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Evaluation of Nuclear Data of "Pu and "Pu

Tsunco NAKAGAWA and Valentin A. KONSHIN*

Department of Reactor Engineering Tokai Research Estabilshment Japan Atomic Energy Research Institute Tokai-mura, Naka-gun, Ibaraki-ken

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The evaluation of nuclear data for "Pu and "Pu was made in the neutron energy region from 10^{-1} eV to 20 MeV. For the both nuclides, the total, elastic and inelastic scattering, fission, capture, (n, 2n) and (n, 3n) reaction cross sections were evaluated on the basis of theoretical calculation. The resonance parameters were given for "Pu. The angular and energy distributions of secondary neutrons were also estimated for the both nuclides. The results were compiled in the ENDF-5 format and will be adopted in JENDL Actinoid File.

Keywords: Nuclear Data, Plutonium-244, Plutonium-237, Evaluation, JENDL Actinoid File, ENDF Format.

^{*}Research Fellow (October 1993-April 1995)

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²⁴⁴Puと²⁵⁷Puの核デーク評価

日本原子力研究所東海研究所原子伊工学部 中川 庸雄・Valentin A. KONSHIN*

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中性子エネルギー10⁻eV ~ 20MeVにおける²⁴⁴P u と²³⁷P u の核デーク評価を行った。理論計算 をもとに、両核種の全断面積、弾性散乱と非弾性散乱断面積、核分裂断面積、捕獲断面積及び (n, 2n)と(n, 3n)反応断面積を評価した。²⁴⁴P u に対しては、分離共鳴パラメークを評価 した。また、反応後に放出される二次中性子の角分布とエネルギー分布も推定した。結果は、 ENDF=5フォーマットで編集されており、JENDLアクチノイドファイルに採用される予 定である。

東海研究所:〒319-11 茨城県那珂都東海村白方白根2-4 * リサーチフェロー(1993年10月~1995年4月)

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1. Introduction

Nuclear data of minor actinoids are important for the fuel cycle study. In Japan, OMEGA project is being promoted to study a way of management of high level waste from nuclear energy plants. It is needed to precisely estimate the amount of minor actinoids in the reactors. A TRU burner reactor¹⁾ is one of options for transmutation of minor actinoids to other nuclides with shorter half-life or stable nuclides. This reactor will have a harder neutron spectrum, and large amount of minor actinoids will be loaded in the reactor. Therefore accurate nuclear data are required even for minor actinoids. To meet the requirement for the minor actinoid nuclear data, "JENDL Actinoid File"²⁾ is under preparation at the Nuclear Data Center in Japan Atomic Energy Research Institute. In this file, evaluated neutron induced reaction data will be provided for about 90 nuclides including main nuclides (²³²Th, ²³³U, ²³⁸U, ²³⁹Pu, ²⁴⁰Pu and ²⁴¹Pu) and minor actinoids with a half-life longer than 1.0 day. In the present work, the nuclear data evaluation was made for ²⁴⁴Pu and ²³⁷Pu in order to store the data in the JENDL Actinoid File.

The nuclide ²⁴⁴Pu disintegrates with the half-life of 8.26×10^7 years and ²³⁷Pu with the half-life of 5.17 days. The nuclide ²⁴⁴Pu decays with α emission of 99.875 % and spontaneous fission of 0.125 %. In the case of ²³⁷Pu, the α decay is only 0.0033 % and the rest is the electron capture. Evaluated data for the both nuclides are available in ENDF/B-VI³⁾ and JEF-2.⁴⁾ However the same data are stored in the both files because they adopted the data from the evaluation made by Mann et al.⁵⁾ for ENDF/B-V. Experimental data exist only for the fission cross section and resonance parameters of ²⁴⁴Pu as is described in Chapter 2. The present evaluation of nuclear data of ²⁴⁴Pu is described in Chapter 2, and that of ²³⁷Pu in Chapter 3. The results of the present work have been compiled in the ENDF format, and will be adopted in the JENDL Actinoid File.

2. Evaluation of ²⁴⁴Pu Data

2.1 Resonance parameters

Auchampaugh et al.⁶⁾ measured the fission cross section by using a nuclear explosion (Physics 8) as a neutron source, and obtained information on the resolved resonance parameters below 285 eV. They used the TOF method with a flight path of 245.45 m and a Pu oxide sample with 99.06 % ²⁴⁴Pu, and deduced the capture areas for the 13 levels.

Their results were adopted in the recommendation made by Mughabghab⁷. In the present work, the recommendation of Mughabghab was used by assuming an average capture width of 20 meV. The fission width was determined so as to reproduce the integrated fission cross sections around each resonance peak measured by Auchampaugh et al. The numerical data were taken from EXFOR.⁸ Thus obtained fission widths are almost 1/1000 of the capture widths, but for some resonances the ratio is quite different from 1/1000. The results are listed in Table 2.1. All the levels were assumed to belong to s-wave resonances. The effective scattering radius of 9.33 fm was obtained from the shape elastic scattering cross section calculated with the optical model. The Breit-Wigner multi-level formula was applied. The fission cross section calculated from the resonance parameters are compared with the experimental data of Auchampaugh et al. in Fig. 2.1.

Thermal cross sections and resonance integrals are listed in Table 2.2. In the calculation of resonance integral, integration was made between 0.5 eV and 20 MeV considering cross sections above the resonance region. The thermal capture cross section obtained from the resonance parameters is in good agreement with the experimental data. However the calculated resonance integral of capture cross section is larger than the experiments. ENDF/B-VI gives too large capture resonance integral. For the fission cross section, no experimental data are existing at the thermal energy and for the resonance integral.

