

## Initial Operating Experience with the Auxiliary Accelerating Cavity for the TRIUMF Cyclotron

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### Abstract

A 92 MHz auxiliary accelerating cavity has been installed in the TRIUMF cyclotron. It operates at the fourth harmonic of the dee frequency with a planned peak voltage of 150 kV. At full power it will almost double the present energy gain per turn in the 400-500 MeV range, reducing by 25% the stripping loss of the  $H^-$  beam. Low current beam tests have been conducted at voltages of up to 90 kV and a maximum voltage of 145 kV has been attained. The cavity has also been used to flattop the integrated energy gain per turn. A description of the cavity design and a summary of the operating experience is given.

### I INTRODUCTION

The 500 MeV TRIUMF cyclotron routinely accelerates 150  $\mu$ A of  $H^-$  ions. Electromagnetic stripping, rising rapidly from 400 MeV, is responsible for  $\sim 1/2$  of the total particle losses and  $\sim 2/3$  of the total activation of the cyclotron. The use of additional accelerating cavities was suggested as early as 1983 [1], primarily to aid in improving the extraction efficiency for  $H^-$  extraction for injection into a KAON Factory [2]. However, even after another method of improving extraction efficiency was chosen [3], the increased energy gain per turn and consequent reduction in the number of turns, hence losses, in the outer radial region were sufficient motivation to design, manufacture and install one cavity.

The cavity operates at the fourth harmonic (92.24 MHz) of the main rf frequency and consists of a trapezoid of dimension  $\lambda/4$  radially and  $\beta\lambda/2$  azimuthally, so that the orbiting ion receives two acceleration impulses on each passage (Fig 1). The peak accelerating voltage rises sinusoidally with radius, covering the energy range from 370-520 MeV. The maximum energy gain per turn will increase from the present 320 keV to 620 keV.

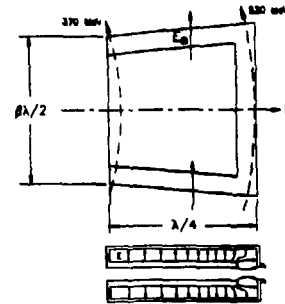


Figure 1: Schematic view of the cavity.

### II. CAVITY AND AMPLIFIER DESIGN

The cavity has been described elsewhere [4]. Briefly, it consists of two halves (Fig. 2), placed above and below the beam plane, separated by 64 mm and mounted independently from the vacuum chamber floor and lid to minimize activation. All conducting walls defining the rf boundaries are made from 1.6 mm thick OFHC Cu sheets with most seams TIG welded, and then brazed together. The cantilevered hot arm is exceptionally stiff ( $\sim 220$  N/mm) to minimize tip vibrations ( $2.7 \mu$ m p-p @ 20 Hz). Cooling circuits were designed to limit the temperature rise from the skin losses (up to  $8.5$  W/cm<sup>2</sup>) to below 25°C. Coarse frequency adjustment is done on assembly by shimming the hot arm to ground arm distance. Fine tuning is provided by a water cooled, hinged flap, built into each ground arm, actuated through a zero backlash linkage system. Each cavity half can be remotely installed in  $\sim 20$  min.

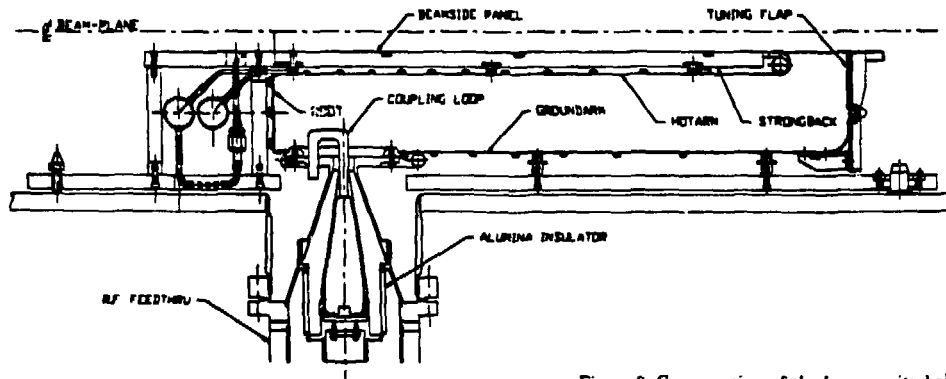


Figure 2: Cross section of the lower cavity half.



