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C. Granja¹, J. Kubasta², S. Pospisil¹, S. A. Telezhnikov^{*}

TWO METHODS OF DETERMINATION OF PARITIES OF LOW-LYING STATES IN $^{159}\mathrm{Gd}$ FROM ANALYSIS OF $\gamma\text{-RAY INTENSITIES FROM }^{158}\mathrm{Gd}(n_{\mathrm{res}},\gamma)^{159}\mathrm{Gd}$ REACTION

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¹ Institute of Experimental and Applied Physics, Czech Technical University, Prague

² Faculty of Nuclear Sciences and Physical Engineering, Czech Technical University, Prague

^{*} E-mail: telezhni@nf.jinr.ru

Гранья К. и др. Два метода определения четностей низколежащих состояний в ¹⁵⁹Gd из анализа интенсивностей γ -лучей из реакции ${}^{158}\mathrm{Gd}(n_{\mathrm{res}},\gamma){}^{159}\mathrm{Gd}$

Энергетические уровни и переходы в ¹⁵⁹Gd были изучены с помощью радиационного захвата резонансных нейтронов в 12 изолированных резонансах ¹⁵⁸Gd. Техника времени пролета была использована на обогащенной мишени на реакторе ИБР-30 в ОИЯИ в Дубне. Зарегистрировано 80 первичных переходов и определены их абсолютные интенсивности на уровни $1/2^{\pm}$ и $3/2^{\pm}$ до энергии возбуждения 2,4 МэВ. Четности найденных уровней были пересчитаны с помощью двух методов: первый метод состоит в анализе интенсивностей, усредненных по 12 резонансам, а во втором методе анализируются индивидуальные интенсивности. Второй метод описан впервые.

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Grania C. et al. Two Methods of Determination of Parities of Low-Lying States in ¹⁵⁹Gd from Analysis of γ -Ray Intensities from 158 Gd (n_{res}, γ) 159 Gd Reaction

Energy levels and transitions in ¹⁵⁹Gd were studied by means of radiative capture of resonance neutrons in 12 isolated resonances of ¹⁵⁸Gd. The time-of-flight technique was used on an enriched target at the IBR-30 reactor at JINR. Dubna. A total of 80 primary gamma transitions were recorded, and their absolute intensities were determined resulting in the observation of $1/2^{\pm}$ and $3/2^{\pm}$ levels up to 2.4 MeV. Parities of the found levels were recalculated using two methods: the first method consists in analyzing of intensities averaging in 12 resonances, and in the second method individual intensities are analyzed. The second method is described for the first time.

The investigation has been performed at the Frank Laboratory of Neutron Physics, JINR.

E3-2018-7

E3-2018-7

INTRODUCTION

We extensively studied spectroscopic properties of 159 Gd by resonance neutrons [1,2], by neutrons from neutron filters [3], by thermal neutrons, and from (d, p) and (d, t) reactions. Full information was published in [4].

In [2] together with the other information the determination of parities of low-lying levels of ¹⁵⁹Gd was obtained. Due to big volume of information in that work, description of the method of this determination is very short. In this paper, we give a more detailed description of parity determination procedure. During preparation of this paper we recalculated all data, and there are some differences between results of the previous work ([2], Table 3) and new ones. Analysis of these differences will be done later.

1. EXPERIMENT

Energy levels and transitions in ¹⁵⁹Gd were studied by means of radiative capture of resonance neutrons in 12 isolated resonances of ¹⁵⁸Gd. The time-of-flight technique was used on an enriched target at the IBR-30 reactor at JINR, Dubna. A total of 80 primary gamma transitions were recorded and their absolute intensities were determined. Absolute intensities of 80 transitions in 12 resonances of ¹⁵⁸Gd are presented in [2] (Table 1).

As ¹⁵⁸Gd is an even-even nucleus, all resonances in the measured range of neutron energy have $J^{\pi} = 1/2^+$. Primary γ rays usually are E1 (transitions on the levels with the opposite parity) and M1 (transitions on the levels with the same parities). Levels on which transitions pass have J = 1/2, 3/2 with parity +, if transition is M1, or – if transition is E1. M1 transitions have energy dependence E^3_{γ} , and dependence of E1 transitions is sharper, namely, about E^5_{γ} . It is known that intensities of E1 transitions. From spectroscopic data eight M1transitions and nine E1 transitions are known.

2. TASK OF PARITY DETERMINATION

Using the difference in intensities of E1 and M1 transitions, we formulated quantitative conditions of parity determination of low-lying levels in ¹⁵⁹Gd. Two methods of parity determination were used: the first method consists in analyzing

of intensities averaging in 12 resonances, and in the second method individual intensities are analyzed. The second method is described for the first time.

