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LATTICE MEASUREMENTS WITH 19-ELEMENT NATURAL URANIUM METAL ASSEMBLIES

PART I: BUCKLINGS FOR A RANGE OF

SPACINGS WITH D₂0 AND He COOLANTS

by

K.J. SERDULA and R.E. GREEN

Chalk River, Ontario October 1965

AECL-2516

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ABSTRACT

Bucklings derived from activation measurements in the **ZED-2** reactor are given for 19-element natural uranium metal assemblies. Measurements were made in triangular arrays of 55 assemblies at pitches in the range 20 to 40 cm. "~oolants" used were ;

- (1) D_{2} O of moderator purity,
- (2) He to simulate a voided condition.

Bucklings obtained with He as coolant are higher than those for D₂0 coolant for the pitches investigated. 2

CHALK RIVER, ONTARIO

OCTOBER, 1965.

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 $\frac{1}{2}$

$-11-$

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$-111-$

FIGURES

 $\sim 10^{-11}$

 $\langle \rangle$ \mathcal{L}_{max}

 $\frac{1}{2} \sum_{i=1}^{n} \frac{1}{i} \sum_{j=1}^{n} \frac{1}{j} \sum_{j=1}^{n$

 $\hat{L}_{\rm{max}}$ \sim

1. INTRODUCTION

Experimental values of reactor physics parameters of cluster fuel are required to test the models or recipes used to predict the nuclear properties of lattices with fuel channels having the complex geometry required to provide the necessary heat transfer characteristics. This report describes buckling measurements for 19-element natural uranium metal fuel assemblies moderated with heavy water, which formed one part of a program of lattice parameter measurements for fuel assemblies having large neutron absorption areas. Earlier measurements on heavy-water-moderated, natural-uranium-metal cluster lattices⁽¹⁾ covered a limited range of pitches and the 19 elements of the cluster were arranged in a hexagonal pattern. In present studies the 19-element clusters were arranged in a circular CANDU-type $\arctan(2)$ with the clusters enclosed in a simulated coolant tube which enabled studies to be made both with and without D₂0 coolant.

Bucklings derived from Mn activation measurements and cellboundary **In** Cd-ratins **were measured** in a triangular array of 55 assemblies in the ZED-2 reactor. Bucklings are given for both D₂0 and He coolant for the following lattice pitches; 20, **22, 24, 26, 28, 32,** 36 **and** 40 cm. The spatial distribution of the In Cd-ratio was measured at pitches of 20, 24 and 28 cm, and the relative In/Cu activation ratio at a pitch of 40 cm.

Radial bucklings were derived from spatial Mn activation distributions using a two-group homogeneous diffusion theory modcl for **a** finitc cylindrical reactor with a radial rellectur. **The** axial distributions well removed from the core boundaries were fitted to a cosine function. Total bucklings (radial plus axial) are corrected to a moderator condition of 25°C and 99.72 atom $% p_{0}$.

2. ONE-GROUP AND TWO-GROUP DIFFUSION THEORY

The homogeneous two-group diffusion equations for the fundamental radial distributions of the thermal neutron flux ϕ_{th} and fast flux ϕ_f in an infinite cylindrical reactor with a radial reflector can be expressed as **(31,**

$$
\phi_{\text{th}}(r) = A^{T}J_{0}(\lambda r) + C^{T}I_{0}(\beta r) - - - - (1)
$$

$$
\phi_{f} (r) = S A^{T} J_{0} (\lambda r) - S^{T} C^{T} J_{0} (\beta r) - - - (2)
$$

respectively, while for a reactor of finite length with the origin located a distance z from the flux maximum, the

Iundamental solution of the axial distribution **f(** z) , in undamental solution of the axial distributi
omogeneous one-group diffusion theory is.

$$
f(z) = \phi(z_0) \cos \alpha (z - z_0) - - - - - - (3)
$$

where

 A' , C' = amplitude coefficients, $S, S' =$ fast-thermal coupling coefficients which depend on **the** cure properties, λ^2 = radial buckling $T = \text{fast-thermal coupling coe:}$
which depend on the core p
= radial buckling
 $T^2 = \text{axial buckling} = \frac{\pi^2}{H}$ H_{ex} = extrapolated height

$$
\beta^2 = \frac{1}{L^2} + \frac{1}{L_s^2} + 2\alpha^2 + \lambda^2 - \dots - \quad (4)
$$