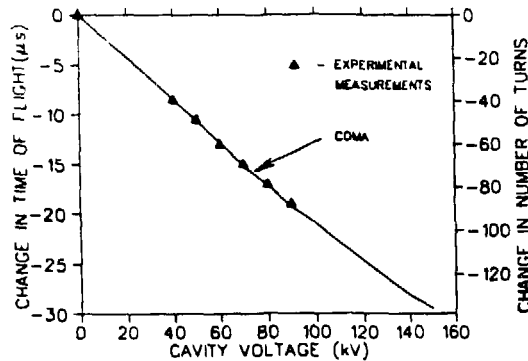


Figure 4 The reduction in the measured time-of-flight (TOF) of the beam through the cyclotron to 500 MeV for various cavity voltages is compared to the results of a computer simulation using the matrix code COMA [6]. The reduction in number of turns is also shown. (Without the cavity the beam makes  $\sim 400$  turns in the cavity region.)

Lower voltages were used to investigate the use of the cavity in flattopping the energy gain per turn. In an isochronous cyclotron the TOF is dependent on the energy gain per turn and the degree to which the magnetic field is isochronous. The time-variation of the fundamental accelerating field is responsible for a cosine-like phase dependence in the energy gain per turn, and hence the TOF is also affected. This variation in the TOF with phase can be reduced substantially, producing a flattopping effect, by adding a higher harmonic cavity opposed to the fundamental. The higher the harmonic number of the cavity, the narrower would be the resultant flattop. The cavity voltage determines the number of turns through the cavity necessary to reach the optimum flattop condition.

For the test the initial beam phase width (23 MHz) was reduced from the nominal  $30^\circ$  used for high current oper-

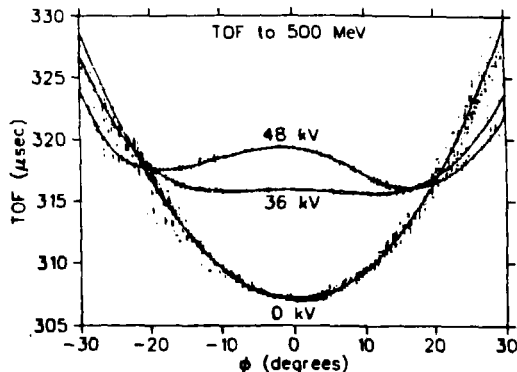


Figure 5 Measured TOF values to 500 MeV as a function of the initial phase for three different cavity settings, 0 kV, 36 kV and 48 kV, with the cavity phased to oppose the fundamental. Smooth curves are plotted through the experimental data points.

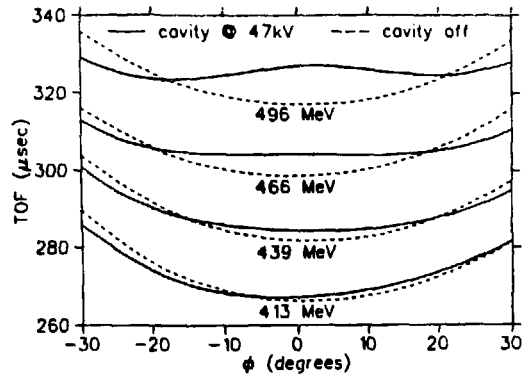


Figure 6: Measured then smoothed TOF curves for four different energies as a function of initial phase for cavity off (dashed curve) and cavity on at 47 kV (solid curve). The cavity was phased to give the best flattop at 466 MeV.

ation, to  $5^\circ$  by inserting radial slits in the centre region. The position of the phase-band with respect to the accelerating field was then altered by scanning the rf frequency, and the TOF was recorded. In Fig. 5 the measured TOF values to 500 MeV are plotted as a function of initial phase for various cavity voltages. At 36 kV an optimal flattop occurs over a phase range of  $\sim 30^\circ$ . The slightly asymmetric result at 48 kV shows the effect of the cavity field being slightly out of phase with respect to the fundamental, prior to optimization.

The cavity was then powered to 47 kV and phased to give the optimum TOF flattop at an energy of 466 MeV. At this setting the TOFs to various other energies were also recorded (Fig. 6). Cavity on results are compared with the corresponding cavity off data. The figure shows how the cumulative effects of the opposing cavity field produce optimal flattopping at only one energy. The variations in the phase of the minimum TOF are due to radial variations in the cyclotron isochronism.

## VI. REFERENCES

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