2.2 Cross sections above Resonance Region

2.2.1 Theoretical calculation

In the energy region above 290 eV, experimental data exist only for the fission cross section. Therefore, the fission cross section was determined mainly on the basis of the experimental data and the other cross sections were taken from theoretical calculations with ECIS⁹⁹, STAPRE¹⁰⁹ and CASTHY¹¹⁹ to obtain a complete set of the cross sections up to 20 MeV.

ECIS_Calculation

The code ECIS was used for the calculation of the total cross section, the shape elastic scattering cross section, angular distributions of elastically scattered neutrons and of the direct component of the inelastic scattering cross section. The deformed optical potential parameters used in the present work have the following values:

$V_{\rm R} = 46.03$ -	- ().3Ē,	$0 \le E \le 20 \text{ MeV}$
$W_D^{surf} =$	3.05 + 0.4E,	$0 \le E \le 10 \text{ MeV}$
	7.05 - 0.082(E-10),	$10 \le E \le 20 \text{ MeV}$
$W_V^{vol} = 8.0 \times$	$\{1+\exp[-(E-50)/10]\}^{-1},$	$0 \le E \le 20 \text{ MeV}$
$V_{so} = 6.2$		
$r_{\rm R} = 1.26,$	$a_{\rm K} = 0.63$	
r _D = 1.26,	a _D = 0.52	
$r_{\rm SO} = 1.12,$	$a_{so} = 0.47$	
$\beta_2 = 0.204,$	$\beta_4 = 0.051$	

These parameters were determined by Konshin considering Refs. 12 and 13. The introduction of the volume absorption term seems to lead to a better agreement with actinide experimental data for the total cross section in the energy region around 20 MeV and for the angular distributions of the inelastically scattered neutrons on low lying levels.

The ECIS calculation was made in the energy range from 10 keV to 20 MeV.

STAPRE Calculation

The STAPRE code was used for calculations of the fission cross section, (n,2n) and (n,3n) reaction cross sections and the total inelastic scattering cross section. The neutron transmission coefficients for these calculations were obtained using the ECIS code. The level densities were calculated with a phenomenological model proposed by Ignatyuk et al.¹⁴⁾ taking into account shell, superfluid and collective effects. The hard component of neutron scattering spectra was parameterized using the experimental data for ²³⁸U in the 6 - 14.7 MeV region and the matrix element for the pre-equilibrium reaction stage description M² = 10/A³ MeV².

The most critical values for a good description of experimental data on the fission cross section within the framework of the model used in STAPRE are reliable neutron transmission coefficients, a tested pre-equilibrium neutron emission contribution and fission barrier parameters. The fission barrier parameters E_f^A and E_f^B used were the following:

.

nuclide	E [∧] (McV)	E ^B (McV)
²⁴⁵ Pu	5.75	5.4()
²⁴⁴ Pu	5.5()	5.2()
²⁴³ Pu	6.00	5.7()
²⁴² Pu	5.60	5.35

The discussions on the fission barrier parameters are given elsewhere.⁽⁵⁾

CASTHY_Calculation

The ECIS code dose not consider the compound process, and the STAPRE code does not calculate inelastic level excitation cross sections. Therefore, the cross sections due to the compound process were calculated by using a statistical model code CASTHY. The optical potential parameters used are the following ones.¹⁶

$$V_{R} = 45.036 - 0.3 \text{ E (MeV)}, \qquad r_{R} = 1.256, \qquad a_{R} = 0.626 \text{ (fm)}$$
$$W_{D} = 4.115 + 0.4 \text{ E (MeV)}, \qquad r_{D} = 1.260, \qquad a_{D} = 0.555 + 0.0045 \text{ E (fm)}$$
$$V_{SO} = 7.5 \text{ (MeV)}, \qquad r_{SO} = 1.256, \qquad a_{SO} = 0.626 \text{ (fm)}$$

The level density parameters for Gilbert-Cameron's formula were determined from average level spacing of measured resonances⁷) and staircase plots of low-lying excited levels taken from ENSDF. Paring energies were assumed as follows¹⁷):

δ =	2×12/√A	for even-even nuclides,
	12/ √A	for odd nuclides,
	0.0	for odd-odd nuclides.

Other parameters of level density were determined so as to reproduce the staircase plot of excited levels. Obtained results are given in Table 2.3. The level scheme of ²⁴⁴Pu listed in Table 2.4 was adopted from ENSDF (Evaluated Nuclear Structure Data File).

In the CASTHY calculation, the fission, (n,2n) and (n,3n) reaction cross sections were considered as competing processes.

2.2.2 Compilation of cross section data

These results of the theoretical calculations were compiled as follows in the ENDF-5 format.

1) Total Cross Section

Above 10 keV, the ECIS calculation was adopted. Below 10 keV, it was obtained as

a sum of the fission, capture and elastic scattering cross sections.

2) Elastic Scattering Cross Section

Above 4.5 MeV, the ECIS calculation was adopted. Between 10 keV and 4.5 MeV, the cross section was obtained by subtracting a sum of partial cross sections from the total cross section. In the low energy region, the present ECIS calculation gives too small elastic scattering cross sections since the compound elastic process is not included in the calculation. Below 10 keV, the cross section was assumed to be a constant value of 13.36 b which was the value obtained at 10 keV by subtraction of partial cross sections from the total cross section.