2.1. The First Method. Eighty intensities averaged in 12 resonances were obtained. Dependence E_{γ}^3 was excluded from these data, and reduced data were normalized on the mean value of reduced intensities of eight known M1 transitions. Here formula of reducing is shown:

$$\xi_{\gamma f} = \frac{\langle I_{\gamma \lambda f} \rangle_{\lambda} / E_{\gamma}^3}{\langle \langle I(M1)_{\gamma \lambda f} \rangle_{\lambda} / E_{\gamma}^3 \rangle_{M1}},\tag{1}$$

where λ is a sign of resonance and f is a sign of the final state.

Values $\xi_{\gamma f}$ of 80 transitions are presented in Fig. 1. There are two curves and a straight line in this figure: curves are dependences of E1 transitions (E_{γ}^5) which normalization was from nine known E1 transitions (upper curve) and from eight known E1 transitions (lower curve). Straight line is a mean of eight known M1 transitions, its y = 1.



Fig. 1. Values $\xi_{\gamma f}$ of 80 γ transitions (points), curves — dependences of E1, and a straight line — dependence of M1; • — known E1, • — known M1, • — unknown parities

As the point about energy 5400 keV (transition 5384.70 keV) is very high, two curves for E1 normalizing are plotted: upper curve with this point and lower curve without one. The meaning of these two curves will be discussed later.

It is clearly seen that intensities of E1 transitions are well-separated from intensities of M1 in the range of 4700–6000 keV. This fact gives an opportunity to separate all intensities into two groups. For this we use statistical properties of intensities. It is known that intensities of transitions from resonances of one type to the levels with certain J^{π} follow the Porter–Thomas (PT) law of distribution [5]. This distribution is from a class of χ^2 distributions, namely, χ^2 distribution with $\nu = 1$. Mean value of intensities from 12 resonances will obey χ^2 distribution with $\nu = 12$. To determine that some transition is E1 we should show that it cannot be from distribution which describes M1 transitions.

We should create statistical distribution which pictures this hypothesis and see how far the point of examined transition is from the center of distribution. As the distribution is normalized on 1, probability to appear accidentally in any piece of this distribution is equal to the area of distribution within this piece. For the events far to the left and far to the right from the center of distribution, probabilities are integrals from the beginning of distribution to this event for events far to the left and from this event to the end of distribution for events far to the right. An example of arbitrary distribution is shown in Fig. 2.



Fig. 2. Arbitrary function f(x) normalized on 1

For deciding if the point of examined transition obeys or not the analyzed distribution, the confidence level must be chosen. In our works we use two confidence levels: 1% and 0.1%. For these two confidence levels critical values must be found. These are values of x integrals to which from the left or from the right are equal to confidence level. When an event falls in the piece p1 with confidence level 0.1%, this hypothesis is abandoned strictly and result of other hypothesis is set without parentheses, and when it falls in the piece p2 with confidence level 1% other hypothesis is set in parentheses. We shall use term "reability" which determines an integral of the distribution from the left to the tested point. This value will be close to 0 if the point is to the left from maximum of the distribution or close to 1 if it is to the right from maximum.

It was said that the mean value of intensities from 12 resonances will obey χ^2 distribution with $\nu = 12$. But apart from this distribution each intensity of transition has its statistical error which obeys the Gaussian distribution. Hence, χ^2 distribution with $\nu = 12$ must be convoluted with the Gaussian with individual parameters.

To find E1 transitions it is needed:

- to normalize all experimental intensities on mean M1 value;
- to obtain χ^2 distribution with $\nu = 12$;

• to make convolution of this distribution with the Gaussian which is individual for each point;

• to find critical values for two confidence levels;

• to find value reability which will be integral from the left, this value will be close to 1 as E1 transitions are greater than M1;

• to compare this value with two critical values.

To find M1 transitions, we should compare intensities with χ^2 distribution which is normalized on the mean of E1 transitions. For this dependence of E1transitions must be eliminated. In [2] two dependences of E1 transitions were discussed: Lorentzian and Markushev–Furman model. But in this work we use a simple dependence E_{γ}^5 because it is sharper than others and this gives more reliable results in the energy range from 3.5 to 4.5 MeV as E_{γ}^5 curve is nearer to M1 points.

Now we must discuss the two curves in Fig. 1. The upper curve is obtained using point 5384.70 keV. During analysis of points with normalizing on E1 with the lower curve this point was very big and it was determined as a doublet. Further, the doublets will be marked as D or (D). In view of this the upper curve was not used and all calculations were performed with the lower curve. Using the described method the points which are lower than critical values can be determined as M1 or (M1) and points higher than critical values with integrals near 1 can be determined as D or (D).

