

Electrical Testing of the Full-Scale Model of the NSTX HHFW Antenna Array*

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Abstract. The 30 MHz high harmonic fast wave (HHFW) antenna array for NSTX consists of 12 current straps, evenly spaced in the toroidal direction. Each pair of straps is connected as a half-wave resonant loop and will be driven by one transmitter, allowing rapid phase shift between transmitters. A decoupling network using shunt stub tuners has been designed to compensate for the mutual inductive coupling between adjacent current straps, effectively isolating the six transmitters from one another. One half of the array, consisting of six full-scale current strap modules, three shunt stub decouplers, and powered by three phase-adjustable rf amplifiers had been built for electrical testing at ORNL. Low power testing includes electrical characterization of the straps, operation and performance of the decoupler system, and mapping of the rf fields in three dimensions.

SIX-ELEMENT, FULL-SCALE MOCKUP ARRAY

The power distribution/phase control system for the NSTX HHFW 12-element antenna array was designed using the FDAC coupled transmission line code [1-3]. Antenna parameters for the transmission line model were calculated from 2D magnetostatic codes; each antenna strap was divided into four sections: two ends, a center,

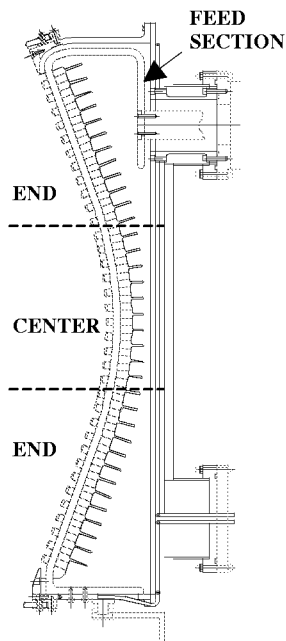


FIGURE 1. NSTX Current Strap



FIGURE 2. Six-element, full scale mockup of the NSTX HHFW array.

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and a radial feed (Fig. 1). The analysis predicts that six transmitters should deliver 6 MW total power to the plasma at 30 MHz with the peak antenna voltages remaining below 25 kV and peak system voltages below 35 kV, providing the expected plasma loading is at least 4 Ω/m . Stub decouplers between resonant loops are expected to keep the magnitude of the strap currents within a few percent and their phase within a few degrees of optimum when the phase of the transmitters is varied, if the plasma loading can be held relatively constant through plasma position control (~ 2.5 cm shift in plasma edge can compensate for a factor of two change in loading.)

Six full-scale mockups of the NSTX antenna modules were fabricated and assembled to form a 6-element array (Fig. 2). The purpose was to check the electrical characteristics of the straps against the values used in the design of the power distribution system, test the performance of the phase control system, develop procedures for tuning the resonant loops, decouplers, and matching network, and make measurements of the field patterns of the array.

COMPARISON OF MOCKUP MEASUREMENTS TO SYSTEM DESIGN

Frequency sweeps of reflection coefficients and time domain reflectometry measurements were made with an HP 8753D network analyzer on a single strap to determine some electrical characteristics of the antenna. However, the full 6x6 scattering parameter matrix, measured at the antenna inputs (Fig. 3), proved to be the more accurate method of determining these parameters. Table 1 shows the calculated values used in the original design study compared with the values needed to match the array measurements. Figure 4 compares the calculated and measured principle transmission coefficients (S_{12} , S_{13} , and S_{14}). The characteristic impedance of the straps turned out to be slightly higher than originally calculated and the inductive coupling between straps was slightly lower (magnetic shielding due to the Faraday shield was ignored in the design study). The biggest difference was in the electrical length of the radial feed section that connects to the strap. This needed to be increased about 40% over the approximate physical length to match the high frequency response of the measured S-parameters.

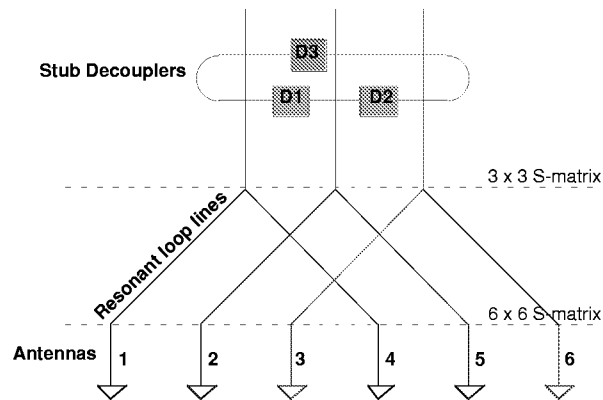


FIGURE 3. The six straps are connected to form three resonant loops; each loop is decoupled from the others by a shunt stub tuner.