3) Inelastic Scattering Cross Sections

The cross sections due to the compound process were calculated with CASTHY. The contributions from the direct process were calculated with ECIS and added to the CASTHY results. The continuum inelastic scattering cross section calculated with CASTHY was too large in the energy region above 4.5 MeV because the optical model parameters used in the CASTHY calculation were not perfectly consistent with those for the ECIS calculation. The continuum inelastic scattering cross section in this energy range was replaced with the values obtained by subtracting a sum of the elastic and direct inelastic scattering cross section, fission, (n,2n), (n,3n) and capture cross sections from the total cross section calculated with ECIS.

The consistency of cross sections were kept by adopting adjusted values for the elastic scattering cross section in the energy range below 4.5 MeV, and by the continuum inelastic scattering cross section above 4.5 MeV.

4) (n,2n) and (n,3n) Reaction Cross Sections

They were calculated with STAPRE. The (n,4n) reaction cross section was ignored because its threshold energy of 17.44 MeV is high and the cross section is not important for the fuel cycle study.

5) Fission Cross Section

There are six sets of experimental data.

Auchampaugh_ct_al.⁶⁾

They measured the fission cross section relative to the ${}^{6}Li(n,t)$ and ${}^{235}U$ fission cross sections in the neutron energy region from 20 eV to 10 MeV by using a nuclear explosion as a neutron source. Their analysis of resonance parameters were adopted in the present work.

Eomushkin_et_al.⁽⁸⁾

The fission cross section was measured with EhG-5 electrostatic accelerator in the energy range from 500 keV to 2.5 MeV. The measurements were made relatively to the 235 U fission cross section.

Gokhberg_et_al.¹⁹⁾

The measurement was performed in the energy range from 0.28 to 1.8 MeV with an electrostatic accelerator. To obtain the 244 Pu fission cross section, the 239 Pu fission cross section of 1.77 barns at 1.03 MeV was used.

Behrens_ct_al.²⁰⁾

The fission cross section ratio to 235 U was measured in the energy range from 0.1 to 30 MeV using 100-MeV linear accelerator at Lawrence Livermore Laboratory and ionization fission chambers.

Khan_et_al.²¹⁾

They measured the fission cross section at 14.8 MeV relatively to the 239 Pu fission cross section. Using the 239 Pu fission cross section of 2.52 barns, the fission cross section of 0.91±0.09 barn was obtained. This cross section is in good agreement with a $Z^{4/3}$ /A systematics of 14 MeV fission cross section.

Moore_ct_al.22)

The fission cross section was measured in the energy range from 1 keV to 8 MeV relative to 235 U fission cross section by using CBNM linear accelerator. The effective resolution was 0.4 ns/m. From the evaluated cross section in ENDF/B-V and the measured data, the 214 Pu fission cross section was obtained.

These data are shown in Fig. 2.2. Since Behrens et al. reported only ratio data, the fission cross section of ²³⁵U evaluated for JENDL-3.2 was used to get the ²⁴⁴Pu fission cross section. The data of Auchampaugh et al., Fomushkin et al., Gokhberg et al. and Khan et al. are smaller than those of Moore et al. and Behrens et al. Figure 2.2 shows also the values calculated with STAPRE. It is seen that STAPRE calculation is in good agreement with the

experimental data of Moore et al. and Behrens et al. in the energy region from 2 to 20 MeV. Below 1 MeV, the calculation might be too small. The STAPRE calculation around 1 MeV was not made, since energies specified by input data are shifted by STAPRE, and it was difficult to get cross sections around 1 MeV.

In the present work, the results of the STAPRE calculation was adopted above 8 MeV. Below 8 MeV, a smooth curve was determined by eye-guilding of the experimental data of Moore et al. and Auchampaugh et al. In the energy region above 300 keV, the data of Moore et al. were adopted, because they were the most recent experimental data. Below 300 keV, the data of Auchampaugh et al. were used. Below 10 keV, the data were smoothed out with an energy resolution of $0.3 \times E$ where E is a neutron energy and a factor of 0.3 was determined to get an adequate structure of smoothed cross section. The fission cross section in this energy range was determined from thus obtained smooth curve. Figure 2.3 is a comparison of the present evaluation with the experimental data.

6) Capture Cross Section

This cross section was calculated with CASTILY. The average capture width of 20 meV⁷ and the average level spacing of 17 eV^{7} were assumed. In the MeV region, direct capture cross section was assumed to be about a few mb (3.0 mb at 4 MeV and 4.0 mb at 20 MeV) and added to the CASTHY calculation.

2.3 Angular Distributions of Secondary Neutrons

The angular distributions of elastically scattered neutrons were calculated with ECIS. Those of inelastically scattered neutrons were obtained by the CASTHY calculation for the compound process and by the ECIS calculation for the direct process. Both were summed up to the final results. For the levels above 957 keV, only the compound process was considered.

The angular distributions of neutrons from the fission, (n,2n) and (n,3n) reactions were assumed to be isotropic in the laboratory system.

