 s_{ij} K_i X_j\right) \quad (4.19)$$

where :

$$S = I'FI \quad (4.20)$$

By putting :

$$M_{ij} = S_{ij} - S_{3i}S_{3j}/S_{33} \quad (i,j=1,2,3,4) \quad (4.21)$$

one may write for the integrals I_2 :

$$I_2 = (2\pi/S_{33})^{1/2} \exp\left(-\frac{1}{2} \sum_{i,j=1}^4 M_{ij} X_i X_j\right) \quad (4.22)$$

In this last expression the indices $i,j=3$ are only formal, as from (4.21) it may be seen that $M_{i3}=M_{3j}=0$ for any i and j .

Finally, if one rewrites :

$$\Delta Q_2 = X_3 \quad \text{and} \quad M_{33} = a_{13}^2 a_{14}^2 / (k_F^2 a_{13}^2 + k_I^2 a_{14}^2) \quad (4.23)$$

one obtains the resolution function in the form :

$$R(X_1, X_2, X_3, X_4) = R_0 \exp\left(-\frac{1}{2} \sum_{i,j=1}^4 M_{ij} X_i X_j\right) \quad (4.24)$$

where

$$R_0 = R'_0 \frac{(2\pi)^{7/2}}{a_{13} a_{14}} k_I \left(\frac{M_{33}}{|N|s_{33}} \right)^{1/2} \quad (4.25)$$

It is a Gaussian function in the quadridimensional space (\vec{Q}, ω) . As in ref./2/, the elements $M_{3i} = M_{i3}$ ($i \neq 3$) are zero, so that the resolution in Q_z and the resolution in Q_x, Q_y, ω are independent each of another.

Although (4.24) is an approximation for the resolution function, it accurately gives the center of gravity and the variance of the real function. However, due to the approximation given by (3.14), the most probable value is not given exactly, though it is to be expected that the difference will be small.

Finally, let us mention that from (4.24) one may define a resolution function depending on the time of flight, $R_0(\Delta T)$, in the conditions which are discussed in ref./6/. Generally, this function depends on the scattering cross-section σ , except for the case of a weak dependence of σ on \vec{Q} .

Table I

The expressions of the coefficients a_i . For cylindrical samples the expressions are given in brackets <...> .

$$\begin{aligned}
 a_1 &= 2\sqrt{6} \operatorname{tg}\theta_M / (\alpha_0 k_I) ; & a_2 &= \operatorname{tg}\theta_M / (\eta k_I) ; & a_3 &= -m\sqrt{12} L_I / (\hbar\Delta\tau k_I^2) \\
 a_4 &= -m\sqrt{12} L_P / (\hbar\Delta\tau k_P^2) ; & a_5 &= \sqrt{6}/\alpha_0 ; & a_6 &= 1/\eta ; & a_7 &= \sqrt{6}/\alpha_1 ; \\
 a_8 &= m\sqrt{12} L_I (\xi_1/k_P - \operatorname{tg}\chi/k_I) / (\hbar\Delta\tau) ; & & & & & \langle m\sqrt{12} L_I \xi_1 / (\hbar\Delta\tau k_P) \rangle ; \\
 a_9 &= \sqrt{12} L_I \cos\chi / y_{OS} ; & & & & & \langle 2L_I / r_{OS} \rangle ; & a_{10} &= \sqrt{12} L_I \xi_2 / y_{OC} ; & a_{11} &= \sqrt{6}/\alpha_2 ; \\
 a_{12} &= \sqrt{12} L_P / y_{OC} ; & a_{13} &= \sqrt{6} (\beta_1^{-2} + (\beta_0^2 + 24\eta^2 \sin^2\theta_M)^{-1})^{1/2} ; & a_{14} &= \sqrt{6}/\beta_2 ; \\
 a_{15} &= -\Omega/\eta ; & a_{16} &= \sqrt{12}/\Delta\tau ; & a_{17} &= m\sqrt{12} (\xi_1 \cos\theta_M / k_P - \xi_1 / k_I) / (\hbar\Delta\tau) ; \\
 a_{18} &= 2/r_0 ; & a_{19} &= \sqrt{12} \cos\theta_M / (y_{OS} \cos\chi) ; & & & \langle 2\cos\theta_M / r_{OS} \rangle ; \\
 a_{20} &= \sqrt{12} \xi_2 \cos\theta_M / y_{OC} ; & a_{21} &= 4m\sqrt{6} \Omega \operatorname{tg}\theta_M \sin^2\theta_M / (\hbar\alpha_0 \tau) ; \\
 a_{22} &= 2m\Omega \operatorname{tg}\theta_M / (\hbar\tau) ; & a_{23} &= m\sqrt{12} (\xi_1 \sin\theta_M / k_P + \xi_2 / k_I) / (\hbar\Delta\tau) ; \\
 a_{24} &= 2/r_0 ; & a_{25} &= \sqrt{12} \sin\theta_M / (y_{OS} \cos\chi) ; & & & \langle 2\sin\theta_M / r_{OS} \rangle ; \\
 a_{26} &= \sqrt{12} \xi_2 \sin\theta_M / y_{OC} ; & a_{27} &= -m\sqrt{12} (\beta/k_P - 1/k_I) / (\hbar\Delta\tau \cos\chi) ; \\
 & & & & & & \langle -m\sqrt{12} (\beta/k_P - 1/k_I) / (\hbar\Delta\tau) \rangle ; & a_{28} &= \sqrt{12}/x_{OS} ; & & \langle 2/r_{OS} \rangle ; \\
 a_{29} &= -\sqrt{12} \operatorname{tg}\chi / y_{OS} ; & & & & & \langle 0 \rangle ; & a_{30} &= \sqrt{12} a / (y_{OC} \cos\chi) ; & & \langle \sqrt{12} a / y_{OC} \rangle ; \\
 a_{31} &= m\sqrt{12} / (\hbar\Delta\tau k_P) ; & a_{32} &= 1/\epsilon' .
 \end{aligned}$$

