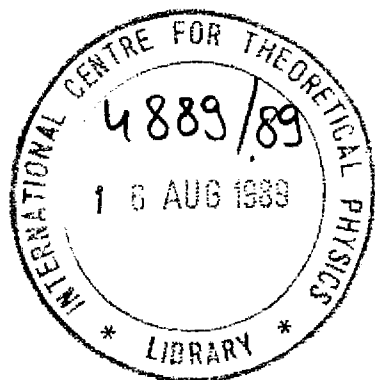


# REFERENCE

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## STUDIES OF THE EFFECT OF AGE ON THE STRUCTURE OF POLYCRYSTALLINE $ReO_3$ \*

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### ABSTRACT

Structural studies of polycrystalline  $H_{0.57}ReO_3$  grown with age of  $ReO_3$  placed in air for  $2\frac{1}{2}$  years, at normal room temperature conditions, are reported.  $H_{0.57}ReO_3$  phase was found to be orthorhombic with space group  $P_{m,m,2}$  and lattice parameters as follows:

$$a_0 = 5.888 \pm 0.003 \text{ \AA}; \quad b = 12.996 \pm 0.002 \text{ \AA}$$

$$c_0 = 5.884 \pm 0.005 \text{ \AA}; \quad \alpha = \beta = \gamma = 90.00$$

$$v = 450.25 \text{ \AA}^3; \quad Z = 6$$

$$D_m = 4.974 \pm 0.032 \text{ gm} \cdot \text{cm}^{-3}; \quad D_x = 5.196 \text{ gm} \cdot \text{cm}^{-3}$$

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## INTRODUCTION

Rhenium trioxide,  $\text{ReO}_3$ , has been thought to be chemically stable compound in air at normal room temperature conditions (1). However, with  $\text{ReO}_3$  single crystal left in the air, a gradual change in the diffraction pattern has been observed and growth of an hydrogen rhenium bronze,  $\text{H}_x\text{ReO}_3$ , has been suggested (2,3). The hydrogen rhenium bronzes are ternary oxide phases which are derived from  $\text{ReO}_3$  by the insertion of the atomic hydrogen. For this purpose various techniques like the cathodic reduction of  $\text{ReO}_3$  in aqueous  $\text{H}_2\text{SO}_4$  (4), the hydrogen spillover methods (5,6), and boiling of  $\text{ReO}_3$  single crystal in water (2,3) etc. have been tried. The structure of the resultant phase seems to be strongly dependent on the amount of hydrogen content present in the  $\text{ReO}_3$  matrix and/or on the method of preparation of the sample. In terms of crystal structure, Dickens and Weller (6) have reported three regions of phase growth as a function of hydrogen content in the  $\text{H}_x\text{ReO}_3$  system. With the hydrogen content increasing, the unit cell symmetry of the resultant compound increased from orthorhombic through tetragonal to cubic (6). Also the amount of the hydrogen intaken by  $\text{ReO}_3$  varies with the method of sample preparation (4,5,6). Such samples have shown contradictory results on other investigations (7,8,9). To the author's knowledge, there is little or no information available about the effect of age and phases etc. thus grown, of polycrystalline  $\text{ReO}_3$ . The present investigations are the first of this kind.

## EXPERIMENTAL

Polycrystalline  $\text{ReO}_3$  was obtained from m/s Alpha Ventron Corp., USA. It was completely crystalline and was at least 99 at%  $\text{ReO}_3$  phase. This was examined using the X-ray diffraction method. The experimental samples were left in air at normal room temperature (298 K) conditions, in a dust free environment, and their X-ray diffraction patterns recorded after regular intervals of

time (approximately 2-3 months). The humidity level in the room was recorded. It ranged from 40-60 at%. The X-ray diffraction data were recorded using a computer controlled powder diffractometer model DMAX-III A of M/S Rigaku Corporation, Japan.  $\text{Cu-K}_\alpha$  radiation ( $\lambda=1.54056 \text{ \AA}$ ), monochromatized by a graphite crystal placed in the diffracted beam, was used and intensities were recorded at 0.02  $2\theta$  steps using a NaI detector. The number of counts were large enough to ensure that the statistical error was less than 1.0 at%. The experimental intensities were corrected for air scattering, polarization of the X-rays, absorption in the specimen and preferred orientation etc. according to the procedures described in Klug and Alexander (10) and Lipson and Steeple (13). The powder X-ray data was indexed using the computer programme ITO (11). The hydrogen content in the samples was determined using the thermogravimetric analysis (TGA) and their density was measured by the Archimede's principle.