2.4 Energy Distributions of Secondary Neutrons

For the (n,2n), (n.3n) and continuum inelastic scattering, the energy distributions of secondary neutrons were obtained by STAPRE. The fission spectrum was assumed to be the evaporation spectrum with the nuclear temperature of 1.347 MeV obtained from systematics

given by Smith et al.²³⁾

2.5 Neutrons per Fission

The number of delayed neutrons per fission (v_d) was estimated with a systematics of Manero and Konshin.²⁴⁾ The number of delayed neutrons is 0.03 in the thermal energy region and 0.019 in the MeV region. The energy range from 4 to 7 MeV was assumed to be a transient region of the two values. The six group decay constants were assumed to be the same as those of ²⁴²Pu evaluated by Brady and England.²⁵⁾

The prompt neutrons (v_p) was determined on the basis of experimental data for ²⁴⁰Pu and ²⁴²Pu:

 $v_p \approx 2.79 + 0.163 \times E(McV).$

This is close to $v_p = 2.688 + 0.184 \times E(MeV)$ obtained from Howerton's systematics.²⁶⁾

2.6 Discussion on 244Pa Data

The cross sections obtained in the present evaluation are compared with those in ENDF/B-VI in Figs. 2.4 to 2.9. The cross sections in the resolved resonance region in these figures are averaged in quarter lethargy intervals. ENDF/B-VI gives hypothetical resolved resonances below 249 eV and unresolved resonance parameters at energies between 249 eV and 10 keV. Large discrepancies are found in the resonance region except the thermal energy region. The fission cross section in ENDF/B-VI is zero at low energies, while the present evaluation gives small values on the basis of the experimental data. Above 100 keV, the both evaluations are atmost the same. ENDF/B-VI adopted the data of Behrens et al. which are slightly smaller than the data of Moore et al. There are also rather large discrepancies in the capture, inelastic scattering, (n,2n) and (n,3n) reaction cross sections, because of no available experimental data.

The angular distributions of elastically scattered neutrons are shown in Fig. 2.10. The present results are almost the same as ENDF/B-VI. Figures from 2.11 to 2.19 are the angular distributions of inelastic scattering neutrons at 2 and 10 MeV. On the figure of 2 MeV data, contributions from the direct process calculated with ECIS are shown together with the present result which is a sum of direct and compound processes.

Figure 2.20 displays the energy distributions of (n,2n) reaction neutrons at the incident energy of 10 MeV. ENDF/B-VI adopted the evaporation spectra, and the present evaluation the STAPRE calculation. The same tendency as the (n,2n) reaction is found in the energy distributions of continuum inelastic scattering neutrons shown in Fig. 2.21. The fission neutron spectra in Fig. 2.22 are almost the same each other.

3. Evaluation of ²³⁷Pu Data

3.1 Cross sections in the thermal region

Available experimental data is 6 billy the fission cross section measured by Gindler et al.³¹) They used the thermal column of the Argönine heterogeneous heavy=water reactor, CP= 5, and obtained the cross section of 2500 ± 500 b. CINDA³²) stores an index line of experiment made by Hulet et al.³³ with the cross section of 2200 b. However, this is not in published reports. Mughabghab⁷) recommended the thermal cross section of 2455 ± 295 b. We adopted this value as the cross section at 0.0253 eV. The ratio of fission cross section to capture cross section was assumed to be the same as that in the keV region. The ratio in the keV region is about 1/5 as is described in the next section. Therefore, the capture cross sections were assumed to have a form of 1/v, and smoothly connected the cross sections at 1 eV. The adopted elastic scattering cross section is a constant of 11.5 b which was calculated at low energies with CASTHY as described in the next section. The total cross section was calculated as a sum of these cross sections.

No resonance parameters were given, because no experimental data were available for the resonance parameters and the level spacing estimated from level density parameters was so small that Doppler effects might not be important.

3.2 Cross sections above 1 eV

3.2.1 Theoretical calculation

In this energy range, no experimental data are available. Theoretical calculations of cross sections were made with ECIS, STAPRE and CASTILY.

ECIS Calculation

The total and shape elastic scattering cross sections, angular distributions of elastically and inelastically scattered neutrons and neutron transmission coefficients were calculated with ECIS in the energy range above 400 keV. An even-Z and odd-N nucleus ²³⁷Pu is difficult to analyze in terms of the coupled channel method, as it has a high spin of the ground state (7/2) and, besides, the K=7/2 and K=1/2 bands become mixed already at low energy (0.15 MeV) and the band mixing increases with the energy of the excited states. This is the evidence of nonaxial symmetric deformation and it seems questionable to assume a symmetric rotational model for the analysis of ²³⁷Pu. However this model has the advantage of making the entire analysis of the neutron scattering on ²³⁷Pu easier.

The code ECIS was used in the energy range from 0.4 to 20 MeV (the symmetric rotational model for the low lying band K=7/2). Five levels of this band were considered coupled. In the ECIS code, it was not possible to take into account the second rotational band K=1/2 mixed with K=7/2. Coupled channel calculations for ²⁰⁷Pu were made using the following optical model parameters:

$V_{R} = 46.2 -$	0.3E,	$0 \le E \le 20$ MeV
$W_D^{surf} =$	3.05 + 0.4E,	$0 \le E \le 10 \text{ MeV}$
	7.05 - 0.082(E-10),	$10 \le E \le 20 \text{ MeV}$
$W_V^{vol} = 8.0x$	{1+cxp[-(E-50)/10]} ⁻¹ ,	$0 \le E \le 20 \text{ MeV}$
$V_{SO} = 6.2$		
$r_{\rm R} = 1.26$,	a _k = 0.63	
r _D = 1.26,	$a_0 = 0.52$	
$r_{SO} = 1.12,$	$a_{\rm SO} = 0.47$	
$\beta_2 = 0.220,$	$\beta_4 \equiv 0.07$	

These parameters were determined by Konshin considering Refs. 12 and 13.

