



Evolutionary Design Studies of PHWR Fuel Rods

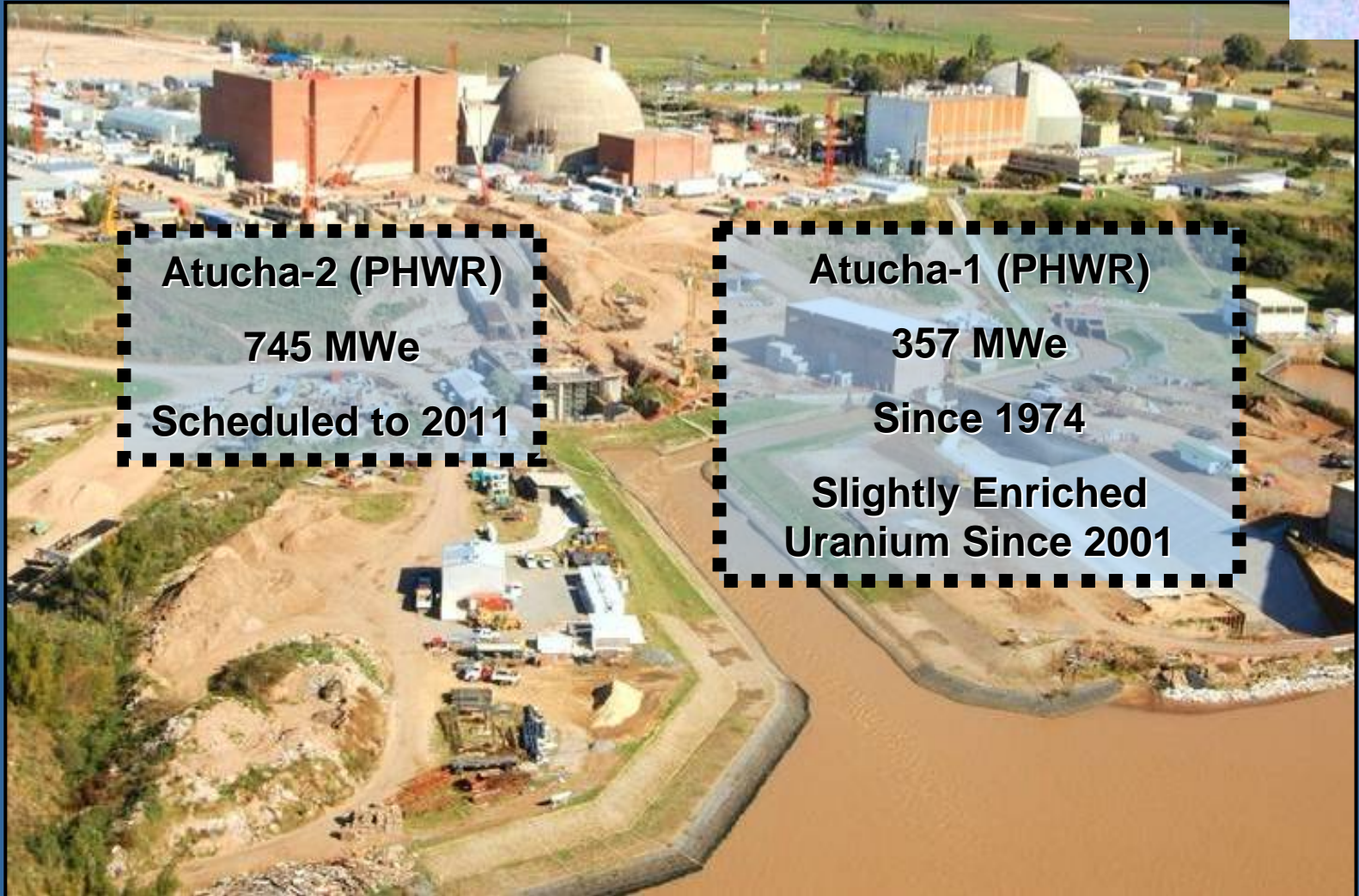
S. Castañiza, L. Alvarez

*Fuel Engineering Department - Atucha-2 Project
National Atomic Energy Commission of Argentina*





Atucha-2 Nuclear Power Plant



Atucha-2 (PHWR)
745 MWe
Scheduled to 2011

Atucha-1 (PHWR)
357 MWe
Since 1974
Slightly Enriched Uranium Since 2001





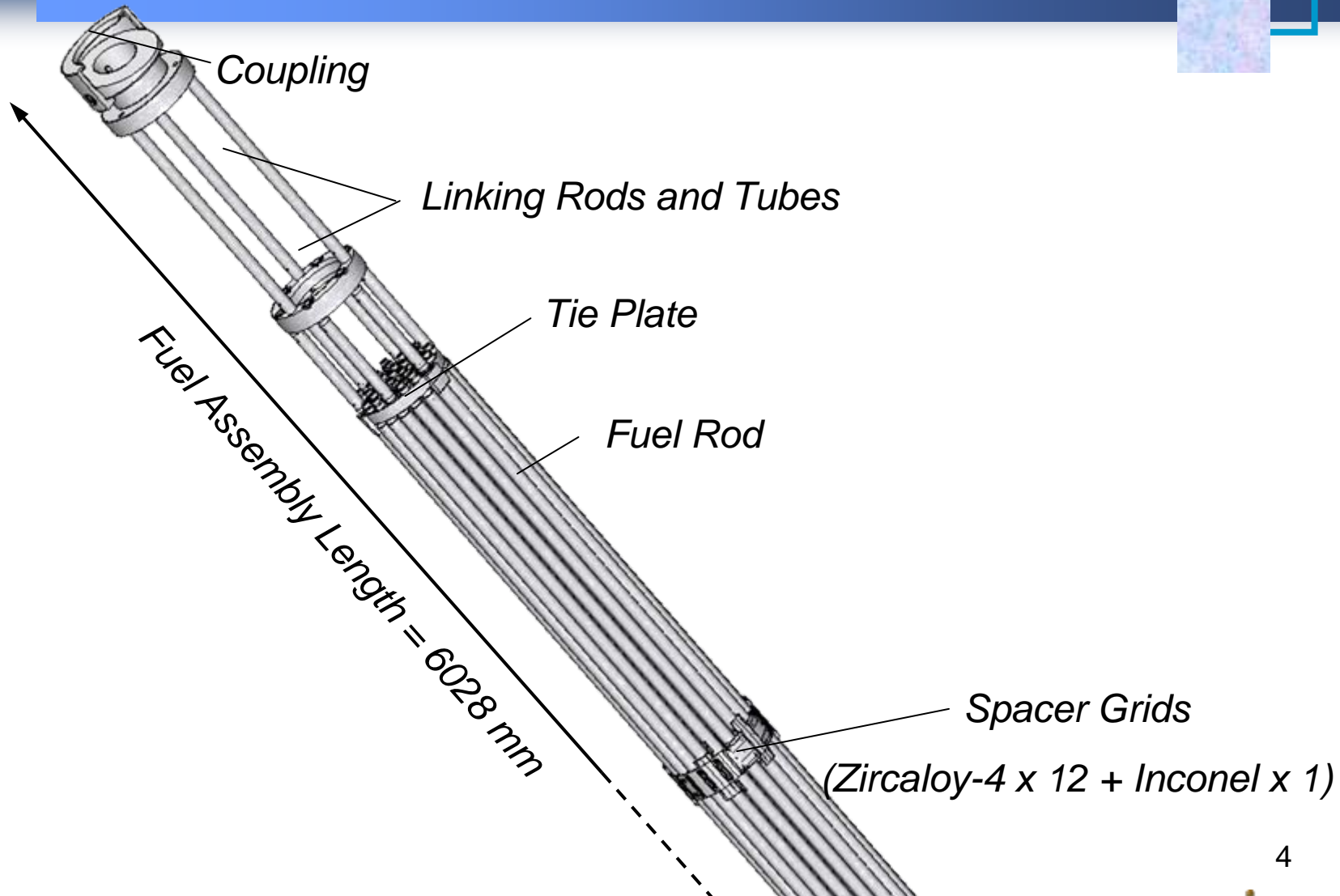
Outline

- 1. Fuel assembly & fuel rod description**
- 2. Design study objectives**
- 3. Calculation methodology**
- 4. Results and conclusions**