## RESULTS AND DISCUSSION

The X-ray diffraction pattern of polycrystalline  $\text{ReO}_3$ , when left in air was found to change gradually with age. The diffraction lines characteristic of cubic  $\text{ReO}_3$  gradually decreased in intensity and several new peaks which were sharp and well separated from those of the mother phase, made their appearance. These peaks grew stronger with the age of the sample. This clearly suggested the growth of a new phase/phases at the expense of the original  $\text{ReO}_3$  phase. Initially these changes were found to be quite rapid but became slow with an age of the sample. In a period of two and half years, the sample was found to contain the  $\text{ReO}_3$  phase to the extent of about 3.5 at% while the remaining had undergone a phase transformation to some new phase/phases. The position of the above mentioned new diffraction peaks did not correspond to any of the compositions in the system hydrogen- $\text{ReO}_3$  and/or water- $\text{ReO}_3$  etc., reported in the literature; suggesting the growth of some new composition. Nevertheless, all these peaks could be indexed on the unit cell in the orthorhombic system. The merit (11,12,13) being 43.5. The X-ray powder data for this new phase/composition

is shown in Table I. The unit cell parameters computed here are as follows.

$$\begin{aligned}a_o &= 5.888 \pm 0.003 \text{ \AA} \\b_o &= 12.996 \pm 0.002 \text{ \AA} \\c_o &= 5.884 \pm 0.005 \text{ \AA} \\ \alpha &= \beta = \gamma = 90.0^\circ\end{aligned}$$

Unit cell volume:

$$V = 450.25 \text{ \AA}^3$$

No. of chemical formula in the unit cell:

$$Z = 6$$

Measured density:

$$D_m = 4.974 \pm 0.032 \text{ gm}\cdot\text{cm}^{-3}$$

X-ray density:

$$D_x = 5.196 \text{ gm}\cdot\text{cm}^{-2}$$

No extinction was observed for the reflections. The space group was determined to be  $P_{mm2}$  (X-ray data also satisfy the conditions of the space group No. 18,  $P_{2,2,2}$ ).

On the basis of the above results and the information obtained from the thermogravimetric analysis (TGA), we could determine the new phase as  $H_{0.57}ReO_3$ , a composition in the  $H_xReO_3$  system. The formation of an hydrogen rhenium bronze in the present case under the effect of water vapor in the air over a length of time is in agreement with the observation of other authors for the single crystal of  $ReO_3(2,3)$ . After 2 1/2 years,  $H_{0.75}ReO_3$  was found to be present in the sample to the extent of about 94 at%.

The powder X-ray diffraction pattern did not reveal any evidence for the presence of any diffraction line below the diffraction angle  $2\theta=16^\circ$ . There were, however, some very weak lines present in the diffraction pattern which could not be indexed on the unit cell parameters of the composition  $H_{0.57}ReO_3$ . But these reflections could be indexed on the unit cell constants reported in Kimizuka et al. (2) and/or Weller and Dickens (5), for a low hydrogen

content phase ( $H_xReO_3$ ;  $x=0.25$  or so:  $a_o=3.77$ ;  $b_o=3.74$  and  $c_o=3.71$ ) The concentration of such a phase was small; being around 1.5 at% or so). Also no evidence for the formation of a superlattice having double the lattice constant of cubic  $ReO_3$  ( $a_o=7.50 \text{ \AA}$ ) was found.

To the author's knowledge as there was no information available in the literature on the unit cell parameters of the composition under present study, therefore, no comparison could be made. Nevertheless, the p-type unit cell observed in the present study for  $H_{0.57}ReO_3$  crystal is in agreement for other compositions in the system  $H_xReO_3$ , having low hydrogen content, reported in Kimizuka et al. (2) and Horiuchi et al. (3).