STAPRE Calculation

The code STAPRE was used for calculations of the fission cross section, (n,2n) and (n,3n) reaction cross sections and the inelastic scattering cross section. Neutron transmission coefficients for these calculations were provided by the ECIS code. The fission barrier parameters E_r^A and E_r^B used were the following:

nuclide	E _f ^(MeV)	E ^B (McV)
²³⁸ Pu	5.60	5.10
²³⁷ Pu	6.00	*5,80
²³⁶ Pu	5.3()	4,70
235Pu	5.60	5.10

These parameters were determined so as to reproduce the experimental data of fission cross sections for neighboring nuclides and by considering their systematic trend.

CASTHY_Calculation

CASTHY was used in order to calculate the inelastic scattering cross sections due to

the compound process and the capture cross section. The optical potential parameters used are listed in Chapter 2 with the following modification:

$$V_{\rm H} = 44.7 = 0.3 \ {\rm E} \ {\rm (McV)}.$$

This modification was made by assuming the total cross section in the keV region to have the same tendency of ²³⁹Pu total cross section, and so as to reproduce such tendency.

The level density parameters for Gilbert-Cameron's formula were determined with the same way as ²⁴⁴Pu evaluation. Obtained parameters are given in Table 2.3. Level scheme of ²³⁷Pu listed in Table 3.1 that was adopted from ENSDF.

3.2.2 Compilation of cross section data

1) Total Cross Section

The adopted total cross section was the theoretical calculation with CASTHY in the energy range from 1 eV to 400 keV, and with ECIS above 400 keV.

2) Elastic Scattering Cross Section

Above 1 keV, this cross section was obtained by subtracting the sum of partial cross sections from the total cross section. Above 3 MeV, the results are essentially the same as ECIS calculation. Below 1 keV, it was assumed to be a constant value of 11.5 b which was obtained by the subtraction at 1 keV.

3) Inelastic Scattering Cross Sections

The direct inelastic process was calculated with ECIS to the 1st, 2nd, 5th and 8th levels. The direct inelastic scattering cross sections were added to the compound inelastic scattering cross sections calculated with CASTHY. Levels above 655 keV were assumed to be overlapping. The continuum inelastic cross section was calculated by means of CASTHY below 2 MeV, and by subtracting a sum of the elastic scattering cross section calculated with ECIS and the fission, (n,2n), (n,3n) and capture cross sections from the total cross section calculated with ECIS above 3 MeV. Thus determined cross sections were simply connected between 2 and 3 MeV.

4) (n,2n) and (n,3n) Reaction Cross Sections They were calculated with STAPRE.

5) Fission Cross Section

Above 1 MeV, the results calculated by STAPRE were adopted. The shape of the cross section in the 100 keV region was assumed to be the same as that of ²³⁹Pu, and it was normalized to the fission cross section at 1 MeV. Below about 100 keV, since the resonance structure of ²³⁹Pu could not be adopted, the cross section was assumed to be $\sigma_{fis} = \sigma_{K} \times 0.85$ where σ_{R} is the total reaction cross section calculated with CASTHY and the factor of 0.85 was estimated at 100 keV.

6) Capture Cross Section

The capture cross section was calculated with CASTHY. The average capture width of 47 meV and the average level spacing of 0.233 eV were assumed. The average capture width was estimated from the systematics by Malecki et al.³⁴⁾, by Bondarenko and Urin³⁵⁾ and by Gardner³⁶⁾. However, results of the CASTHY calculation that took into account of competing cross sections had unexpected shape around 1 MeV because the shape of the fission cross section based on the reaction cross section calculated with ECIS was inconsistent with the reaction cross section calculated with CASTHY. Therefore, the capture cross section adopted was calculated by CASTHY without competing process and normalized to the calculation with competing process at 10 keV. In the MeV region, the same amount of direct capture cross section as ²⁴⁴Pu was added to the CASTHY calculation.

3.3 Angular and Energy Distributions of Secondary Neutrons

The angular distributions of elastically scattered neutrons were calculated with ECIS above 400 keV, and with CASTHY below 400 keV. Those of inelastically scattered neutrons were obtained by the CASTHY for the compound precess and by ECIS for the direct process. The angular distributions of neutrons emitted from the fission, (n,2n) and (n,3n) reactions were assumed to be isotropic in the laboratory system.

The energy distributions of neutrons from the (n,2n), (n,3n) and continuum inelastic scattering were obtained by STAPRE. The fission neutron spectrum was assumed to be the evaporation spectrum with the temperature of 1.387 MeV that was obtained from the systematics given by Smith et al.²³⁾

3.4 Neutrons per Fission

The number of delayed neutrons per fission (v_d) was estimated with a systematics of

Manero and Konshin.²⁴⁾ Estimated delayed neutron yield v_d in the low energy region is 0.002 and that in the high energy region is 0.0014. The energy range from 4 to 7 MeV was assumed to be a transient area of these two values. The six group decay constants were assumed to be the same as those of ²³⁹Pu evaluated by Brady and England²⁵⁾.

The number of prompt neutrons (v_p) was determined on the basis of experimental data for ²³⁹Pu:

 $v_{\rm p} = 2.863 + 0.123 \times E({\rm MeV}).$

This is close to $v_p = 2.9203 + 0.1420 \times E(MeV)$ obtained from Howerton's systematics.²⁶⁾

3.5 Discussion on ²³⁷Pu Data

The present evaluation is compared with evaluated data⁵⁾ in ENDF/B-VI. Table 3.2 is a list of thermal cross sections and resonance integral. Both evaluations give almost the same values.