The total geometrical buckling for a finite cylindrical reactor is

$$
B2 = \alpha2 + \lambda2 \t\t - - - - - - (5)
$$

For a neutron detector whose activation cross-section an be expressed as,
 $\frac{1}{\sum_{\text{total}}} = \frac{1}{\sum_{\text{th}}} + \frac{1}{\sum_{\text{f}}}$

- -

where

and $\bar{\Sigma}_c$ are activation cross-sections averaged ω_{th} and ω_{f} are accreation cross-sections averaged
nor the thermal and fast neutron flux distributions respecver the thermal and fast neutron flux dist.
ively, the total activation Act(r,z), is

$$
Act(r, z) = \phi_{th}(r, z)\overline{\Sigma}_{th} + \phi_{f}(r, z)\overline{\Sigma}_{f} \quad - - - (7)
$$

Substitution of (1) and (2) in (7) and neglecting the awstitution of (1) and (2) in (1) and neglecting the state of the induced xial variation gives the radial variation of the induced
ctivity Act'(r) as
Act'(r) = ($\overline{\Sigma}$ +SZ)A'J (λ r) + ($\overline{\Sigma}$ -S'Z)C'I (β r)

$$
Act'(r) = (\overline{\Sigma}_{th} + S\Sigma_{f})A'J_{o}(\lambda r) + (\overline{\Sigma}_{th} - S' \Sigma_{f})C'I_{o}(\beta r) - - - (8)
$$

Equation (8) can be expressed in the general form

 $Act'(\tau) = A J_0(\lambda \tau) + C I_0(\beta \tau) - - - (9)$

where the magnitude and sign of C will be dependent on the detector parameters and the core properties.

Equations (3) and (9), valid for homogeneous systcms, can be applied to a heterogeneous reactor if the neutron flux is measured at identical positions in each cell so **that the macroscopic distribution is not distorted by the** microscopic distribution. This implies separability of macroscopic and microscopic flux variations.

Total bucklings were determined by measuring neutron flux distributions throughout the reactor core and fitting the measured radial and axial distributions to equations (9) and (3) respectively.

3. EXPERIMENTAL

3.1 Fuel and Lattice Arranqements

Figure 1 shows a cross-sectional view of the 19-element uranium metal fuel assembly.

The natural-uranium fuel is that described in AECL- $759^{(1)}$.
Density of the fuel is 18.93 ±0.05 g/cm³. Thirteen cylindrical slugs each 15.2 ± 0.08 cm long and 1.31 ± 0.01 cm in diameter are sheathed in type 1s aluminum tubes of 1.59 cm 0.d. and 1.02 mm wall thickness to form a full-length element.

Elements were arranged in a CANDU-type array, i.e. one element at the center, six on a circle of 3.55 cm diameter and twelve on a circle of 6.85 cm diameter. Each cluster of 19 elements **was** contained in a type 65s aluminum coolant tube with 8.89 cm **0** .D. and a wall thickness of 1-57 **mm to** form a fuel assembly. Table 1 gives the cross-sectional areas of the various materials for a cell.

The minimum sheath-to-sheath spacing of 1.8 **mm** was fixed by a headpiece from which the elements were suspended. Addi**tional constraints were provided by 0.81** mrn **thick A1 plates** drilled to fix the elements on a **CANDU** array. Four plates

were used per cluster, at \sim 5 cm, \sim 60 cm, \sim 110 cm and \sim 160 cm from the bottom of the element sheaths. Not all \sim 160 cm from the bottom of the element sheaths. elements were straight so that the sheath-tu-sheath spacing varied from its nominal value by \leq 0.6 mm between positioner plates.