Also there was no information available on the density of any of the composition in the system  $H_xReO_3$ ; therefore, no comparison could be made.

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TABLE I

Powder X-ray data for  $H_{0.57}ReO_3$  $\Delta\theta^* = 2\theta_{exp} - 2\theta_{calc}$ 

| SR. NO. | $2\theta_{EXP}$<br>(DEGREES) | $L/T_0$ | $d_{EXP}$<br>(Å) | HKL             | $\Delta\theta^*$<br>(DEGREES) |
|---------|------------------------------|---------|------------------|-----------------|-------------------------------|
| 1.      | 16.506                       | 100     | 5.3660           | 110             | +0.011                        |
| 2.      | 25.380                       | 88      | 3.5064           | 121             | -0.012                        |
| 3.      | 25.512                       | 20      | 3.4884           | 031             | -0.007                        |
| 4.      | 27.401                       | 19      | 3.2522           | 040             | -0.028                        |
| 5.      | 30.323                       | 24      | 2.9452           | 200             | -0.012                        |
| 6.      | 31.110                       | 2       | 2.8723           | 012             | -0.034                        |
| 7.      | 33.370                       | 2       | 2.6829           | 220             | -0.016                        |
| 8.      | 34.720                       | 38      | 2.5809           | 211             | -0.007                        |
| 9.      | 34.788                       | 64      | 2.5767           | 112             | -0.035                        |
| 10.     | 35.000                       | 25      | 2.5616           | 141             | -0.007                        |
| 11.     | 37.795                       | 4       | 2.3783           | 150             | -0.008                        |
| 12.     | 40.038                       | 21      | 2.2501           | 231             | -0.004                        |
| 13.     | 41.350                       | 32      | 2.1817           | 240             | +0.002                        |
| 14.     | 43.442                       | 12      | 2.0813           | 202             | -0.007                        |
| 15.     | 46.757                       | 8       | 1.9412           | 310             | -0.014                        |
| 16.     | 47.257                       | 25      | 1.9218           | 161             | -0.012                        |
| 17.     | 49.208                       | 23      | 1.8502           | 251             | -0.014                        |
| 18.     | 51.005                       | 33      | 1.7891           | 123,130         | -0.005                        |
| 19.     | 51.560                       | 5       | 1.7711           | 170             | -0.014                        |
| 20.     | 52.339                       | 16      | 1.7528           | 242             | -0.013                        |
| 21.     | 56.287                       | 5       | 1.6331           | 102,203         | -0.013                        |
| 22.     | 56.589                       | 1       | 1.6281           | 080,252         | -0.021                        |
| 23.     | 56.765                       | 14      | 1.6204           | 312,213         | -0.018                        |
| 24.     | 58.914                       | 6       | 1.5663           | 350,081         | -0.002                        |
| 25.     | 60.537                       | 11      | 1.5282           | 312             | -0.02                         |
| 26.     | 61.001                       | 11      | 1.5177           | 271             | -0.017                        |
| 27.     | 63.136                       | 4       | 1.4714           | 004             | -0.018                        |
| 28.     | 65.565                       | 10,5    | 1.4226           | 280,082         | -0.015                        |
| 29.     | 65.740                       | 5       | 1.4193           | 411             | +0.01                         |
| 30.     | 66.122                       | 10      | 1.4122           | 361,163         | -0.004                        |
| 31.     | 66.628                       | 1,5     | 1.4025           | 190             | -0.029                        |
| 32.     | 67.726                       | 5       | 1.3824           | 352,253,182,281 | -0.010                        |
| 33.     | 69.205                       | 15      | 1.3564           | 431,134,123     | -0.012                        |
| 34.     | 69.643                       | 3       | 1.3489           | 370,073         | -0.012                        |
| 35.     | 70.138                       | 8,5     | 1.3408           | 440,044         | -0.010                        |
| 36.     | 71.637                       | 9,6     | 1.3163           | 402,204         | -0.006                        |
| 37.     | 73.965                       | 7       | 1.2804           | 282,054         | +0.006                        |
| 38.     | 74.946                       | 6,4     | 1.2661           | 271,172         | +0.002                        |