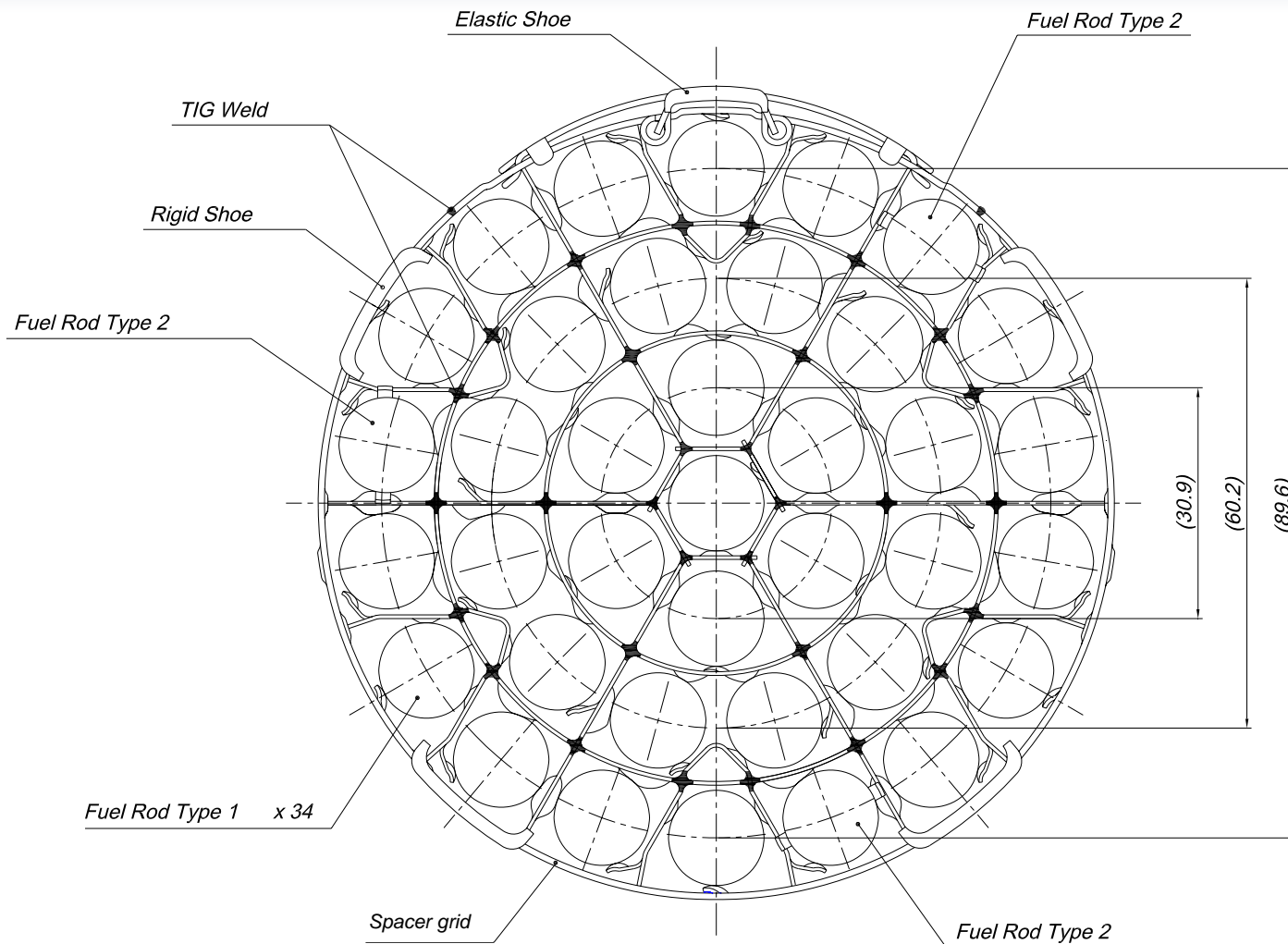


Atucha-2 Fuel Assembly



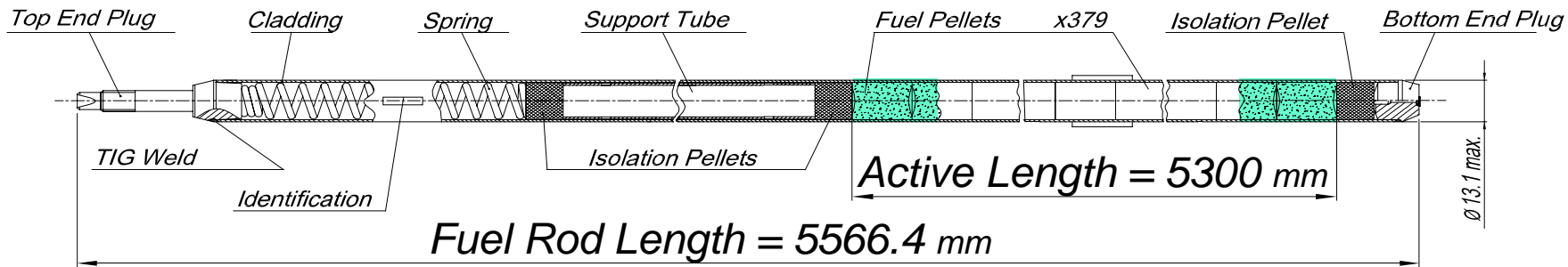


Atucha-2 Fuel Bundle Cross-Section





Atucha-2 Fuel Rod



.....

Zircaloy-4 cladding

Inner diameter = 11.81 mm

Thickness = 0.55 mm

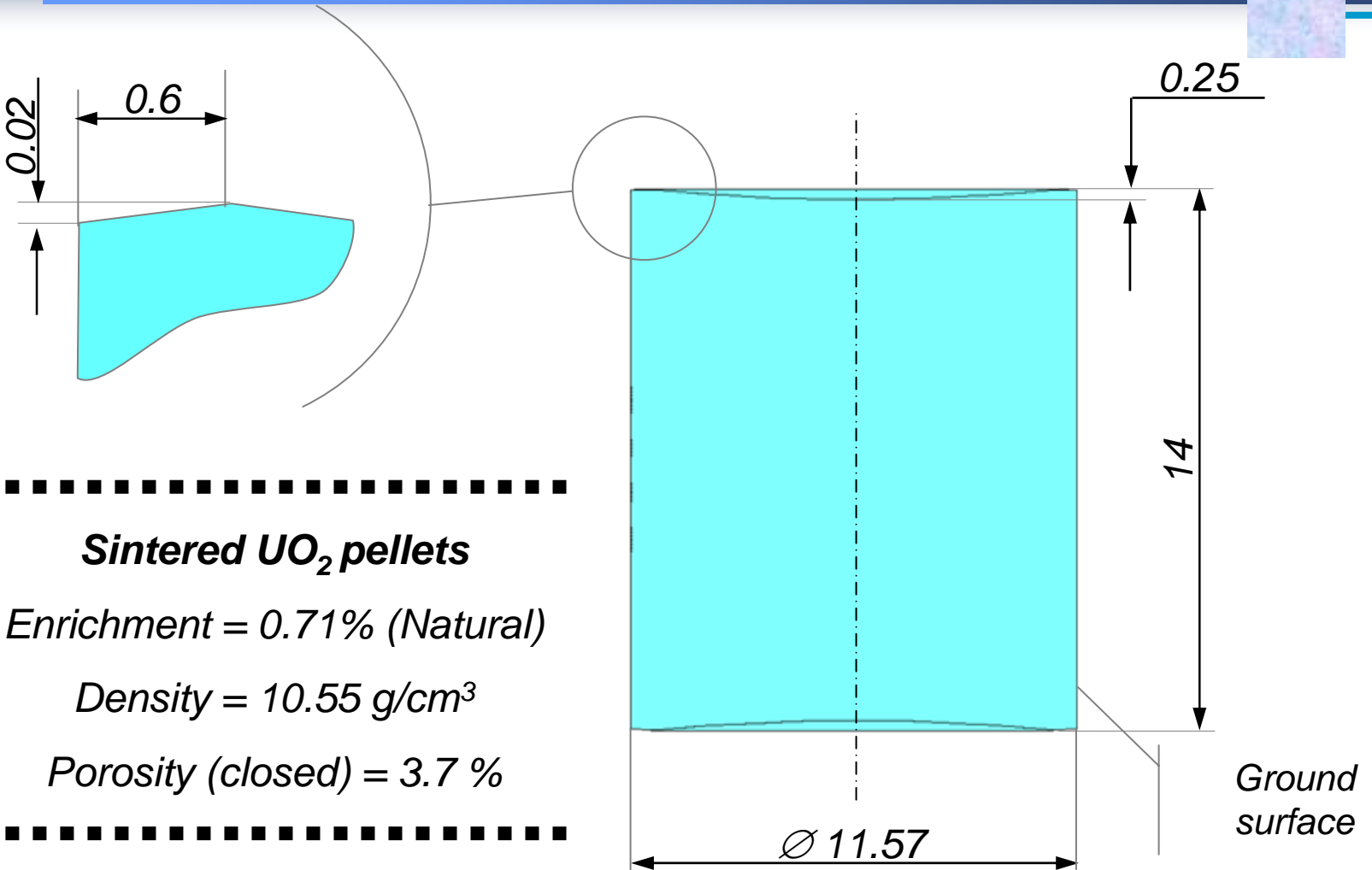
Initial Pressurization = 22.5 bar

.....