The assemblies were suspended from the rod hangers by a length of stainless steel chain attached to a stainless steel bolt threaded through the headpiece to which the coolant
tube flange was bolted. (See Figure 2). This arranger tube flange was bolted. (see Figure 2). This arrangement allowed the bottom of the element sheaths to be suspended \sim 1.7 cm above the bottom of the coolant tube, a feature which allowed free passage of the coolant. Heavy water **coo3ant was** expelled through the bottom of the fuel assembly by the introduction of pressurized helium through a Poly-£10 coupling located on the top plate of each fuel assembly. **(see Figure** 3).

Fifty-five fuel assemblies were used fox measurements in **the** triangular **arrays** with pitches of 22 to **40** cm, inclusive, both with **D20** and He coolants. For the **20** cm lattice a 'driver' region of 36 air-cooled 7-element $\overline{U_0}$ assemblies(4) surrounded the central 55 **assemblies** to produce criticality with a moderator height less than the fuel height. The 'driver1 region was also used in some measurements at 24 cm pitch.

Heavy water purity decreased from 99.74 to 99.70 atom $%$ **D20** thruuyhout the experimcnts . **The** purity **at any date was** obtained from interpolation of the results of analyses of moderator samples taken monthly.

3.2 Determination of the Geometrical Bucklinq

Total buckling was determined from foil activation measurements made at positions mid-way between fuel assemblies. Figures 4 and 5 show the radial locations of measuring thimbles
for two loading patterns. The thimbles contained three foi The thimbles contained three foils 10 cm apart at elevations near the vertical flux maximum except for the two central thimbles which contained detectors spaced at 10 cm intervals over the entire moderator **height. Detectors** fixed to aluminum backing plates were substituted for blank backing plates at the required locations in the suspension system. The backing plates were joined by lengths of 0.076 cm diameter Zircaloy wire. The wire-foil system was suppor The wire-foil system was supported in an air-filled aluminum thimble of a cruciform cross-section. The main components of the thimble system are illustrated in Figure 6.

Manganese and copper foils were used as neutron detectors. The $Mn(11\% Ni)$ circular foils are 1.13 cm diameter, weigh \sim 85 mgm and are fixed to 25 x **20 x** 0.5 **mm** A1 backing plates. The foils have been intercalibrated by irradiation to an accuracy of \sim ±0.25%. The Cu foils are of identical area, weigh \sim 115 mgm and are glued to the backing plates. Sensitivities of these latter foils were assumed to be proportional to their weights which are known to a relative accuracy of \sim ±0.2%.

After irradiation the induced 2.58 hr Mn **56** activitg was measured with a TQQB electroscope while the 12.8 hr $\text{Cu}^{\text{6}\text{4}}$ γ -activity was counted with a NaI(T1) scintillation counter. At least two irradiations were performed at each pitch with each coolant.

3.3 Measurement of Spectrum Parameters

Macrnscnpi r neutron-spectrum parameters were measured in D20-cooled lattices at pitches of 20, 24, 28 and **40 cm.** All measurements were made at moderator positions mid-way between **fuel clusters. For the 40 cm lattice the relative I~/CU** ratio was derived from the activity induced in Cu foils (as described above) and in similar Pb-In foils, **0.8** In by weight, **Cadmium ratios wcre measured with the Pb-In foils at other** listed pitches. For Cd-ratio measurements foils were enclosed in either 0.030" thick Cd or A1 boxes cemented to A1 backing **plates. Detectors were placed every 10 cm along the** vertical in thimbles KlW and KlE (Figure 4) and radially throughout the core at either two or three elevations near the flux maximum. **Induced y-activities** were **cuurlted with** a **N~I(T~)** scintillation counter.

3.4 Critical Height Measurements

An accurate determination of the critical **D20** level in the **ZED-2** calandria was required for a determination of foil loading corrections and derivation of axial extrapolation lengths. Measurements of the moderator height were made with the accurate height indicator described in AECL-1505. Height differences due to 'loading' effects were accurate to ~±0.003 cm. Foil elevations with respect to the moderator level, as required for derivation of axial extrapolation lengths were accurate to \sim to.2 cm.