The cross sections are shown in Figs. 3.1 to 3.7. The total and elastic scattering cross sections of the both evaluations are almost the same as shown in Figs. 3.1 and 3.2. Figures 3.3 and 3.4 are comparison of fission cross sections. Tendency of the cross section is the same in the both evaluations. However, ENDF/B-V1 is larger than the present evaluation above 1 eV. As a result of these discrepancies, the resonance integral of ENDF/B-V1 is about 30 % larger than the present evaluation. The capture cross sections in Fig. 3.5 are discrepant from each other around 1 eV and above 10 keV. The cross sections of inelastic scattering, and (n,2n) and (n,3n) reactions have remarkable discrepancies as shown in Figs. 3.6 and 3.7.

The graphs of the angular distributions of elastically and inelastically scattered neutrons and the energy distributions of neutrons emitted from (n,2n), continuum inelastic scattering and fission are shown in Figs. 3.8 to 3.15. Large discrepancies among the present results and ENDF/B-VI evaluations are found in the energy distributions of neutrons the (n,2n) reaction and continuum inelastic scattering. These discrepancies come from the discrepancies of their cross sections.

4. Conclusion

The nuclear data evaluation of ²⁴⁴Pu and ²³⁷Pu was made in the incident neutron energy range from 10⁻⁵ eV to 20 MeV. The available experimental data are quite limited, so the theoretical calculations were widely used. The parameters needed to the calculation was determined by systematic investigation for several nuclides around ²⁴⁴Pu and ²³⁷Pu. Especially the fission cross section calculated with the STAPRE code is reliable because the results of STAPRE are in good agreement with experimental data for several Pu isotopes. The present results will be stored in JENDL Actinoid File.

In order to improve the nuclear data of minor actinides, experimental data are quite important in particular for the fission, capture, (n,2n) cross sections and resolved resonance parameters in the low energy region. However, only the fission cross section of ²⁴⁴Pu in wide energy range and that of ²³⁷Pu at the thermal energy are available in the present work. Therefore, the uncertainties of the present results might be rather large except for the ²⁴⁴Pu fission cross section. New experimental data are deeply required to improve the present status of these nuclides.

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Resonance	Neutron	Fission
cnergy (eV)	width (mcV)	width (meV)
-6.0	1.558	0.02
4.0	0.026	0.02
30.7	2.2	0.022
40.3	1.03	0.022
53.5	0.80	0.025
64.3	15.5	0.021
87.6	3.2	0.013
102.0	43.0	0.020
128.0	3.0	0.020
161.0	2.10	0.012
185.0	31.0	0.018
191.0	3.20	0.023
227.0	300.0	0.020
233.0	4.1	0.020
285.0	61.0	0.020

Table 2.1	Resolved	resonance	parameters	of ²⁴⁴ Pu
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 $\Gamma_{\gamma} = 20 \text{ meV}$ for all resonances.

R' = 9.33 fm.

All levels are s-wave resonances .

Table 2.2 Thermal cross sections and resonance integrals of²⁴⁴Pu

(in barns)

 quantity	present	ENDF/B-VI	others	Rcf. of others
 (J _{tot}	12.036	11.465		
(7 _{cla}	10.354	9.635		
U _{fis}	0.0017	0.0		
σ _{cap}	1.680	1.830	1.7±0.1	Mughabghab ⁷⁾
			2.1±0.3	Butler et al. ²⁷⁾
			1.5±0.3	Fields et al. ²⁶⁾
			1.6±0.3	Schuman ²⁹⁾
RI _{fis}	5.07	4.73		
RI _{cap}	5 0.0	106.	40.6±2.9	Mughabghab ⁷⁾
			35±7	Schuman ²⁹⁾
 			40±3	Druzhinin et al. ³⁰⁾

Nuclide	a(MeV ⁻¹)	T(MeV)	δ(MeV)	E _z (MeV)	u	$D_{obs}^{cal}(cV)$	Dobs ^{exp} (eV)
²³⁷ Pu	30.94	0,389	0.779	4.2131	31.10	4.60	-
²³⁸ Pu	31.68	0.394	1.556	5.1959	31.56	0.233	-
²³⁹ Pu	30.35	0.394	0.776	4.2035	30.98	9.01	9.0±0.7
²⁴² Pu	32.60	0.380	1.543	5.0169	32.37	0.90	().9±().1
²⁴³ Pu	32.66	0.355	0.7698	3.7248	32.49	15.5	15.5±1.7
²⁴⁴ Pu	31.0	0.380	1.536	4.7720	31.74	2.34	-
²⁴⁵ Pu	34.87	0.315	0.7667	3.1895	33.76	17.0	17±3

Table 2.3 Level density parameters of Pu isotopes used in CASTILY calculation

a: level density parameter

T: nuclear temperature

8: pairing energy

Ex: connection energy of constant temperature model and Fermi gas model

a: spin-cutoff parameter

Dobe: s-wave average level spacing at neutron binding energy

Table 2.4 Level scheme of ²⁴⁴Pu

Energy (keV)	spin	parity	
0.0	0	+	
48.0	2	+	
153.0	4	+	
315.4	6	+	
531.8	8	+	
708.0	2	+	
798.3	10	+	
957.0	3	-	
1015.0	2	+	

The levels above 1.068 MeV were assumed to be overlapping.