Atucha-2 Fuel Pellet





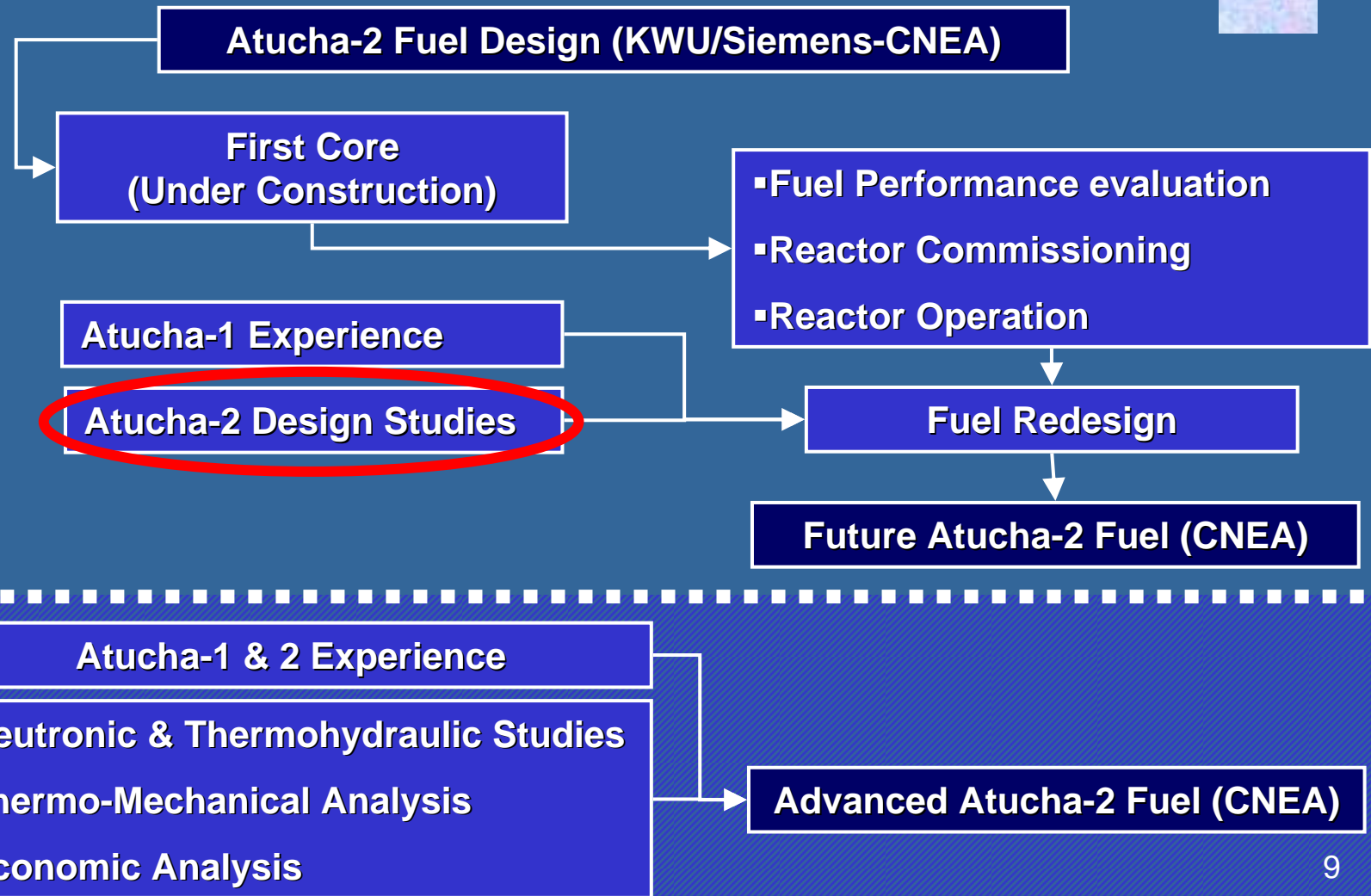
Design Parameters for Atucha's Fuel Rod

	Atucha-1	Atucha-1 (MASU)	Atucha-2
Pellet length (mm)	12	13	14
Pellet diameter (mm)	10.62	10.74	11.57
Pellet length/diameter ratio	1.13	1.21	1.21
Pellet density (g/cm ³)	10.55	10.60	10.55
Dishing depth (mm)	0.30	0.23	0.25
Cladding outer diameter (mm)	11.90	11.92	12.90
Cladding inner diameter (mm)	10.80	10.92	11.81
Minimum clad thickness (mm)	0.505	0.460	0.495
Pellet-cladding gap (mm)	0.18	0.18	0.24





Fuel Engineering Department





Atucha-2 Fuel Assembly





Fuel Rod Design Studies



Studied fuel rod parameters:

1. Fuel pellet density
2. Fuel pellet diameter
3. Fuel pellet length
4. Initial pressurization of the fuel rod

Motivations:

- Evaluate operational constraints of the current fuel rod design
- Generate information to maintain the suitability and safety of future modifications
- Support the possible trends on design modifications
 - ✓ Increase safety margins
 - ✓ Uranium mass increase
 - Increase the residence time
 - Reduce fuel consumption

Background:

MASU Program for Atucha-1: (Similar program applied to Embalse, a CANDU-6)

- Change in pellet length, dishing depth, pellet density, pellet diameter, cladding diameter and cladding thickness
- Nominal uranium mass increase of 6.7%

ULE Program for Atucha-1:

- Use of slightly enriched uranium (0.85%)
- Reduction on fuel consumption by almost duplicating resident time & burnup





Design and Safety Limits

A fuel rod performance code (Siemens/KWU) is used to predict the fuel rod behavior during irradiation

Calculations are performed to determine if any fuel-related design margins are exceeded in normal operational conditions.

The most important for this kind of reactors are:

1. Maximum fuel temperature: **< UO₂ melting ~ 2800° C**
2. Fuel-rod internal pressure: **< coolant pressure = 115 bar**
3. Strain of the clad due to pellet-cladding interaction: **< 1%**

-
4. Maintain the structural design of the fuel assembly. Like cladding outer diameter or number of fuel rods





Fuel Rod Code (Siemens/KWU)

- **Input data:** Cladding geometry, pellet geometry, material properties, fuel characteristics, rod plenum volume, pellet stack length, parameters of the models, operation conditions.
- **Geometrical subdivision of fuel rod:** Axial segments of equal length.
- **Geometrical subdivision of fuel pellet:** Concentric annular element of equal mass.
- **Time subdivision of power and fast neutron flux:** Variable time step lengths for a best representation of changes in fuel condition.
- **Conservatism:** Proper selection of input data (tolerances, model parameters, operative conditions) to obtain conservative results.