3.5 **He-Cooled Latticcs**

Measurements with He coolant in the 55 assemblies were made by **expelliny** the **D20 coolant into the moderator** region through a hole in the bottom of the coolant tube. This was accomplished by varying He pressure in a Poly-£10 tube attached to the top of each **dssembly which altered** the level of the D_2O coolant. (Figure 3). D₀0 coolant level relationship was determined experimentally by observing the pressure required for the onset of **bubbling** from the bottom of the assembly for different D_2O levels. During a He-cooled irradiation all but \sim 1 cm of D₂0 was excluded from the assemblies.

4 **DATA ANALYSIS ANDRESULTS**

4.1 Neutron Activation Distributions

The counting data from measurements with the Mn-Ni foils were corrected for exponential decay, detector sensi-
tivities, background and electroscope drift, Relative tivities, background and electroscope drift. activities were obtained by normalizing to the activity of a foil located near the maximum neutron flux in the core.

y-counting data from measurements with Cu foils were also corrected for exponential decay, detector sensitivities, **dead-time losses** and background.

Normalized and corrected activities obtained from each **irradiation are given in** Tables 1-A to 36-A, Appendix A. The radius, elevation and exact position in the core (refer to Figures 4 and 5) are given for each foil. Foil elevations and **the critical moderator height. h, are** both measured with respect to the ZED-2 zero plane, i.e. the elevation of the central region of the calandria bottom.

4.2 Derivation of the Geometrical Bucklings

Corrected axial distributions, well-removed from the core boundaries, were fitted by the method of least-squares to the cosine function given by equation (3). Bracketed activities as given **in** the **tables of Appendix A were** not included in the fit. The average of the two values of α and z_0 obtained from each irradiation is listed in the tables.

Radial distributions were fitted by the method of least-squares to equation (9) but with a fixed value of **^B** calculated from equation (4) . Values of L^2 and $L^2_{S,\epsilon}$ calculated by the Chalk River lattice recipe POOOF (5) for a moderator condition of 25°C and 99.75 atom $%$ D₂0 were used. These are listed in Table 11. The fitted value of *a* was used and *h* was at **first** approximated by the value obtained from a $J_0(\lambda r)$ fit to activities obtained in a region of constant Cd-ratio. This fitting procedure was adopted after only limited success **was** achieved whcn all four **para**meters, A , λ , C and β were allowed to vary in the fit. Even in the latter cases when convergence was attained the fit error calculated for λ was \sim 50% and it was concluded that radial bucklings should be obtainable from the measurements to a higher precision. The determination of radial buckling by the above method is described in more detail in $(6, 7)$.

Six values of λ were obtained from each irradiation by combining the west-plus-south (W+S) and east-plus-north (E+N) data for each of the three elevations. $\lambda(n)$, $\lambda(n-1)$ and $\lambda(n-2)$ listed in the tables are the average values of all six results. Here n designates a value derived from Here n designates a value derived from a fit to all radial activities, n-1 the results when the outermost point in each set of data is omitted from the fit and n-2 when the two outermost points in each set are omitted. $\lambda^2(n)$ values are used in deriving the geometrical bucklings given in Tables I11 and IV.

The error quoted for the α , λ and z_n values is

1) the error obtained from the "goodness-of-fit" of the data to the assumed distribution function, or

2) the standard deviation in the mean of the several values obtained for each parameter, whichever is the larger.

4.3 Corrections to Buckling Values

Corrections for foil and thimble loading effects and small temperature and purity variations during the period of measurements had to be applied to obtain a consistent set of buckling values to compare with lattice calculations.

Corrections for the 'loading effect' were obtained from measurements of the critical height with and without thimbles and foils in the core. It is assumed that the radial buckling is independent of loading and critical height and therefore α_{CORR} is

$$
\alpha_{\text{CORR}} = \frac{\pi}{\frac{\pi}{\alpha_{\text{FIT}} - \Delta h}} - \frac{\pi}{\alpha_{\text{FIT}} - \Delta h}
$$

where

 α_{FIT} = value derived from the fit.

Ah = difference in critical heights with and without foils and thimbles.

Temperature and purity c e ficients of buckling are Temperature and purity coefficients of buckling are
erived from POOOF calculations (5) . The buckling values listed in Tables I11 and IV are corrected to a moderator condition of 25° c and 99.72 atom $\%$ D₀.