Table	3.1	Level	scheme	of	237 Pu
Taolo	J. 1	Devel	scheme	OF.	1 4

Encrgy (kcV)	spin	parity
00	712	_
47.71	9/2	-
106.0	11/2	-
145.54	1/2	÷
155.45	3/2	+
175.0	13/2	-
201.18	5/2	+
224.25	7/2	4
257.0	15/2	-
280.22	5/2	+
304.0	9/ 2	+
320.97	7/2	+
370.4	3/2	+
371.0	9/2	+
404.19	5/2	+
407.83	5/2	+
438.41	7/2	+
453.2	7/2	+
473.5	7/2	+
486.0	9/2	+
513.0	9/2	+
545.0	1/2	-
582.0	5/2	-
591.0	3/2	-

The levels above 655 keV were assumed to be overlapping.

 quantutÿ	present	ENDF/B-VI	others	Ref. of others
(J ₁₆₁	2966.5	2651.7		
(J _{els}	11.50	11.73		
θ _{fb}	2455.0	2100.0	2455±295 2500±500 2200	Mughabghab ⁷⁾ Gindler et al. ³¹⁾ Hulet et al. ³³⁾
(T _{cap}	500.0	540.0		
R1 _{fis}	816	1085		
RI _{cap}	142	190		

Table 3.2 Thermal cross sections and resonance integrals

(in barns)



Fig.2.1 Fission cross section in the resolved resonance region. The experimental data were measured by Auchampaugh et al.". Solid curve shows the cross section calculated from the resonance parameters taking account of Doppler effect at 300 K. Peaks not followed by the solid curve are due to impurities in the sample.



Fig.2.2 Fission cross sections in the energy range from 10 keV to 20 MeV. Squares are results of STAPRE calculation, and they are simply connected with a solid line.



Fig.2.3(a) Comparison of evaluated fission cross section with the experimental data".



Fig.2.3(b) Comparison of evaluated fission cross section with the experimental data.







Fig.2.5 ²¹¹Pu elastic scattering cross section



Fig.2.7 ²¹¹Pu capture cross section



Fig.2.8 244Pu total inelastic scattering cross section



Fig.2.9 241Pu(n,2n) and (n,3n) reaction cross sections



Fig.2.10(a) Angular distributions of elastically scattered neutrons from ²⁴⁴Pu



Fig.2.10(b) Angular distributions of elastically scattered neutrons from ²⁴¹Pu



Fig.2.11 Angular distributions of inelastically scattered neutrons from ²⁴⁴Pu 48-keV level. The solid line shows the present result, and the dashed one the result of ECIS calculation. At 10 MeV, the both are the same.



Fig.2.12 Angular distributions of inelastically scattered neutrons from ²⁴¹Pu 153-keV level (See Fig.2.11)



Fig.2.13 Angular distributions of inelastically scattered neutrons from ²⁴⁴Pu 315-keV lovel (Sco Fig.2.11)



Fig.2.14 Angular distributions of inelastically scattered neutrons from ²⁴⁴Pu 532-keV level (See Fig.2.11)



Fig.2.15 Angular distributions of inelastically scattered neutrons from ²⁴⁴Pu 708-keV level (See Fig.2.11)



Fig.2.16 Angular distributions of inelastically scattered neutrons from ²⁴⁴Pu 798-keV level (See Fig.2.11)



Fig.2.17 Angular distributions of inelastically scattered neutrons from ²⁴⁴Pu 957-keV level



Fig.2.18 Angular distributions of inelastically scattered neutrons from ²⁴⁴Pu 1015-keV level



Fig.2.19 Angular distributions of inelastically scattered neutrons from ²⁴¹Pu continuum level



Fig.2.20 Energy distributions of neutrons emitted from ²⁴⁴Pu (n,2n) reaction at 10 MeV



Fig.2.21 Energy distributions of neutrons emitted from $^{244}{\rm Pu}$ continuum inelastic scattering at 5 MeV



Fig.2.22 Energy distributions of ²⁴⁴Pu fission neutrons (E.=500 keV)











Fig.3.3 ²³⁷Pu fission cross section



Fig.3.4 ²³⁷Pu Fisson cross section (Above 100 keV)







Fig.3.6 ²³⁷Pu total inelastic scattering cross section



Fig.3.7 237Pu (n,2n) and (n,3n) reaction cross sections



Fig.3.8(a) Angular distributions of elastically scattered neutrons from ²³⁷Pu



Fig.3.8(b) Angular distributions of elastically scattered neutrons from ²⁹⁷Pu



Fig.3.9 Angular distributions of inelastically scattered neutrons from ²³⁷Pu 48-keV level



Fig.3.10 Angular distributions of inelastically scattered neutrons from ²³⁷ Pu 105-keV level



Fig.3.11 Angular distributions of inelastically scattered neutrons from ²³⁷Pu 175-keV lovel



Fig.3.12 Angular distributions of inelastically scattered neutrons from ²⁹⁷Pu 257-keV level



Fig.3.13 Energy distributions of neutrons emitted from 237 Pu(n,2n) reaction at 10 MeV



Fig.3.14 Energy distributions of neutrons emitted from ²³⁷Pu continuum inelastic scattering at 5 MeV



Fig.3.15 Energy distributions of 237Pu fission neutrons (E.= 500 keV)

国際単位系 (SI) と換算表

表1 BI基本単位わよび補助単位。

	t	名称	記り
K	ð	A - + N	115
ព	5A 111	キログラム	kg
83) 381	(ii) 24	19	H A
熱力的	ni. Alite	サルビン	ĸ
177 1	竹柏	10 IV	mot
_ <u>K</u>		カンチウ	cd
4 1	前角	ラジアン	rad
· 北 杉	F 明	スチウジアン	ыP