TABLE 1 Comparison of original calculated values to measurements

		Calculated Design Values	Values To Match Mockup Measurements
Strap Inductance	Center	2.81e-7 H/m	2.94e-7 H/m
	Ends	3.39e-7 H/m	3.57e-7 H/m
Strap Capacitance	Center	1.21e-10 H/m	1.12e-10 F/m
	Ends	1.21e-10 H/m	1.08e-10 F/m
Strap Z_0	Center	48 Ω	52 Ω
	Ends	53 Ω	58 Ω
Phase Velocity	Center	0.57 c	0.58 c
	Ends	0.52 c	0.54 c
Inductive Coupling, k_{12}	Center	0.09	0.08
	Ends	0.14	0.10
Inductive Coupling, k_{13}	Center	*	0.02
	Ends	*	0.02
Strap Length	Center	0.30 m	0.285 m
	Ends	0.30 m	0.285 m
Feed Length		0.20 m	0.35 m
Feed Z_0		27.5 Ω	26 Ω

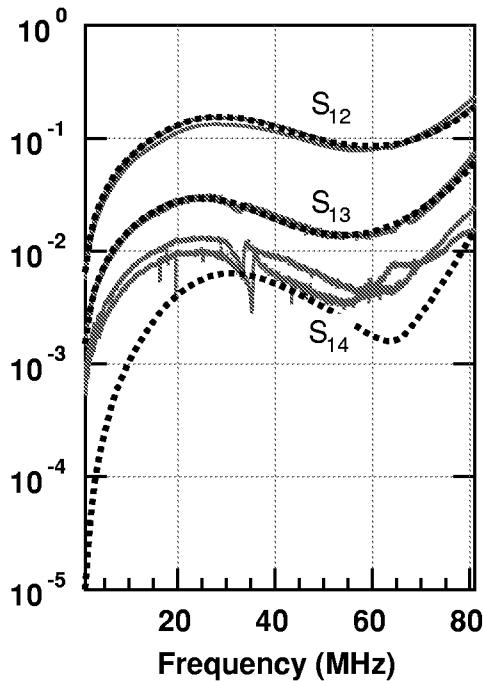


FIGURE 4. S_{11} , S_{12} , and S_{13} as a function of frequency. Solid lines are measurements, dotted lines are calculations.

Strap pairs 1-4, 2-5, and 3-6 were connected together with RG-58 cables of lengths 5.33 and 10.24 m to form three loops, each resonant at approximately 30 MHz (29.95 MHz). The resonant lengths of each loop were set by shorting the other two loops at their T-feed point, which is normally a high impedance point. This detunes them sufficiently at 30 MHz so they are decoupled from the test loop and do not respond to its excitation.

Figures 5a-c show the reflection and transmission coefficients of the 3x3 S-matrix measured at the inputs of the resonant loops (dotted lines are calculated from the model). Agreement between measurement and model could not be maintained over a large frequency range due to the dispersive nature of the RG-58

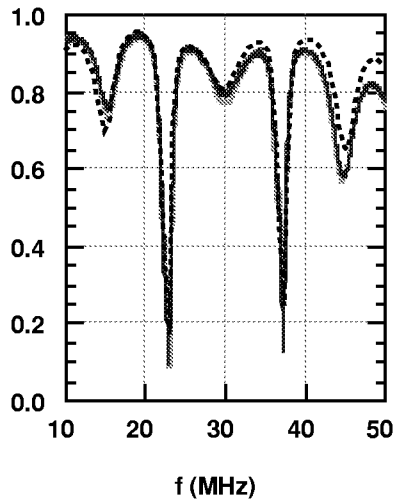


FIGURE 5a. S_{11} , S_{22} , S_{33} at loop input

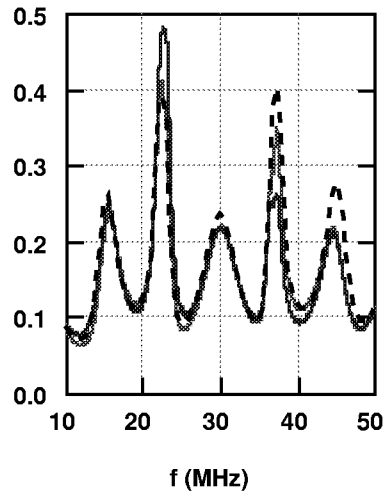


FIGURE 5b. S_{12} , S_{23} at loop input

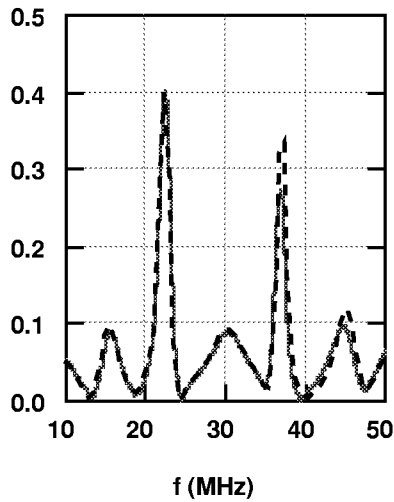


FIGURE 5c. S_{13} at loop input

cable and BNC connections; the measured electrical length of the cables changed from 15.73 to 15.67 m as the frequency was increased from 28.6 to 52.6 MHz. These cables were chosen for reasons of availability and economy; the remainder of the power distribution system, including the decouplers, used RG-8 cable with Type N connectors.

FOLLOW ON TESTING

Decoupler D1 was adjusted to minimize S_{12} with D2 and D3 disconnected and loop 3 shorted at the T. Then D2 was connected and adjusted to minimize S_{23} with D3 disconnected. Finally, D3 was

connected and adjusted; the S_{12} , S_{23} , and S_{31} were between -30 and -35 dB with the decouplers in place. The shunt lengths (3.0 and 2.5 m) connecting the stub tuners have not yet been adjusted to their optimum lengths (2.67 and 2.36 m respectively) needed to minimize system voltages for a given power.

REFERENCES

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