No corrections have been applied for variation of **the radial bucklinq with loading because it is assumed to** be negligible. This assumption was verified both analytically and experimentally. The experiment consisted of loading the **ceriLral** region **of one lattice with extra thimbles** and foils. The buckling derived from this measurement agreed with the buckling derived from a measurement with a normal thimble and foil loading. **A f irst-order perturbation theory** model based on one-group, four-region homogeneous diffusion theory and the measured differences in critical height, also indicated that flux flattening **produced** by the **increased** absorption in the central region of the core due to more thimbles and foils per unit volume (see Figure 4), could be ignored.

4.4 Macroscopic Distribution of Cd-Ratio and Relative 1n/Cu ratio

Results of the macroscopic In Cd-ratio and the 1n/Cu ratio measurements for D_2O cooled lattices are summarized in Appendix B. Cd-ratio values (Tables 1-B to 3-B) are ratios of Al-covered to Cd-covered activities for foils irradiated at the same elevation at equivalent radial positions (see Figure 4).

Axial variations of the Cd-ratio are shown in Figure 7 and radial variations in Figure 8.

Results of the In/Cu ratios measured in the 40 cm pitch D_2O -cooled lattice are shown in Table $4-B$. Axial and radial **variations of** relative 1n/Cu ratios are shown in Figures 9 and 10 respectively.

Average values of the In Cd-ratio or relative 1n/Cu ratios for the region where they are constant within individual experimental errors of \pm 3% are listed in Table V. This constant

region is defined by the dotted lines in the figures. Errors in averages are the standard deviation, σ , of all the values within the constant region for the axial and radial plots.

Values **marked** with **an** asterisk have been omitted from the averages. Many of these omissions are justified because the Cd-covers were found to be loose after irradiation.

4.5 Extrapolation Lengths

Analysis of neutron activation distributions yield values for the extrapolation lengths if the core size and critical height are known. The radial extrapolation length **CdIl** be defined as

$$
\delta R = R_{ex} - R_{c} = \frac{2.405}{\lambda} - R_{c}
$$

where

R_c = equivalent core radius defined for a triangular erray by

 $R_C = 0.525 d/\bar{N}$ whcre $d =$ lattice pitch

 $N =$ number of rods, 55 in all cases except the driven lattices.

The total axial extrapolation length 52^+_t can be defined as

$$
\delta Z_{\rm t} = H_{\rm ex} - (h_{\rm c} - 15)
$$

= $\frac{\pi}{\alpha} - (h_{\rm c} - 15) = \delta Z_{\rm u} + \delta Z_{\rm l}$

where

 δZ_{11} , δZ_{1} = upper and lower extrapolation lengths respectively,

 h_a - 15 = distance in cm from bottom of fuel to the critical moderator level.

Values of δR , δZ , δZ and δZ obtained from the flux distributions for all lattices are listed in Tables VI and Errors quoted are derived from the errors in α , λ , VII. z_{α} and h_{α} .

Figures 12 and 13 show the variation of the radial extrapolation lengths with lattice pitch. Plotted values at each pitch are the average of the measurements listed in Tables VI and VII. Axial extrapolation lengths listed in Tables VI and VII are also plotted as a function of lattice pitch in Figures 13 and 14. Lines in the figures are drawn as guides-to-the-eye only and are not the results of a leastsquares fit to the data.

5. DISCUSSION OF RESULTS

5.1 Buckling

Summaries of buckling values for D₂O and He coolants are given in Tables III and IV respectively, and are plotted in Figure 15 as a function of lattice pitch. Figure 15 shows that the maximum buckling is at a pitch of approximately 25 cm for both coolants with the He coolant giving higher values for the range investigated. These results, combined with the critical height measurements (Tables VI and VII), indicate that a positive reactivity effect results from complete loss of D₂O coolant in the cold-clean critical state for the lattices studied.