Table II

The symmetrical matrix N_{ij} ($i, j=1, 2, \dots, 5$) ($N_{ij}=N_{ji}$)

$$N_{11} = a_{15}^2 + a_{16}^2; \quad N_{12} = a_{16}a_{17}; \quad N_{13} = a_{15}a_{22} + a_{16}a_{23}; \quad N_{14} = a_{16}a_{27};$$

$$N_{15} = a_{16}a_{31}; \quad N_{22} = a_{17}^2 + a_{18}^2 + a_{19}^2 + a_{20}^2; \quad N_{23} = a_{17}a_{23} + a_{19}a_{25} + a_{20}a_{26};$$

$$N_{24} = a_{17}a_{27} + a_{19}a_{29} + a_{20}a_{30}; \quad N_{25} = a_{17}a_{31};$$

$$N_{33} = a_{21}^2 + a_{22}^2 + a_{23}^2 + a_{24}^2 + a_{25}^2 + a_{26}^2; \quad N_{34} = a_{23}a_{27} + a_{25}a_{29} + a_{26}a_{30};$$

$$N_{35} = a_{23}a_{31}; \quad N_{44} = a_{27}^2 + a_{28}^2 + a_{29}^2 + a_{30}^2; \quad N_{45} = a_{27}a_{31}; \quad N_{55} = a_{31}^2 + a_{32}^2$$

Table III

The matrices $K(5,5)$ and $J(5,4)$

$$K = \begin{pmatrix} 0 & a_{15} & a_{16} & 0 & 0 \\ 0 & 0 & a_{17} & a_{19} & a_{20} \\ a_{21} & a_{22} & a_{23} & a_{25} & a_{26} \\ 0 & 0 & a_{27} & a_{29} & a_{30} \\ 0 & 0 & a_{31} & 0 & 0 \end{pmatrix} \quad J = \begin{pmatrix} a_1 & 0 & a_5 & 0 \\ a_2 & 0 & a_6 & 0 \\ a_3 & a_4 & a_8 & 0 \\ 0 & 0 & a_9 & 0 \\ 0 & 0 & 0 & a_{12} \end{pmatrix}$$

APPENDIX
CHANGE OF ANGULAR DIVERGENCES AND THE ENERGY RESOLUTION AT
REFLECTION FROM ROTATING CRYSTALS

It is well known (see for instance ref./8/) that the Bragg law is modified in the case of a moving crystal. For a perfect crystal, small enough, moving with a velocity \vec{v} , the momentum and energy conservation laws in a reflection process are (in the laboratory system) :

$$\vec{k}_1 = \vec{k}_0 + \vec{\tau} \quad (\text{A.1.1})$$

$$k_1^2 = k_0^2 + (2m/\hbar) \vec{v} \cdot \vec{\tau} \quad (\text{A.1.2})$$

where $\vec{\tau}$ is the reciprocal lattice vector, \vec{k}_0 and \vec{k}_1 are the wave vectors of the neutron before and after reflection. If one denotes the angles before and after reflection by θ_{m0} and θ_{m1} respectively (in the laboratory system), the expressions (A.1) are equivalent with :

$$\tau = 2k_0 \sin\theta_{m0} + (2m/\hbar) \frac{\vec{v} \cdot \vec{\tau}}{\tau} = 2k_1 \sin\theta_{m1} - (2m/\hbar) \frac{\vec{v} \cdot \vec{\tau}}{\tau} \quad (\text{A.2})$$