Simulation of Rod Behavior

Normal Operating Conditions

- Primary system pressure (Coolant) = 115 bar
- Coolant channel inlet temperature = 277.8° C
- Mean coolant channel outlet temperature = 314.6° C

Power History

- Ramp on fresh fuel to the maximum LHGR (**Hot Channel**)
- Simulated power histories (most demanding) with extended burnup (**End of Life**)

Fuel Rod Model

- Selection of geometrical tolerances
- Selection of model parameters

Time Dependent Fuel Rod Thermo-Mechanical Behavior



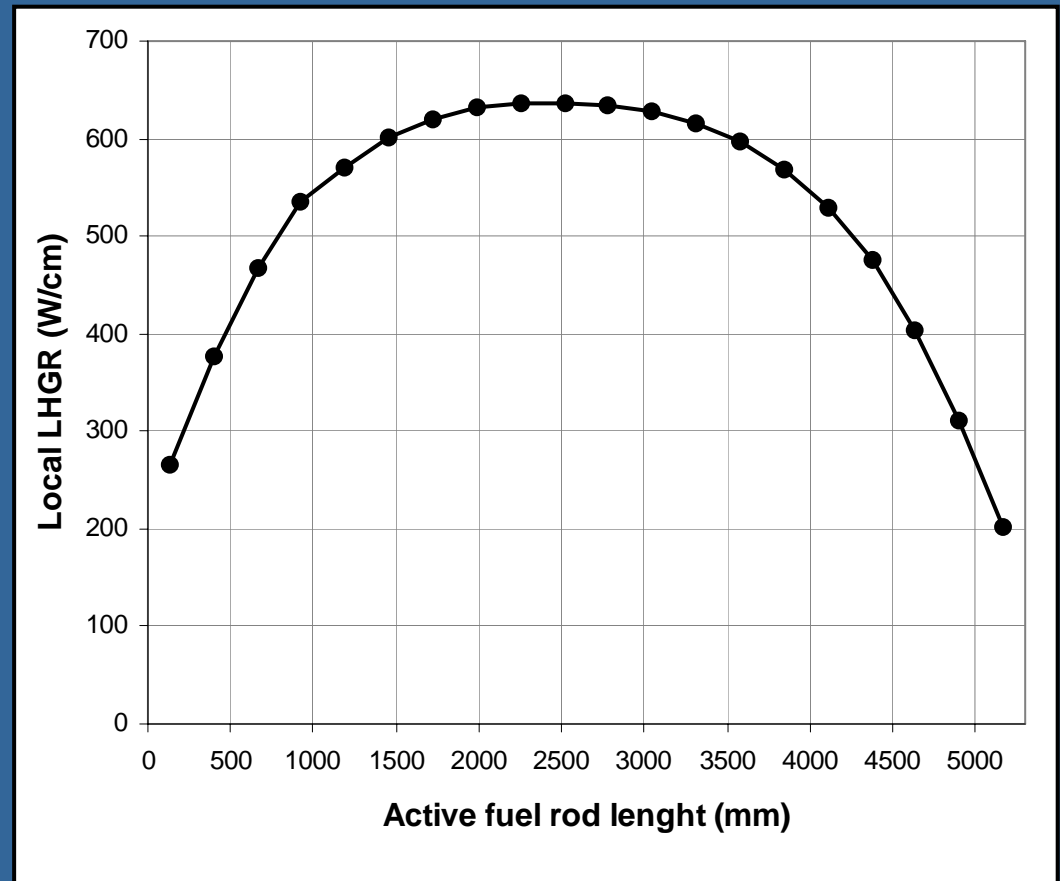


Hot Channel Calculations

**Design Maximum LHGR
640 W/cm**

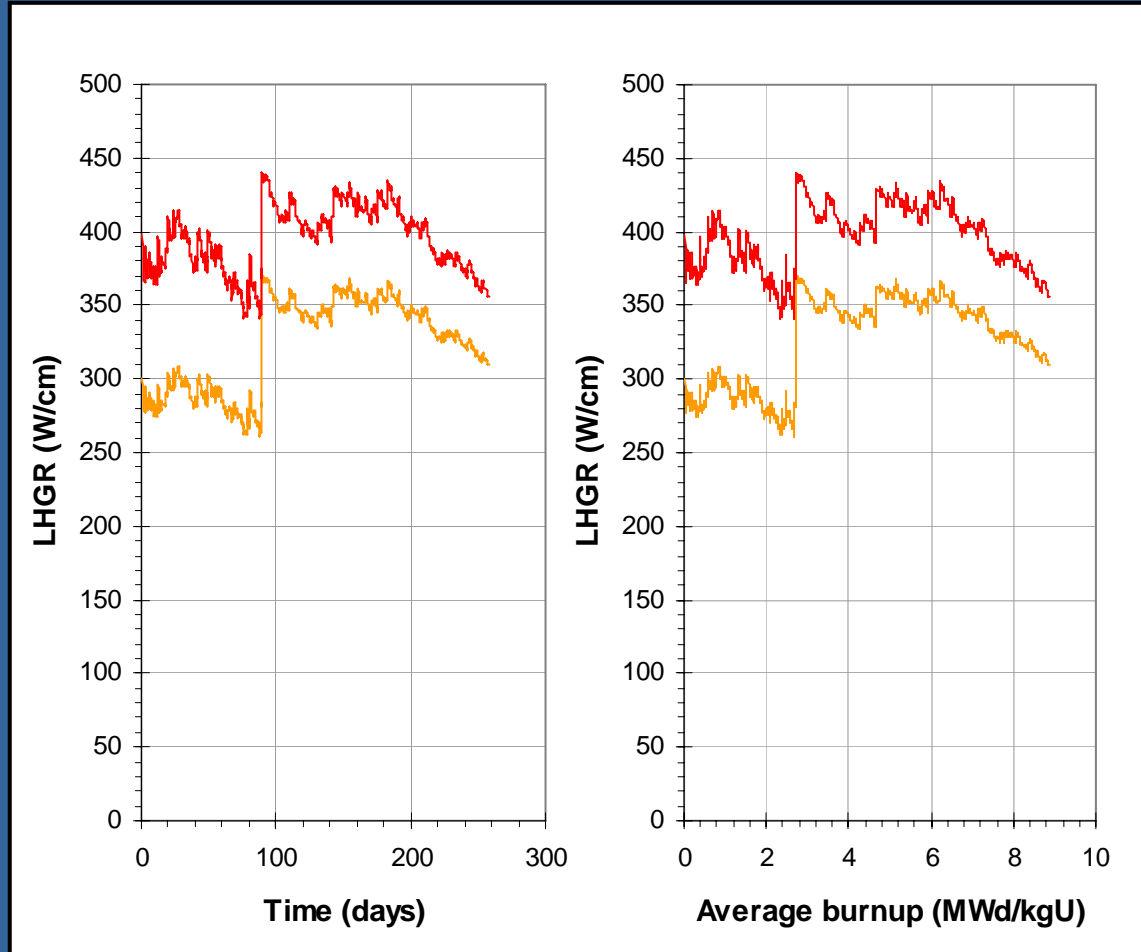
**Maximum LHGR
468.7 W/cm**

**Average core LHGR
237.7 W/cm**





End of Life Calculations



Selected power history, most demanding in:

- Average LHRG
- Dwell time
- Burnup

Extended 160 days to reach 15 MWd/kgU.





1. Study of Fuel Pellet Density

- Current fuel Pellet density 10.55 g/cm^3
- Possible fuel pellet density 10.60 g/cm^3 (Used in Atucha-1)
- Current fabrication tolerances

Hot Channel Calculations

- Cladding strain due to pellet-cladding interaction
- Maximum pellet temperature & fuel rod pressure

End of Life Calculations

- Cladding strain
- End of life fuel rod pressure

No significant impact up to the studied burnup





2. Study of Fuel Pellet Diameter

- Pellet diameter from 11.56 mm to 11.73 mm
- Pellet cladding gap from 0.24 mm to 0.08 mm
- Current fabrication tolerances

Hot Channel Calculations

- Cladding strain due to pellet-cladding interaction
- Power to reach hard contact
- Maximum pellet temperature & rod pressure