At a pitch of 24 cm, with both D₂0 and He coolants, three buckling values were obtained. The first value is derived from flux distributions measured in the 55-assembly core when surrounded by a driver region of 36 7-element UO₂ assemblies. The other two values are derived from measurements in the 55-assembly core only. Results agree within experimental errors for the D₂O-cooled lattices but for the He-cooled lattices the "driven" result is slightly outside the experimental errors as compared This may be due to the existence to the "undriven" results. of anisotropy in the air-cooled lattices or larger uncertainties in the measured bucklings than those quoted. At this pitch the 55-assembly core result is probably more accurate since the neutron streaming effect, if any will be less due to the higher critical height.

Apart from systematic effects the quoted buckling errors vary from 0.01 m⁻² for 40 cm pitch lattices to 0.09 m⁻² for the 20 cm He-cooled lattice.

5.2 Macroscopic In Cd-Ratios and Relative In/Cu Ratios

The measurements indicate that these ratios are constant within experimental errors at radial positions
 \le 2.6 x d (d = lattice pitch), for all lattices studied. At a pitch of 20 cm the In Cd-ratio at radial positions beyond 2.6 x d does not rise as rapidly due to the presence of the surrounding driver region (see Figure 7.

From the axial plots the region of constant ratio for all lattices studied was found to be:

40 cm \leq Z \leq h -25, h = moderator critical height within experimental errors.

Individual measurements agreed with the average values listed in Table V to better than ± 3%.

5.3 One-Group and Two-Group Models in Analysis

Although analysis of axial distributions was based on homogeneous, one-group diffusion theory, analysis for the radial component of the buckling was based on two-group theory.

Use of the two-group model was considered to be warranted after analysis of activation distributions obtained with the improved measuring techniques discussed indicated a systematic crror in the derived radial bucklings. The error increased as the radius of the region analyzed was decreased. A more detailed report of this investigation and adoption of the two-group formulation is given in (γ).

Similar trends did not exist as points within the selected region of the axial distributions were omitted in the analysis of the axial distributions.

5.4 Extrapolation Lengths

Radial and axial extrapolation lengths are plotted in Figures 11 to 14 and summarized in Tables VI and VII. Radial extrapolation lengths derived from measurements with D₂0 coolant are generally less than He coolant values for all pitches except 20 cm. From Figures 11 and 12 the radial extrapolation length appears to be constant within ± 2 cm for lattice pitches in the range 24 to 32 cm with either coolant.

Total axial extrapolation lengths exhibit the same trend as the radial lengths, i.e. D_2O -cooled values are lower than He-cooled values. Derived upper axial extrapolation lengths are considerably greater than the theoretical This could be due to neutrons values given by 0.71 λ_{tr} . arising from

- 1) backscattering in the graphite reflector and
- 2) backscattering and production in the fuel itself,

since both fuel and moderator extend above the critical moderator height.

Present values of extrapolation lengths and previous ones(4) should assist in predicting critical sizes of cores in ZED-2. They should also be of value in assessing the effective worth of reflectors.

6. CONCLUSIONS

Buckling values have been obtained for 19-element natural uranium motal fuel assemblies both with D₂0 and He coolants for triangular arrays with pitches from 20 to 40 cm, For this range of pitches the He-cooled lattices inclusive. yielded higher bucklings.

Spatial distributions of the In Cd-ratio with D₂0 coolant were measured at pitches of 20, 24 and 28 cm and the distribution of relative In/Cu activation rates was measured at a pitch of 40 cm also with D₂0 coolant.

Extrapolation lengths derived from flux plots yield information on reflector effectiveness in ZED-2.

ACKNOWLEDGEMENTS

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REFERENCES

 $\mathcal{L}^{\text{max}}_{\text{max}}$ and $\mathcal{L}^{\text{max}}_{\text{max}}$

 $\sim 10^{-10}$

 \sim $\lambda_{\rm{max}}$

 \mathbb{R}^2 $\frac{1}{2}$

Table II

Values of L^2 and L_s^2 for

Lattices of 19-element Natural-Uranium Metal Assemblies

as Calculated by POOOF*

For moderator conditions of 25°C, 99.75 atom $\%$ D₂°

<u> Table III: Buckling Summary - D₂O Coolant - 19-element Natural-Jranium Metal Fuel Assemblies</u>

 $\frac{1}{\sqrt{2}}$ $\ddot{}$

 $\ddot{}$

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+ Loading correction included
* Not included in average - see text, 5.1.