For given θ_{m0} one obtains :

$$k_0 = \frac{\tau}{(2 \sin\theta_{m0})} \left(1 - 2 \frac{m}{\hbar} \frac{\vec{v} \cdot \vec{\tau}}{\tau^2} \right) \quad (\text{A.3})$$

and in the approximation $(2m/\hbar) \frac{\vec{v}t}{\tau^2} \ll 1$ (A.4)

one obtains :

$$k_i = (1 - 2\frac{m}{\hbar} \frac{\vec{v}t}{\tau^2} \cos 2\theta_{mo}) \tau / (2 \sin \theta_{mo}) \quad (A.5)$$

$$\sin \theta_{mi} = \sin \theta_{mo} (1 + 4\frac{m}{\hbar} \frac{\vec{v}t}{\tau^2} \cos^2 \theta_{mo}) \quad (A.6)$$

which is equivalent with

$$\theta_{mi} = \theta_{mo} + 2\frac{m}{\hbar} \frac{\vec{v}t}{\tau^2} \sin 2\theta_{mo} \quad (A.6')$$

Let us consider now the real crystal in the layout of fig.1. A neutron which passes the C_0 collimator along its axis, and is reflected in the point $\vec{r}=0$ at the momentum $t=0$ on the most probable mosaic block, will have after reflection a wave vector k_I and a direction parallel to the axis of the collimator C_1 . A neutron having the direction (γ_0, δ_0) , reflected at a moment t in a point \vec{r} on a certain mosaic block $\vec{r}(\Delta_h, \Delta_v)$, will have after reflection a wave vector $(k_1, \gamma_1, \delta_1)$. Here $\Delta_h = \vec{r}j/\tau$ and $\Delta_v = \vec{r}l/\tau$. Our purpose is to calculate γ_1, δ_1 and k_1 . Taking into account fig.3 one can write :

$$\theta_{mo} = \theta_M + \Delta_h + \omega^* - \gamma_0 \quad (A.7.1)$$

$$\theta_{mi} = \theta_M - \Delta_h - \omega^* + \gamma_1 \quad (A.7.2)$$

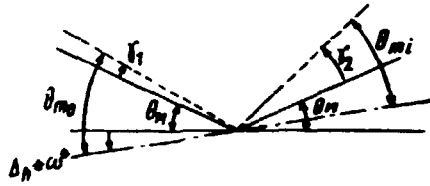


Fig.3.

Geometry of the reflection process in the monochromating crystal in real space.

Here ω^* is the angle between $\vec{\tau}_p$ and the \vec{I} axis. For small values of ω^* one has :

$$\omega^* = \vec{\tau}_p \cdot \vec{I} / \tau \quad (\text{A.8})$$

By subtracting the relations (A.7) and using (A.6') one obtains :

$$\gamma_1 = -\gamma_0 + 2(\Delta_h + \omega^*) + 2\frac{m}{h} \frac{\vec{vI}}{\tau^2} \sin 2\theta_M \quad (\text{A.9})$$

The last term in (A.9) is the contribution of the Doppler effect. This effect does not change the vertical divergence (in a first approximation), therefore :

$$\delta_1 = -\delta_0 + 2\Delta_v \sin \theta_M \quad (\text{A.10})$$

From the relation :

$$\tau = 2k_I \sin \theta_M = 2k_I \sin \theta_{mi} - 2\frac{m}{h} \frac{\vec{vI}}{\tau} \quad (\text{A.11})$$

it follows immediately :

$$\Delta k_1/k_I = (\Delta_n + \omega^* - \gamma_1) \text{ctg} \theta_M + 2 \frac{m}{n} \frac{\vec{v} \vec{T}}{\gamma^2} \quad (\text{A.12})$$

In the relations (A.9) and (A.11) \vec{v} may be replaced by \vec{v}_p , because only the first order terms are retained.

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