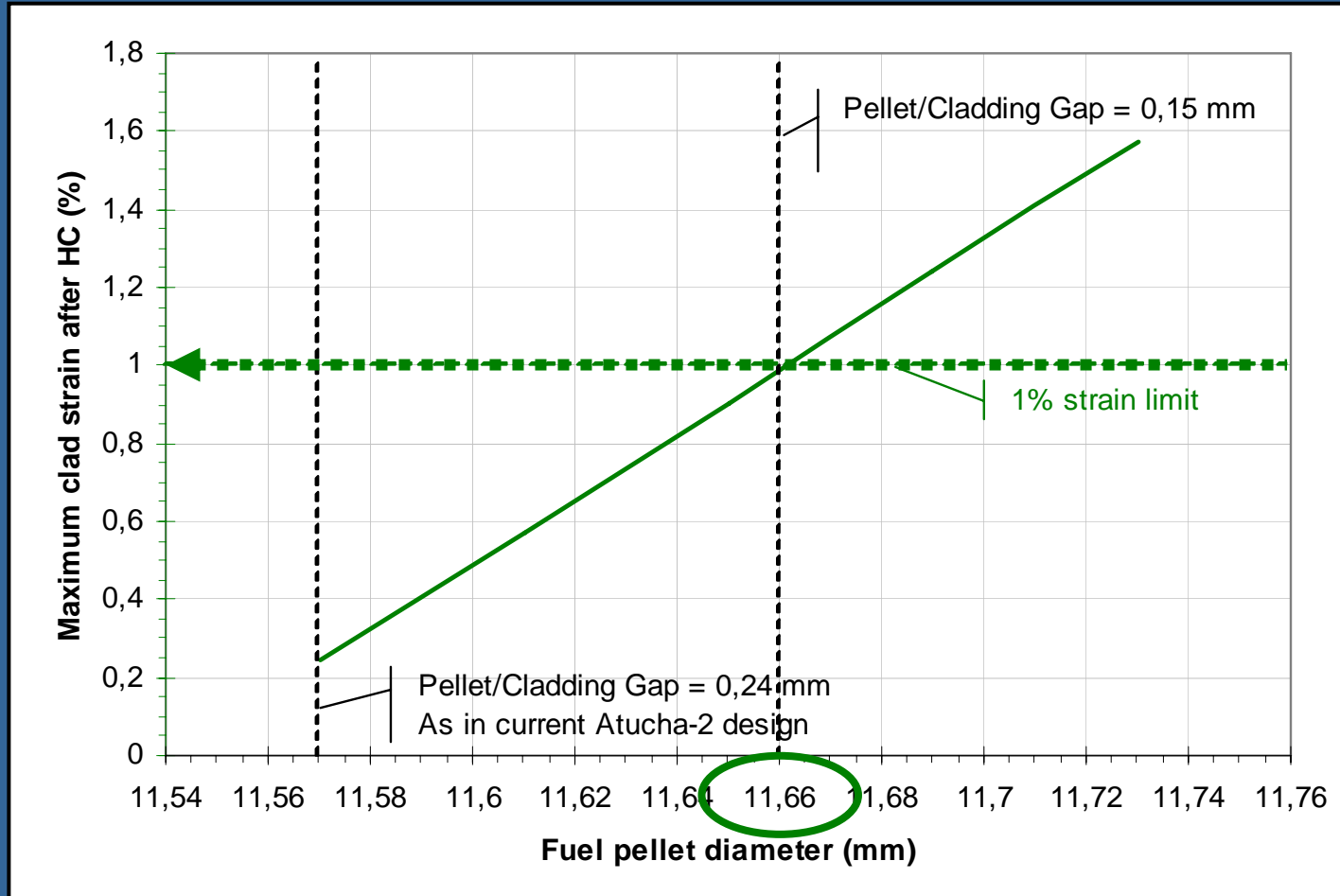
End of Life Calculations

- Cladding strain
- End of life pressure



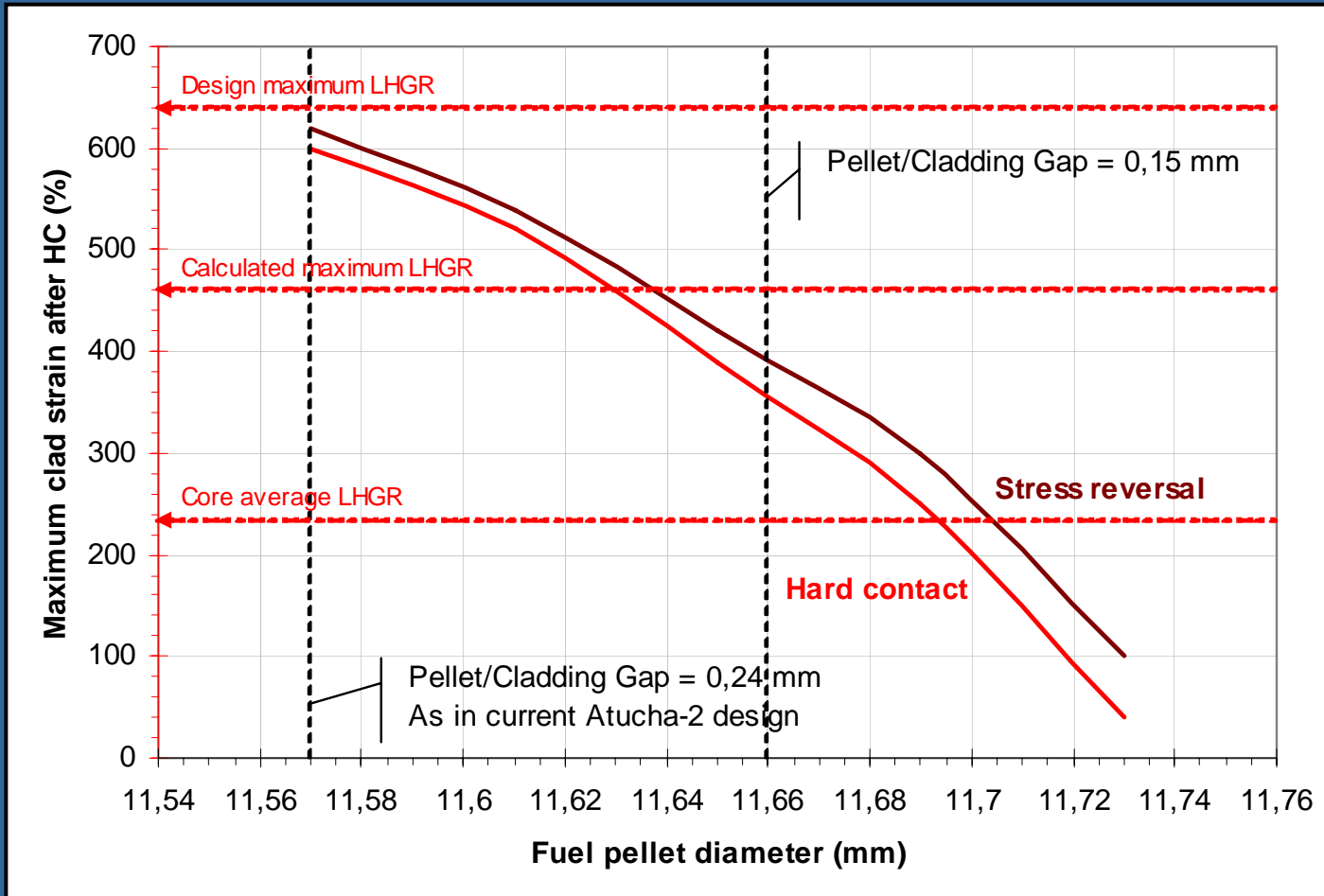


Study of Fuel Pellet Diameter



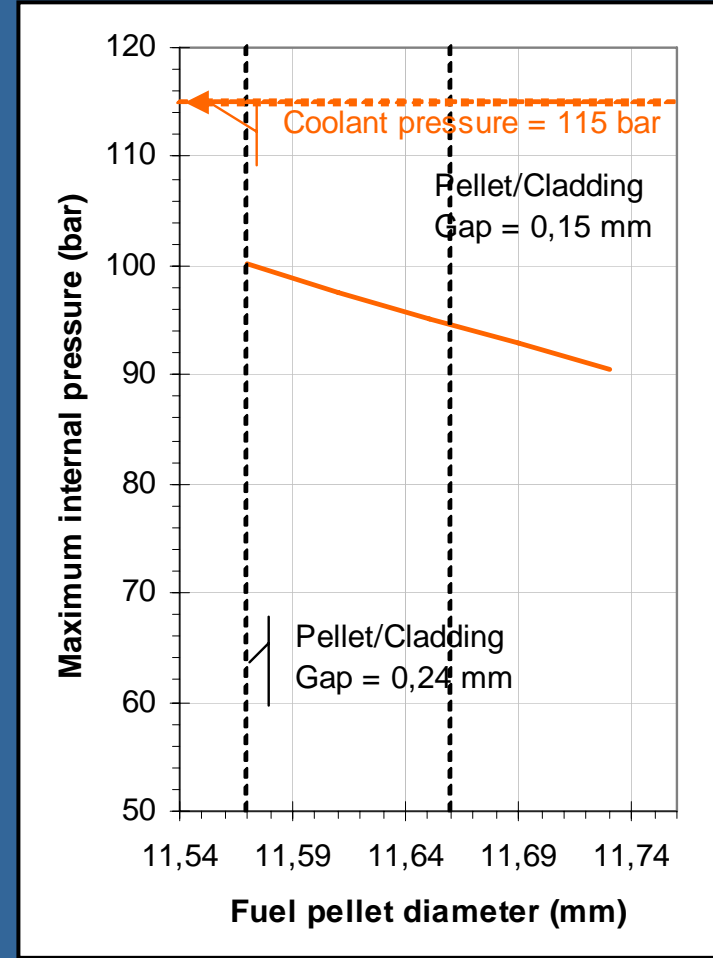
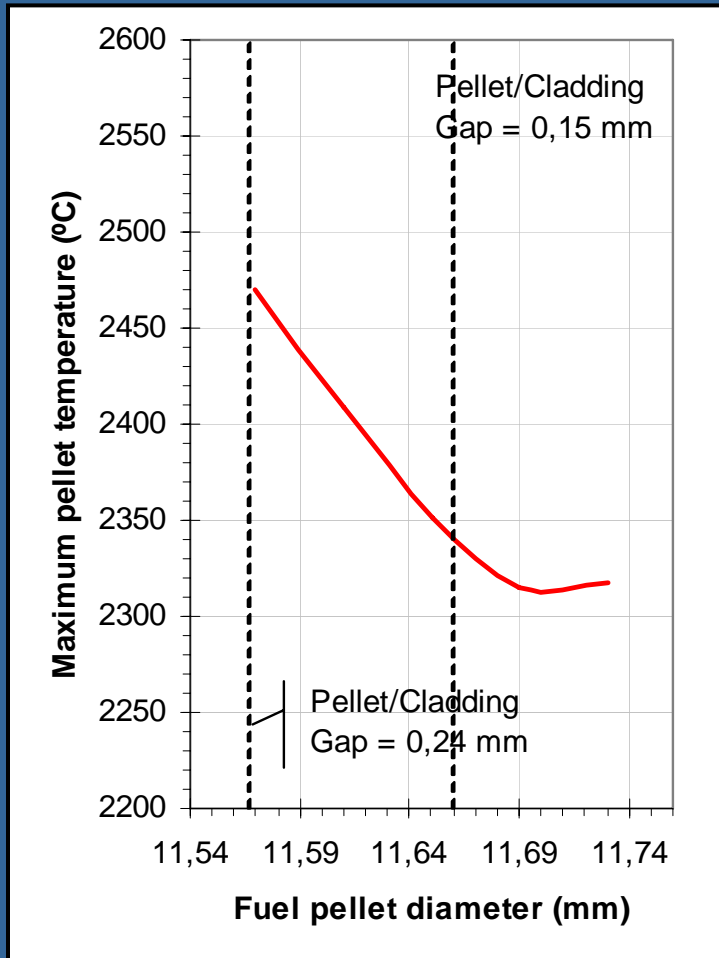