 $-17-$

<u>Table IV: Buckling Summary - He Coolant - 19-element Natural-Uranium Metal Fuel Assemblies</u>

 $-18-$

Table V

 $\bar{\mathcal{A}}$

 \mathcal{L}

 \mathcal{L}

 \hat{A}

Average Values of the Macroscopic In Cd-Ratio or Relative In/Cu Ratio Measured at Cell Boundaries as a Function of Triangular Lattice Pitch

Table VI: Summary of Extrapolation Lengths Measured in ZED-2 10-element D O-cooled Natural Uranium Assemblies $-20-$

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ŀ,

 $\frac{1}{2}$

l.

Table VII: Summary of Extrapolation lengths Measured in ZED-2

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 $\ddot{}$

 $\ddot{}$ $\frac{1}{2}$

 $-21-$

FIGURE I-CROSS SECTION OF 19 ELEMENT NATURAL URANIUM METAL ASSEMBLY.

 22

FIGURE 2 PARTIAL CUT-AWAY OF 19-ELEMENT NATURAL URANIUM FUEL ASSEMBLY

 $\ddot{}$

 $\hat{\boldsymbol{\theta}}$

FIGURE 3 COOLANT EXCLUSION CIRCUIT IN ZED-2

 24

 $\ddot{}$

 $\overline{}$

 $\ddot{}$ $\frac{1}{2}$

FOIL LOADING PATTERN A (6 DIFFERENT RADII) FIGURE 4

 $-25-$

 $-26-$

 $-28-$

RADIAL VARIATION OF IN CD-RATIO (D₂O-COOLANT) FIGURE 8.

 $-29-$

FIGURE 9 AXIAL VARIATION OF RELATIVE In/Cu RATIO FOR 40 cm D₂0-COOLED LATTICE

FIGURE II. RADIAL EXTRAPOLATION LENGTHS SR, MEASURED IN ZED-2 (D₂O COOLANT)

8R, MEASURED IN ZED-2 (He-COOLANT) RADIAL EXTRAPOLATION LENGTHS FIGURE 12:

 $-34-$

FIGURE 14. AXIAL EXTRAPOLATION LENGTHS, 8ZTITOTAL), 8ZLILOWER) AND 8ZUIUPPER)

 $-35-$

 $-36-$

APPENDIX A

Summary of Relative Activation Distributions Measured in Cores of 19-element Natural-Uranium Metal Assemblies

 \mathcal{F}_{max}

 $\label{eq:2.1} \begin{split} \mathcal{L}_{\text{max}}(\mathbf{r}) = \mathcal{L}_{\text{max}}(\mathbf{r}) \,, \end{split}$

 $\sim 10^{-10}$

 $\frac{1}{2}$

 $-38-$

 $\frac{1}{\sqrt{2}}$

 $\begin{bmatrix} 1 & 1 \\ 1 & 1 \\ 1 & 1 \end{bmatrix}$

 $\ddot{}$

 $\frac{1}{2}$

55 19-element U-metal Clusters plus
parior of 36 7-01 metal Clusters plus

g intiver Region of 36 7-element UV and the cooled Clusters and a linear Region of 36 7-element UO₂ (air-cooled) Clusters

 $Table 4-A$: Buckling Data - 22 cm Hex Lattice (p_2 Coolant)

 $\overline{\mathcal{L}}$

 $\ddot{}$

55 19-element U-metal Clusters plus
a 'Driver Region' of 36 7-element UO₂ (air-cooled) Clusters

 $\lambda(n-2)$ 1.7859 ±.0325

 $-41-$

 $-42-$

 $\ddot{}$ $\ddot{}$

 $-43-$

84.00

62.35

60.00

36.00

20.79

12.00

12.00

 $\frac{34.00}{26.35}$ 60.00 36.00 20.79

Radius cm Thimble

Direction

rable $7-A$: Buckling Data - 24 cm Hex Lattice (p_2O_{colast})

 $\mathcal{L}(\mathcal{L})$. The set of $\mathcal{L}(\mathcal{L})$

 \mathcal{L}_{max} .

