A New Uncertainty Reduction Method for Fuel Fabrication Process and PWR cores with Erbia-Bearing Fuel

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1. Introduction

To achieve the super high burnup

Increasing the 235U enrichment

The 235U enrichment must be less than 5wt% in Japan

Erbia high burnup fuel

- 235U enrichment : >5wt%
- **Erbia** : Er_2O_3

Fuel Fabrication System, Reactor Core

- The erbia addition to the fuel with over 5wt% 235U enrichment retains the neutronics characteristics to those with under 5wt% fuel.
- We have no experience for the reactor cores and the fuel fabrication systems with full loaded erbia
- The use of erbia may produce additional uncertainty of the neutronics characteristics

• The Uncertainty of neutronics chracteristics

The cross section error

Evaluating with the sensitivity coefficient and the cross section covariance matrix

The calculational method error
 Monte-Carlo method

- The standard deviation of the neutronics characteristics
- Deterministic method
 - The self-shielding model
 - The energy condensation
 - The calculational mesh divisions

The production error (manufacturing tolerance)



Improvement of prediction accuracy

1) Bias Factor Method

Measured data of critical experiment

Bias Factor = -

Calculated data of critical experiment

- Bias factor is multiplied to calculated neutronics characteristics for a target system to improvement the accuracy
- Simple and easy to apply to design calculations

2) Cross Section Adjustment Method

- The method can utilize a wide range of neutronics characteristics
- Use of many experimental data
- Reliable cross section

2. Calculational Method

The effective neutron multiplication factor of the erbia bearing fuel system

$$\frac{1}{k_{eff}} = \rho + \frac{1}{k_{eff,0}}$$

O : the erbia worth

 $k_{e\!f\!f,0}$: the neutron multiplication factor of the system without the erbia

The uncertainty of the k_{eff} $\frac{1}{(k_{eff})^2} d(k_{eff}) = -\rho G_{\rho} \Delta \sigma + \frac{1}{k_{eff,0}} G_{k_{eff,0}} \Delta \sigma$

The variance of the k_{eff}



The uncertainty of the $k_{eff,0}$

Using the bias factor method or the generalized bias factor method

$$G_1 = G_{\rho} \rho$$
 $G_2 = \frac{1}{k_{eff,0}} G_{k_{eff,0}}$

 $V_{\rm Er}$: The cross section covariance matrix of Er V_{σ} : The cross section covariance except for Er

Bias factor method The $k_{eff,0}$ of the target core The measured $k_{eff,0}$ for the mockup core $\widetilde{k}_{eff,0} = k_{eff,0} \times f$ **Bias factor** $f = \frac{k_{eff,0,e}^{e}}{k_{eff}^{c}}$ The calculated $k_{eff,0}$ for the mockup core eff ,0,e $\widetilde{k}_{eff,0} = k_{eff,0}^{0} \left(1 + G_{r,k_{eff,0}} \Delta \sigma \right) \times \frac{1 + \Delta E_{k}}{1 + G_{e,k_{eff,0}} \Delta \sigma}$ The sensitivity coefficient \Box The variance of the $\widetilde{k}_{eff,0}$ of the system $Var(\widetilde{k}_{eff,0}) = \Delta G_k V_{\sigma} \Delta G_k^{t} + Var(E_k)$ $\Delta G_{k} = G_{k_{eff,0}} - G_{e,k_{eff,0}} \qquad G_{e,k_{eff,0}} : \text{the sensitivity coefficient of experimental mockup core}$ $Var(E_k)$: the variance of the measured $k_{eff,0,e}^e$

Generalized bias factor method N experimental data

$$f_i = \frac{k_{e\!f\!f,c,i}^e}{k_{e\!f\!f,e,i}^e} \qquad (i=1,2,3,\cdots,N)$$

Generalized bias factor is determined by

$$\widetilde{f} = \sum_{i=1}^{N} C_i f_i$$

Weighting factor

$$\sum_{i=1}^{N} C_i = 1.0$$

The k_{eff,0} of the target core by generalized bias factor method

$$\widetilde{k}_{eff,r} = k_{eff,r,0} \left(1 + G_k \Delta \sigma \right) \times \sum_{i=1}^{N} C_i \frac{1 + \Delta E_i}{1 + G_{k,i} \Delta \sigma}$$

The variance of the $\widetilde{k}_{eff,0}$

$$Var(\widetilde{k}_{eff,r}^{c}) = \left(G_{k,r} - \sum_{i=1}^{N} C_{i} G_{k,i}\right) V_{x} \left(G_{k,r} - \sum_{i=1}^{N} C_{i} G_{k,i}\right)$$
$$+ \sum_{i=1}^{N} \sum_{j=1}^{N} C_{i} C_{j} Var(\Delta E_{i} \cdot \Delta E_{j})$$

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The uncertainty of the erbia worth is reduced by using the cross section adjustment method