Study of Fuel Pellet Diameter



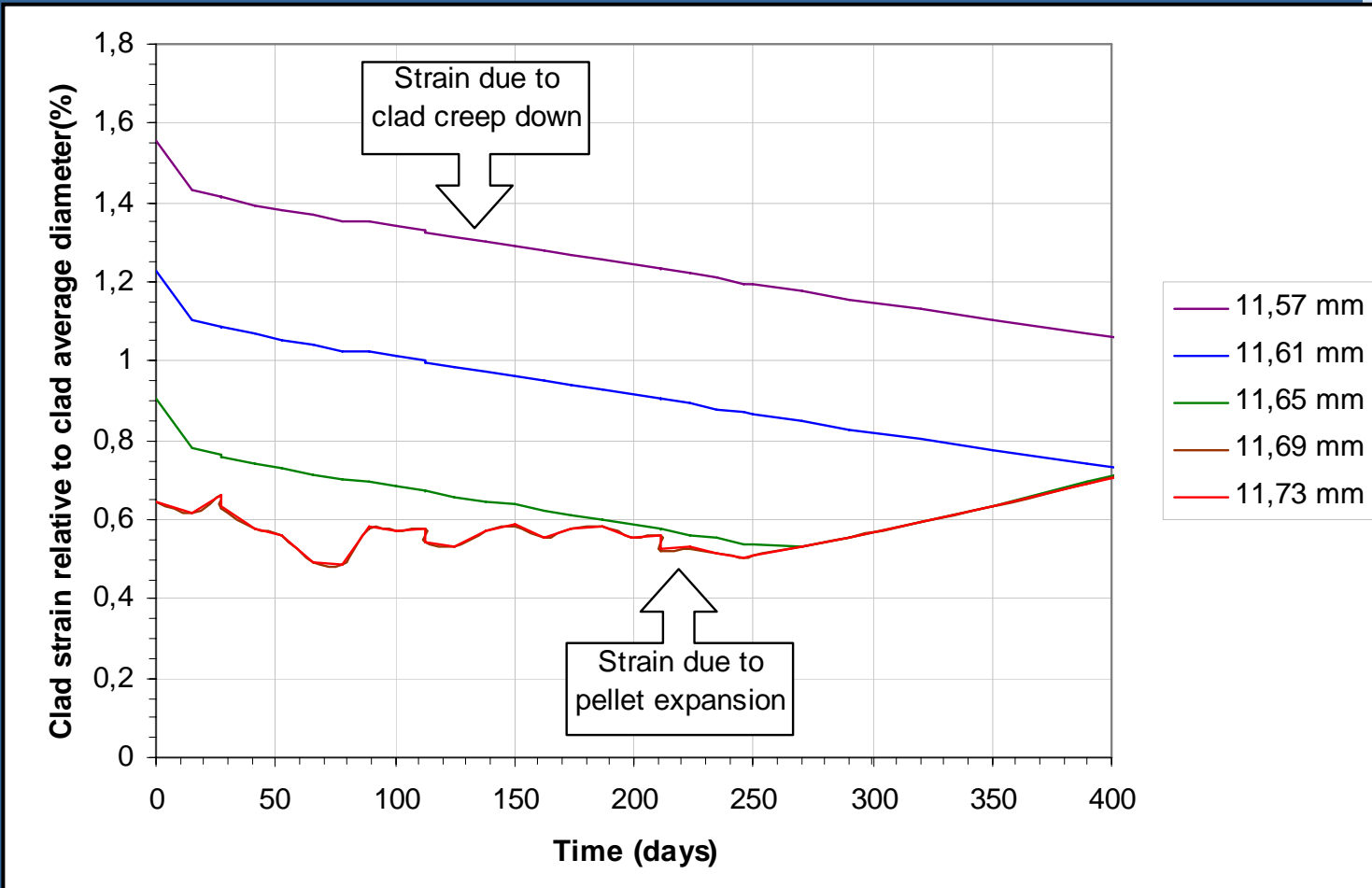


Study of Fuel Pellet Diameter





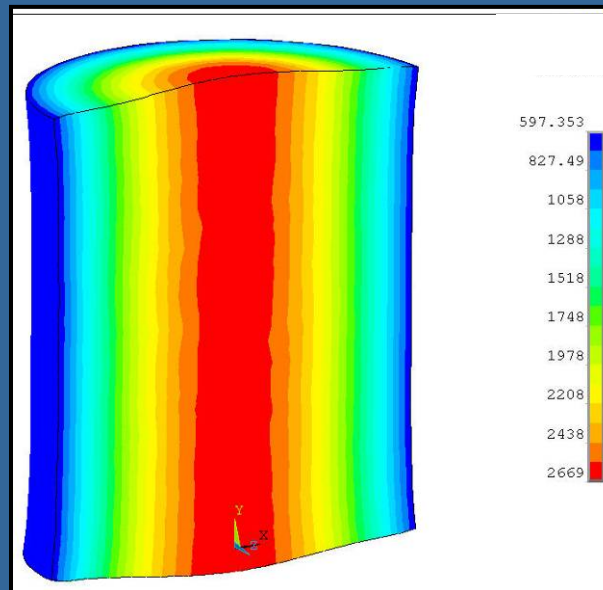
Study of Fuel Pellet Diameter



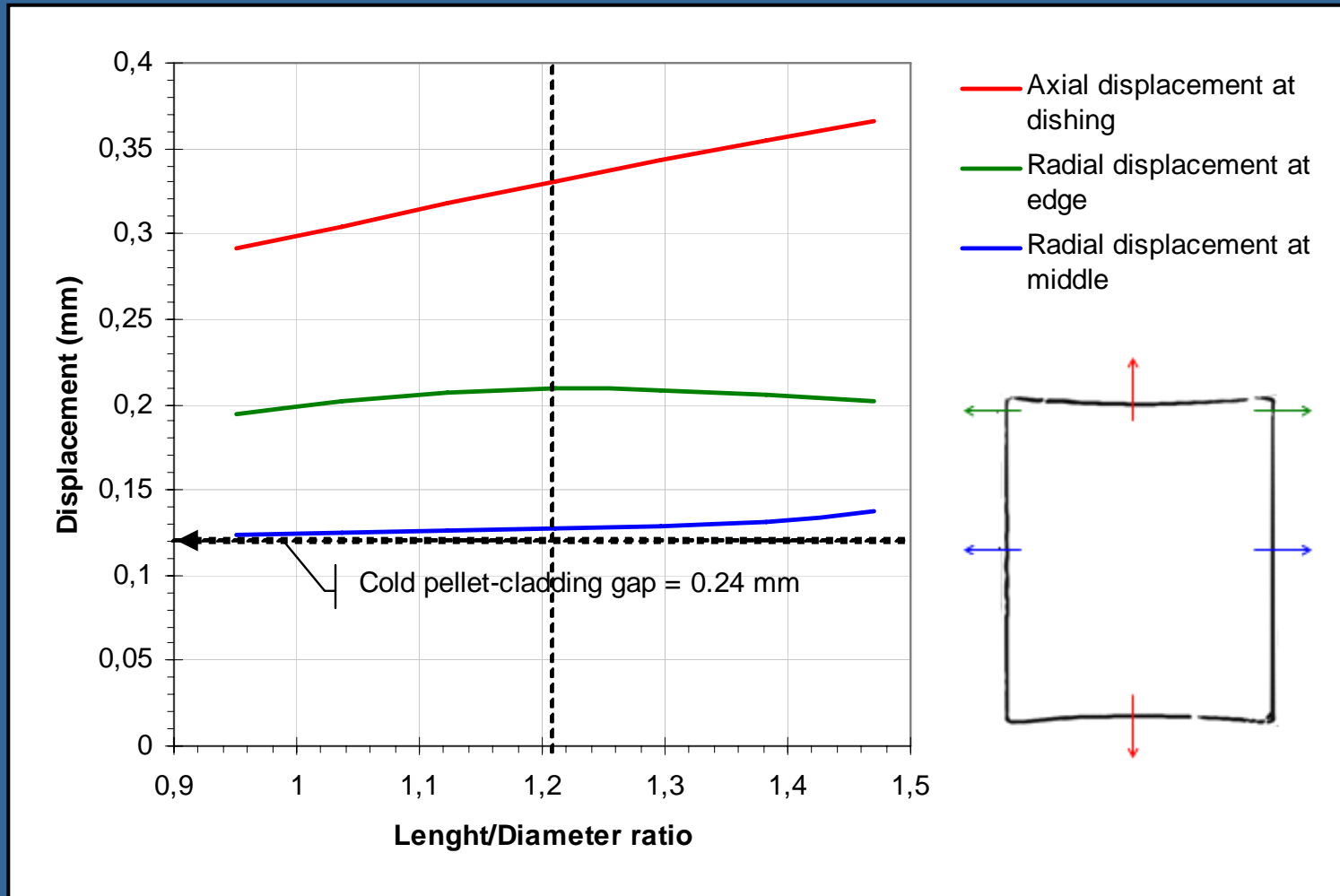


3. Study of Fuel Pellet Length

- Length/diameter ratio from 0.95 to 1.40
- Current fabrication tolerances
- Use fuel **radial temperature profile** (fuel rod output) **at maximum power** (hot channel) to calculate **pellet thermal expansion** by a 3D finite element model of the pellet



Study of Fuel Pellet Length





4. Study of Rod Initial Pressurization

- Rod initial pressurization from 10 bar to 35 bar
- Current fabrication tolerances