 $\mathcal{L}^{\text{max}}_{\text{max}}$

 $-45-$

 $\underline{\mathtt{Table 9-A}}\,:\,\underline{\mathtt{Backling}\, \mathtt{Data}-26}\,\,\underline{\mathtt{cm}\,\,\mathtt{Hex}\,\,\mathtt{Lattice}\,}\,(\mathtt{D}_2\mathtt{0}\,\underline{\mathtt{Coolant}}).$

 $\frac{1}{\sqrt{2}}\sum_{i=1}^{n} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$

 $\mathcal{L}(\mathcal{A})$ and $\mathcal{L}(\mathcal{A})$

 $\label{eq:2} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1$

 $\mathcal{L}^{\text{max}}_{\text{max}}$

 $-47-$

 $-48-$

 $-49-$

 $-50-$

 $\mathcal{L}^{(1)}$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{0}^{\pi} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2} \frac{1}{\sqrt{2\pi}}\int_{0}^{\pi} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2} \frac{1}{\sqrt{2\pi}}\int_{0}^{\pi} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac$

 $-52-$

 $\sim 10^{11}$

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 $\mathbb{Z}^{\mathbb{Z}^2}$.

 \mathbb{Z}^2

<u>ت</u> Cklir

 $\label{eq:2.1} \begin{split} \frac{1}{\sqrt{2}}\frac{1}{\$

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\sum_{i=1}^{n} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2n}$

 $\frac{1}{\sqrt{2}}\sum_{i=1}^{n} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2}$

 $-53-$

 $-54-$

 \mathcal{A}^{max}

 $\mathcal{L}^{(1)}$

 $-55-$

Table 20-A : Buckling Data - 20 cm Hex Lattice (He Coclant)

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S $\frac{1}{2}$

 $\ddot{\cdot}$

 $\ddot{}$ \cdots 55 10-element 11-

 $-58-$

 $\ddot{}$

 $\frac{1}{2}$

 $\frac{1}{2}$

 $-59-$

a 'Driver Region' of 36 7-element UJ (air cooled) Clusters

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 $\ddot{}$

 $\ddot{}$

55 19-element U-metal Clusters plus

Table 25-A : Buckling Data - 24 cm Hex Lattice (He Coolant)

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$

 $-63-$

 $-64-$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$

 $\mathcal{L}^{\text{max}}_{\text{max}}$

 $-65-$

 $-66-$

Table 30-A : Buckling Data - 28 cm Hex Lattice (He Coolart)

 $\frac{1}{2}$

 $\ddot{}$

 $\ddot{}$

 $\ddot{}$

 $-67-$

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م $\mathcal{L}(\mathcal{A})$.

 $-68-$

 \bar{z}

 $-69-$

 $\mathcal{A}^{\text{max}}_{\text{max}}$ and $\mathcal{A}^{\text{max}}_{\text{max}}$

 $\Delta \sim 10^{11}$

 $-70-$

 $\widetilde{\mathbf{t}}$ $\frac{1}{1}$ ϵ $Table 34-A$: Buckling Data - 36 cm Hex Lattice (He</u>

 $\frac{1}{\sqrt{2}}$

 $\ddot{}$

 $\frac{1}{2}$

 $\frac{1}{\sqrt{2}}$

 $-71-$

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 $-72-$

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4 n de la posta
De la posta de ੂ $\frac{1}{2}$ $\frac{1}{2}$

 $\Delta \sim 10^{11}$

 $\mathcal{A}^{\text{max}}_{\text{max}}$

 $\mathcal{L}^{\text{max}}_{\text{max}}$

 $-73-$

APPENDIX B

Spatial Distributions of In Cd-ratios and Relative In/Cu Ratios

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2}d\mu\,d\mu\,d\mu\,.$

 $\Delta \sim 10^{11}$

 $-76-$

Table 3-B: In Cadmium Ratio - 28 cm Lattice with D.O Coolant

 \sim

 $\frac{1}{2}$

 $\frac{1}{2}$

 $-78-$