表1 固有の名称をもつ 81 相立単位

N	名称	記号	他の出理侍 による表現
M N K	~ ~ "	Hz.	
h	- a - + 4	N	m·kg/s²
甩力,吃力	KX H IV	Pa	N/m'
コネルドッ仕事 熱陸	2 11	J	N-m
上半,放射束	リット	W	J/m
电気量, 电荷	リーロン	C	A+#
油鱼。油用,起油力	16 JE F	V	W/A
静讯学科队	ソ・クド	۲	C/V
准负抵抗	1 4	11	V/A
コンダクタンス	40 142	ន	A/V
做一些	1 1 - 14	Wb	V-s
磁水常度	7 2 7	r	Wb/m/
インタクタンス	マンリー	H	Wb/A
セルシウス晶度	セルシウス度	Ĵ,	l
光电	10-17	lm	cd-at
<u>照</u>	ルクス	lx –	lm/m*
秋 引 能	~ 7 ~ ~	Bq	8 ⁻¹
败 化 線 陆	グレイ	Gy	J/kg
网络当场	シーベルト	Sv	J/kg

表 2	81	Ł	俳	川	ð	ł	12	伸	1
-----	----	---	---	---	---	---	----	---	---

26 Hr	3년 15
- 分, 時, 目 度, 分, 長 リットル ト シ	min, h, d T, 7, T h, h
相子ポルト 現子質量単位	eV 11

1 eV=1.60218×10^{-1*}J 1 u=1.66054×10⁻¹⁹ kg

表4	81と共に物定的に
	推持される単位

	名梢		11 11
12	グストロ	1.	Å
14		2	h
16		16	bar
11		n	Gal
4	.a. 1)	-	Cì
してい	レトク	r 7	ĸ
ゥ		- K [rad
~		1.	rem

1 Å = 0.1 nm = 10⁻¹⁴ m 1 b = 100 fm³ = 10⁻¹⁴ m³ 1 bar = 0.1 MPa = 10⁻²⁴ m³ 1 Gal = 1 cm/s³ = 10⁻² m/s³ 1 Ci = 3.7 × 10¹⁴ Bq 1 R = 2.58 × 10⁻³ C/kg 1 rad = 1 cGy = 10⁻³ Gy 3 rem = 1 cSy = 10⁻⁴ Sy

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表6 出技项语

价数	i te ya Mili	起号
10 "	エクサ	K
1011	4 9	P
1011	チョ	Т
101	4 <i>1</i>	G
10*	1 11	М
101	4 U	k
101	ヘット	h
101	デーカ	da
10.1	チジ	d
10 1	センチ	C
10-1	()	m
10.4	41911	μ
10-1	+ 1	n
10°11	ะ ม	p
10*11	7:41	1
10-14	7 F	n

(it)

- 九1…5は「国際単位希上第5場。国際 改統術局 1985年利村による。ただし、1 eV および1 aの値は CODATA の 1986年推奨 値によった。
- 友々には前型。ノット。アール。ペクタ ールも含まれているが目常の単位なのでこ こでは省略した。
- bar(t, JISでは歳体の圧力を表わす場 合に関け表えのカナゴリーに分類されている。
- 4. EC期位理事会指令では bar, barn およ び手面圧の単位上 mm相関を表2のカテゴリ 一に入れている。

ŋ	N(~10'dyn)	kgf	167
	1	0.101972	0.224809
	9,80665	1	2.20462
	4.41822	0.453592	1

|拈_|皮_|1 Pa+s(N+s/m¹)=10 P(ボアズ)(g/(cm+s)) |動粘度_|1 m¹/s=10¹St(ストークス)(cm¹/s)

Ц.	MPa(=10 bar)	kgf/cm*	atm	mmlig(Torr)	lbf/in*(pai)
	1	10,1972	9.86923	7.50062 × 101	145.038
h	0.00940665	1	0.967841	735.559	14 2233
	0.101325	1.03323	1	760	14.6959
	1.33322 × 10**	1.35951 ± 10°?	1.31579 + 10 +	1	1.93368 × 10° *
	689476 # 1017	7.03070 = 10 /	6 80460 = 10 +	51.7149	1

T	J(=10' erg)	kgfem	k₩+h	ent(1444).)	Btu	ft + lbf	rV	1 cal # 4.18605 J (41 Mil.)
1	1	0.101972	2.77778 × 10-7	0.230989	9 47813 × 10 *	0.737562	6 24150 × 1014	
	940065	1	2.72107 + 10 *	2 3 1270	9.29497 + 10 *	7,23301	6.12082 × 101*	⊕ 4.1855 JL (15 °C)
	3.6 × 10*	3 67098 + 10 1	1	8.5(FFP) = 10 ⁺	3112.13	2.65522 × 10*	224594 = 1015	» 4, 1868 J (国際加加人)
	4 18605	0.426858	1.16279 * 10 *	1	3 96759 * 10-1	3.08747	261272 + 10"*	1144 APS (1297)
	1055.66	107.586	2,93072 + 10 *	252 012	1	778,172	6.58515 × 10+1	∞ 75 kgf+m/s
	135582	0,139255	376616 + 10 7	0.323890	1 28506 × 1011	1	8.46233 = 101*	+ 735 479 W
	1.60218 × 10 .04	1 63377 × 10 ⁻⁷⁸	445050 × 10-4	382743 + 10 *	1.51857 + 10 14	1.18171 × 1011	1	

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Ŋ

44	154	Ci	2	Gy	rad	F.L	C/kg	R	12	Sv.	setti
41	ł	2.70279 + 10 **	12	1	100	12	I	3476		1	100
HC.	3.7 × 10 ¹⁰	t		0.01	1	ų,	2.58 • 10**	1	μī	0.01	1

(86年12月26日現在)

EVALUATION OF NUCLEAR DATA OF 24Pu AND 237Pu