Hot Channel Calculations

- Maximum temperature & pressure

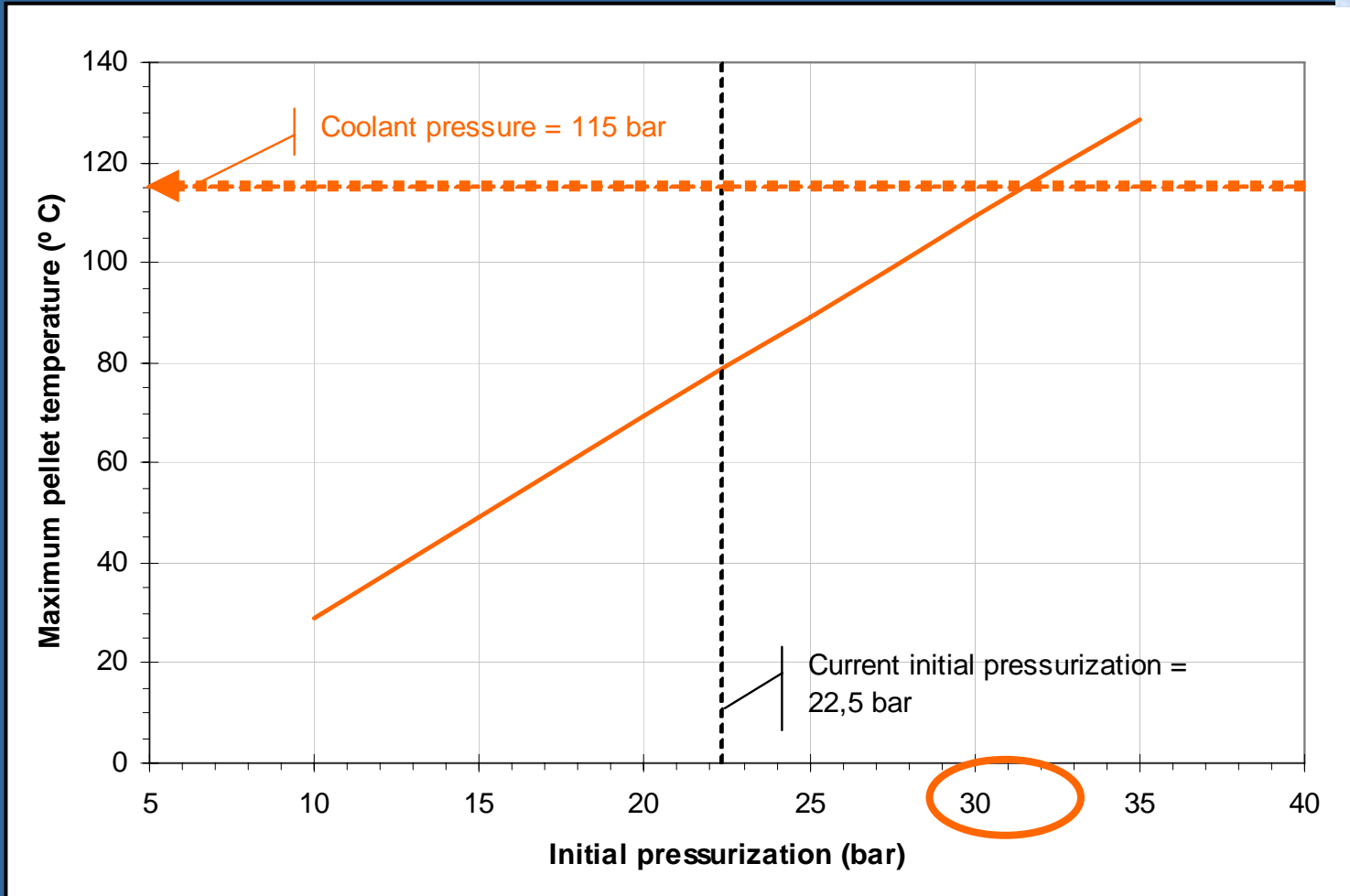
End of Life Calculations

- Cladding strain
- End of life pressure



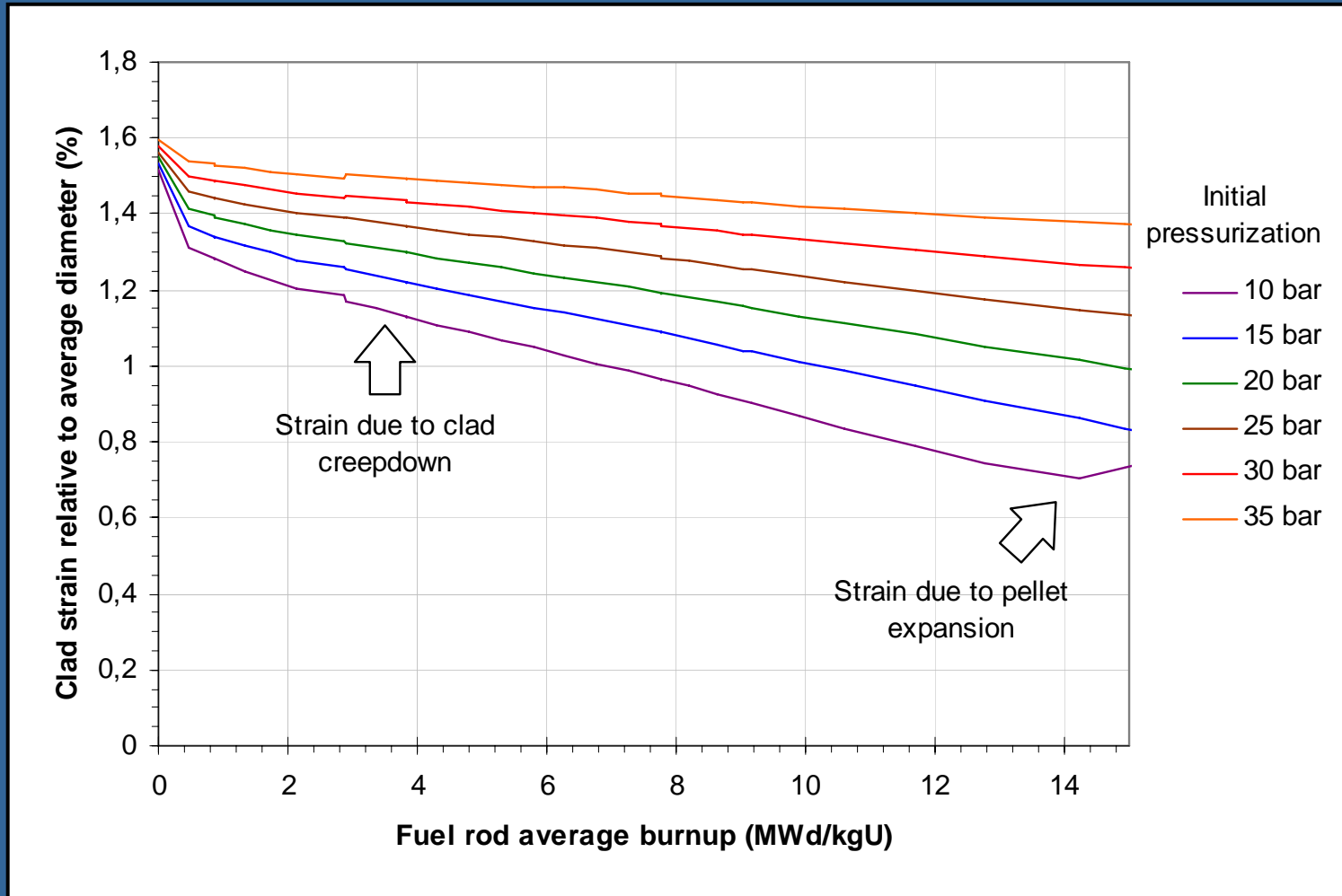


Study of Rod Initial Pressurization





Study of Rod Initial Pressurization





Summary

- **Fuel rod performance for a nominal pellet density of 10.60 g/cm^3 for hot channel and end of life**
- **Minimum pellet-cladding gap to reach the strain limit at hot channel (0.15 mm)**
Safety margins for a range of pellet-cladding gap size
- **Pellet thermal expansion characterized for a range of pellet length/diameter ratio**
- **Maximum initial pressurization to reach coolant pressure at hot channel (30 bar)**
Safety margins for a range of initial pressurization





Conclusions

- Various margins for design improvement has been identified
- Important information for future development of Atucha-2 fuel was obtained