Utilizing the erbia sample worths measured by critical experiment

The adjusted cross section

$$\sigma = \sigma_0 \left\{ 1 + V_{Er} G_{e,\rho}^{t} \left[G_{e,\rho} V_{Er} G_{e,\rho}^{t} + Var(E_{\rho}) \right]^{-1} \frac{\left[\rho_e^e - \rho_e^c(\sigma_0) \right]}{\rho_e^c(\sigma_0)} \right\}$$

 $\sigma_{\scriptscriptstyle 0}\,$: the cross section before adjustment

- $Var(E_{\rho})$: the variance of the measured erbia sample worth
 - $G_{e,\rho}$: the sensitivity coefficient of the erbia sample worth
 - ρ_e^e : the measured erbia sample worth
- $ho_{e}^{c}(\sigma_{0})$: the erbia sample worth calculated by

The covariance of the adjusted cross section

 $V_{Er}' = V_{Er} - V_{Er} G_{e,\rho}^{t} \left[G_{e,\rho} V_{Er} G_{e,\rho}^{t} + Var(E_{\rho}) \right]^{-1} G_{e,\rho} V_{Er}$

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The variance of $\rho_r^c(\sigma)$

$$Var[\rho_r^c(\sigma)] = G_{r,\rho} V_{Er}' G_{r,\rho}^{t}$$

The variance of the effective neutron multiplication factor in the target system

$$Var\left(\widetilde{k}_{eff}\right) = k_{eff}^{2} \left\{ G_{r,\rho} V_{Er} G_{r,\rho}^{t} \rho^{2} + \frac{1}{k_{eff,0}^{2}} \left[\Delta G_{k} V_{\sigma} \Delta G_{k}^{t} + Var(E_{k}) \right] \right\}$$

The uncertainty reduction (UR) is defined by

 $UR = 1 - \frac{Var(\tilde{k}_{eff})}{Var(k_{eff})}$ When UR becomes 1.0, the uncertainties are zero

3. Calculational Model





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Table Calculated erbia sample worth and C/E value of KUCA experiment

Number of erbia plates	Calculated sample Worth (∆k/k)	C/E
3	4.11X10 -4	1.09
5	7.07X10 ⁻⁴	1.13
9	1.27X10 -3	1.11
13	1.44X10 -3	1.12
17	1.67X10 -3	1.10

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Fig. Comparison of sensitivity coefficients for erbia reactivity worth in KUCA

167Er capture cross section is adjusted

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Fig. Alteration rate of 167Er capture cross section due to adjustment

4. Calculation Results

Evaluation of uncertainty reductions
 Blending machine in fuel fabrication process
 PWR core

Method of uncertainty reductionPresent method

Erbia worth : cross section adjustment method

keff : Generalized bias factor method

Two critical experiment data without erbia

Bias factor method

critical experiment data with erbia is directly applied

Without Experiment Data

Case of a blending machine

TableComparison of prediction uncertainties and uncertainty
reduction (UR) for k_{eff} in a blending machine (H/U=0)

	Uncertainty (%)	UR
Present method	0.495	0.604
Bias factor method	0.525	0.555
Case without experimental dat	a 0.787	0.000

$$k_{eff} = 0.6210$$

 $k_{eff,0} = 0.6361$
 $\rho = 3.823X10^{-2} (\Delta k/k)$



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Fig. Sensitivity coefficients of keff with respect to 238U capture cross section Fig. Sensitivity coefficients of keff with respect to 235U fission cross section

Table Comparison of prediction uncertainties and uncertainty reduction (UR) for k_{eff} in a blending machine (H/U=1)

	Uncertainty (%)	UR
Present method	0.414	0.760
Bias factor method	0.539	0.593
Case without experimental da	ta 0.845	0.000

$$k_{eff}$$
 = 0.8026
 $k_{eff,0}$ = 0.8287
 ρ = 3.924X10⁻² (Δ k/k)





Case of a PWR core

Table Comparison of prediction uncertainties and uncertainty reduction (UR) for k_{eff} in a PWR core

	Uncertainty (%)	UR
Present method	0.322	0.865
Bias factor method	0.392	0.801
Case without experimental dat	a 0.879	0.000

$$k_{eff}$$
 = 1.0072
 $k_{eff,0}$ = 1.0479
 ρ = 3.856X10⁻² (Δ k/k)



Fig. Components of prediction uncertainty of keff in a PWR core



Fig. Sensitivity coefficients of keff for a PWR core and KUCA



5. Conclusion

A new method was proposed.

Combining the bias factor method and the cross section adjustment method

The present method was applied to evaluate the prediction uncertainty of neutronics characteristics of the blending machine and the PWR core loading the erbia bearing fuel.

The uncertainty of erbia worth was reduced through the cross section adjustment method using the erbia sample worth measured in KUCA.

Blending machine			
	H/U=0		
	UR = 0.604	by the present method	
	UR = 0.555	by the bias factor method	
	H/U=1		
	UR = 0.760	by the present method	
	UR = 0.593	by the bias factor method	
PWR core			
	UR = 0.865	by the present method	
	UR = 0.801	by the bias factor method	

The uncertainties were reduced by the present method

Thank you for your attention!!

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