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Evolution of Fuel Cycles for NPP with VVER-440. Status and Prospects

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Main ways of improving VVER-440 fuel assemblies (FAs)

Extended list of manufactured operational FA types Expansion the nomenclature of different types FAs
Improved FA construction
Increased fuel column height in assemblies
Increased fuel rod lattice pitch
Reduced neutron absorption in FA construction materials (reduced hafnium (Hf) contents)
Reduced FA shroud thickness
Improved construction of the control rod assembly's coupler part



Basic parameters of VVER-440 FA designs

| Parameter | Initial fuel cycle | Current fuel cycle | Projection 2010 г |
|---|-----------------------|-----------------------|-----------------------------|
| Construction materials | Zr(Hf≤0.05%) | Zr(Hf≤0.05%) | Zr (Hf≤0.01%) |
| Cover FA | Zr(Hf≤0.05%) | Zr (Hf=0.01%) | NO |
| Burnable absorber | | UO_2 - Gd_2O_3 | UO_2 - Gd_2O_3 |
| Profiled FA average enrichment | 1.100元子3 | | |
| in horizontal section | YES | YES | YES |
| in axial section | NO | NO | YES |
| Weight of uranium in FA (rel.) | 1.00 | 1.05 | 1.15 |
| Axial hole Diameter, rel. /Height | 1.00/1.00 | 0.86/1.02 | 0.0/1.02 |
| Fuel rod lattice pitch, rel./ Fuel rod diameter, rel. | 1.00/1.00 | 1.01/0.99 | 1.03/0.97 |
| The maximal enrichment of fuel (%) | 4.40 | 4.25 | 4.65 |
| The maximum admissible FA burn-up (MWd/kg HM) | 53.9 | 57.5 | 62.0 |
| The maximum admissible FA energy production (rel.) | 1.00 | 1.12 | 1.32 |



Typical FA pattern of the for VVER-440



Standard FA fuel enrichment 1.6%, 2.4%, 3.6%, 4.4%





Present-day FA pattern of the for VVER-440





Advanced FA pattern of the for VVER-440 (second generation)



CT IN TVEL 4.4% 2 GENERATION
 TVEL 4.4% 2 GENERATION(78mwtday/kg)
 TVEL 4.0% 2 GENERATION(78mwtday/kg)
 TVEL 3.6% 2 GENERATION(78mwtday/kg)
 6 tweg GD335X40 IN in assembly 4.25% 2 GEN
 fuel enrichment 4.25%
 with (Gd₂O₃)







Control Rod Assembly (Hf shielding) coupler part Improvement design







Main ways of improving VVER-440 fuel cycle

>Increased initial fuel enrichment and reduced share of reloaded fuel >Use of fuel refueling patterns with lower neutron leakage >Increased FA operational period (from 3-4 to 5-6 years) ► Increased fuel burn-up (from 30-40 to 50-60 MW·day/kg) > Decrease in conservatism of substantiation of fuel cycle



ADVANCED FOUR-YEAR FUEL CYCLE with 3.82% FA PROFILED AVERAGE ENRICHMENT

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Number of loaded FAs, 84 pcs Cycle length, 307 FPD Period average FA operation 4.14 year Average burnup, 44.61 MWd/kg

• fuel economy

Number of loaded FAs, 78 pcs Cycle length, 286 FPD Period average FA operation 4.58 year Average burnup, 44.91 MWd/kg



Further improvement of VVER-440 fuel utilization efficiency and safety Modern 5-year fuel cycles using uranium-gadolinium fuel

√Using burnable absorbers integrated with fuel
√Ensuring fuel cycle flexibility
√No need of changing NPP fresh fuel handling instructions at the moment of second-generation assemblies' introduction
√Developing fuel cycles providing for excess power reactor operation (105-110%)
√Developing fuel cycles with account of maneuvering reactor operation modes



EQUILIBRIUM 5-YEAR FUEL CYCLE with 4.25% FA PROFILED AVERAGE ENRICHMENT with (Gd₂O₃)

EQUILIBRIUM 5-YEAR FUEL CYCLE with FA 4.4% ENRICHMENT



Number of loaded FAs, 66 pcs Refueling pattern IN-IN-IN-OUT



Number of loaded FAs, 78 pcs Refueling pattern WITH A LOW NEUTRON LEAK



Main Neutron Physics Parameters of Equilibrium Fuel Cycles

| Name of cycle | | | 4.4% |
|---|---------|------|----------|
| | | UGBA | Ref. Com |
| Amount of loaded FAs, pcs | | 66 | 78 |
| Average enrichment of fresh FAs, % | | | 4.4 |
| Burnable absorber type | | | Not used |
| Time of FA operation average lifetime, year | | 5.01 | 4.47 |
| Cycle length, EFPD | | 314 | 327 |
| Unloaded fuel Burn-up, MWd/kgU | Average | 49.9 | 47.9 |
| · 通道下部的 通道下部的 通道 | Maximum | 53.0 | 52.7 |
| Maximal relative power of fuel rods in the core | | | 1.57 |
| Critical concentration of boric acid, g/kg | | | 6.15 |
| Coefficient of reactivity on coolant temperature | | | >0 |
| (BOC, hot T _M =200 °C, zero power, all control rods out), pcm/°C | | | 2.56 |
| Repeat criticality temperature, °C (End of Cycle) | | | 141 |
| Maximal Linear Heat Rate of Fuel Rod, W/ CM | | | 253.6 |





EQUILIBRIUM 5-YEAR FUEL CYCLE with 4.25% FA PROFILED AVERAGE ENRICHMENT with (Gd₂O₃)

EQUILIBRIUM 5-YEAR FUEL CYCLE with 4.4% FA ENRICHMENT



ADVANCED EQUILIBRIUM FIVE-YEAR FUEL CYCLE with 4.25% FA PROFILED AVERAGE ENRICHMENT with (Gd₂O₃)







ADVANCED FIVE-YEAR FUEL CYCLE with 4.25% FA PROFILED AVERAGE ENRICHMENT with (Gd₂O₃) Power to increase by 5%-10% of power rating

Equilibrium Fuel Cycles

Reactor thermal power 1444 MW

Cycle length, 306 FPD

Amount of loaded FAs, 72 pcs

Max. relative power

of FA

1.36 (Kq_{max})

Max. relative power

of fuel rods

1.50 (Kr_{max})

Maximal value of

fuel rods linear heat rate, 280.0 W/cm









CONCLUSION

> Operational reliability of this new fuel has the same level, as traditional fuel.

- > Technical solutions laid in the design of second-generation fuel assemblies, were proven and confirmed by the results of trial and commercial operation.
- Development of a technical proposal on a third-generation fuel assembly is currently underway.



RRC

CONCLUSION

Profiled fuel with burnable absorber based on gadolinium makes it possible to realize full-scale 5-year fuel cycles with average fuel enrichment reduced from 4.4-4.38% to 4.25% (in second-generation assemblies).

>Present-day fuel cycles for VVER-440 developed on the base of new FA constructions (second-generation fuel) ensure considerable increase of nuclear fuel utilization efficiency.

>Present-day fuel cycles for VVER-440 make it possible to realize various operational fuel load lifetimes. This allows optimal adapting of the unit's electricity production to the specific energy system requirements.

>Fuel cycles for VVER-440 using modernized construction of fuel were developed. These cycles make it possible to work at excess reactor power of up to 105-110%.

>In case the modernized fuel is used, present-day fuel cycles for VVER-440 also make it possible to realize the maneuvering reactor operation mode, when the reactor power varies in wide frames during a short time period.