- Conservative models and operative conditions were used in the calculations

▪ Next Steps

- Calculation with other fuel rod codes to compare results
- Studies on more design parameters





Atucha-2 Project

*Fuel Engineering Department
National Atomic Energy Commission of Argentina*

Thank You for Your Attention!!!

Sebastián Castañiza

scasta@cnea.gov.ar

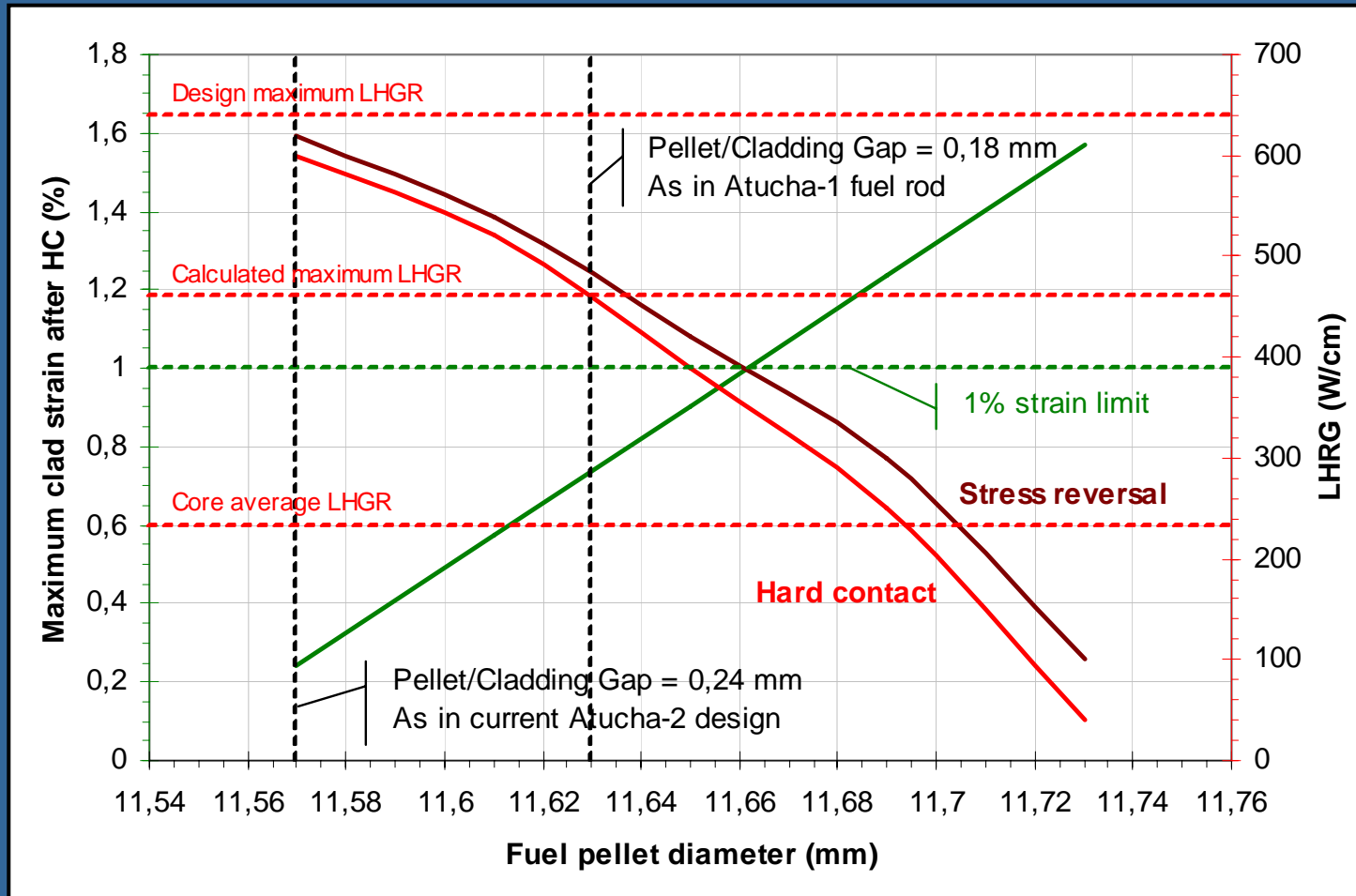
Luis Alvarez

lalvarez@cnea.gov.ar





Study of Fuel Pellet Diameter





Fuel Rod Code (Siemens/KWU)

- Temperatures
- Thermal expansion and elastic deformation
- Thermal and irradiation creep
- Growth induced by irradiation
- Corrosion
- Absorption of hydrogen (deuterium)

Cladding

- Temperatures
- Thermal expansion
- Cracking, radial and axial relocation
- Densification and irradiation swelling
- Restructuring
- Release of fission gas
- Release of residual gases
- Absorption of helium

Pellet

- Pressure
- Temperature and volume of the plenum
- Composition of the internal atmosphere

Rod