| 39.     | 76.020                       | 5,5     | 1.2509           | 154,083         | +0.008                        |
| 40.     | 76.784                       | 6,3     | 1.2403           | 110,1           | +0.016                        |
| 41.     | 77.860                       | 4,3     | 1.2258           | 273,377         | -0.002                        |
| 42.     | 78.322                       | 12      | 1.2198           | 244,442         | -0.008                        |
| 43.     | 81.800                       | 6,7     | 1.1765           | 005,104         | -0.028                        |
| 44.     | 82.500                       | 2       | 1.1681           | 363             | -0.001                        |
| 45.     | 82.725                       | 1       | 1.1656           | 210,1,1,10,2    | -0.024                        |
| 46.     | 82.950                       | 1       | 1.1610           | 390             | +0.006                        |
| 47.     | 83.388                       | 1,4     | 1.1580           | 025,324         | -0.008                        |
| 48.     | 85.365                       | 12,6    | 1.1362           | 125             | -0.001                        |
| 49.     | 89.895                       | 5,8     | 1.0903           | 084,480         | -0.005                        |
| 50.     | 91.191                       | 1       | 1.0782           | 522,1,1,1,2     | +0.008                        |
| 51.     | 91.240                       | 1,5     | 1.0777           | 1,1,1,2,225     | +0.01                         |
| 52.     | 91.85                        | 6       | 1.0721           | 055,154         | -0.005                        |
| 53.     | 92.632                       | 7       | 1.0597           | 0,12,1,1,12,0   | -0.003                        |
| 54.     | 93.247                       | 3       | 1.0494           | 235,532         | -0.022                        |
| 55.     | 95.521                       | 2       | 1.0004           | 404             | +0.009                        |
| 56.     | 97.802                       | 7,8     | 1.0232           | 284             | +0.044                        |
| 57.     | 98.316                       | 6,4     | 1.0182           | 165             | +0.033                        |
| 58.     | 98.626                       | 6,4     | 1.0158           | 481,0,12,2      | -0.08                         |
| 59.     | 99.179                       | 1       | 1.0116           | 434,0,1,1,3     | -0.042                        |
| 60.     | 101.152                      | 5,7     | 0.9972           | 125,1,1,1,3     | +0.021                        |
| 61.     | 101.592                      | 3,5     | 0.9940           | 174,075,473,506 | +0.012                        |
| 62.     | 102.018                      | 3       | 0.9910           | 444             | -0.016                        |
| 63.     | 102.797                      | 2       | 0.9856           | 1,13,0,0,13,1   | -0.007                        |
| 64.     | 105.793                      | 1,5     | 0.9645           | 116             | +0.021                        |
| 65.     | 108.899                      | 2       | 0.9479           | 0,12,3          | +0.023                        |
| 66.     | 109.782                      | 2       | 0.9416           | 275             | +0.022                        |
| 67.     | 110.290                      | 4       | 0.9387           | 046             | +0.027                        |
| 68.     | 111.790                      | 2       | 0.9303           | 208             | +0.024                        |
| 69.     | 114.312                      | 1       | 0.9168           | 0,14,1          | +0.020                        |
| 70.     | 114.735                      | 2,5     | 0.9147           | 365             | +0.035                        |
| 71.     | 115.235                      | 2       | 0.9121           | 095             | +0.021                        |
| 72.     | 116.357                      | 1       | 0.9065           | 154             | +0.010                        |
| 73.     | 117.915                      | 1,5     | 0.8990           | 435             | +0.024                        |
| 74.     | 118.901                      | 2,8     | 0.8944           | 246             | -0.003                        |
| 75.     | 123.208                      | 1,7     | 0.8756           | 613,2,14,1      | -0.004                        |
| 76.     | 124.164                      | 1       | 0.8717           | 592             | -0.026                        |
| 77.     | 126.516                      | 5,4     | 0.8625           | 1,12,4,1,10,5   | +0.049                        |
| 78.     | 127.249                      | 1,5     | 0.8596           | 336             | +0.005                        |
| 79.     | 127.811                      | 1       | 0.8576           | 583             | -0.040                        |
| 80.     | 133.193                      | 1       | 0.8393           | 710             | +0.018                        |
| 81.     | 139.955                      | 6,2     | 0.8252           | 017             | -0.009                        |

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