2.2. The Second Method. This method consists in analysis of absolute intensities of each transition from resonances to each level. As there are 12 resonances, we have 12 distributions for each level. Statistical distribution of these values is PT distribution. This distribution must be convoluted with the Gaussian from the statistical error of transition intensity. In this way 12 values of reability can be obtained. These values must be analyzed. They represent 12 points on [0, 1] cut. Now we try to obtain quantitative conditions to refuse the hypothesis that 12 transitions on one level belong to obtained distributions.

Divide [0,1] cut into two pieces p and q. We know that p is a small part of [0,1] cut:

$$p+q=1.$$

From 12 resonances we have 12 independent probabilities, and the whole probability is

$$(p+q)^{12} = 1.$$

It is Newton's binomial. Open the parentheses:

$$p^{12} + 12p^{11}q + 66p^{10}q^2 + 220p^9q^3 + 495p^8q^4 + 792p^7q^5 + 924p^6q^6 + + 792p^5q^7 + 495p^4q^8 + 220p^3q^9 + 66p^2q^{10} + 12pq^{11} + q^{12} = 1.$$

Now analyze some member of this expression, for instance, the fourth. This member is the probability that 9 points fall to part p. If we solve the equation $220p^9q^3 = 0.001$ or $220p^9q^3 = 0.01$ we can obtain critical values which show that probability to have 9 points in piece p is 0.1% or 1%, respectively.

In this way we can obtain all 12 pairs of critical values for all members with p of this expression. Now for all 80 transitions it is needed to do convolutions of one function of PT with the individual Gaussians from experimental errors and to find a set of 12 reability values. These data can be compared with critical values.

3. CALCULATIONS

We should

 \bullet obtain the Gaussian, χ^2 distribution with $\nu=1,~\chi^2$ distribution with $\nu=12;$

 \bullet make convolution of χ^2 distributions with Gaussians which are individual for each intensity;

• find critical values for two confidence levels for χ^2 distribution with $\nu = 12$;

- find reability values for $\nu = 12$;
- calculate critical values for 12 pairs of confidence levels for $\nu = 1$;

• analyze all data and obtain parities by two methods.

Figure 2 shows that bounds of p pieces are set far from maxima of distributions and integrating must be to the area with small values of functions.

For better precision all calculations were made in Fortran codes with variables REAL*16. Calculations with such variables give precision of results with about 33 right signs.

For the convolution all curves were replaced by piecewise continuous polynomials of the third power through each 4 points of x coordinates with different steps which were determined as gave high precision of replacing. Precision of replacing was tested by integrating of curves and comparing of integrals with 1. In Table 1 parameters of fit of some functions by polynomials are shown. It is seen that precision depends on the number of points x.

Table 1. Parameters of polynomials for four functions: N — number of points x, area — integral, NR — number of right signs in integrals

Function	N	Area	NR
Gaussian	2031	0.9999999999897369E+00	9
χ^2 with $\nu = 1$	1463	0.9999999991390689E+00	8
χ^2 with $\nu = 2$	5594	0.99999999999999126E+00	12
χ^2 with $\nu = 12$	1950	0.9999999998204125E+00	8

Function χ^2 with $\nu = 2$ is very simple: $\exp(-x)$. It was not used and is given as an example. The most computer time is spent on convolutions. In [2] these calculations were provided in old systems UNIX or SANOS and time of calculations was limited. For this reason calculations were performed with smaller precision of convolutions: namely, 5 or 6 signs. Now calculations were made on modern desktop computer, and 8 signs of precision were achieved. This is a source of differences between old and new results which will be discussed later. The most time was spent on method 2 as there must be 12 convolutions for each of 80 levels.

Borders of reability for four confidence levels were calculated and are shown in Table 2. These borders were tested by Monte Carlo simulation. In Monte Carlo simulations 12 random numbers were generated, and events which fall to pieces with borders from Table 2 were added in four counters. Results are shown in Table 3.

Led No.	20%	10%	1%	0.1%
1	0.97893530	0.99077201	0.99915892	0.99991661
2	0.91343027	0.94958514	0.98684847	0.99602932
3	0.83148438	0.89147431	0.95961344	0.98253584
4	0.74358207	0.82471770	0.92095554	0.95900744
5	0.65528965	0.75295264	0.87335509	0.92642683
6	0.57046992	0.67804360	0.81823516	0.88558257
7	0.49108195	0.60097700	0.75631922	0.83685452
8	0.41670281	0.52218020	0.68779033	0.78017426
9	0.34546533	0.44160458	0.61227202	0.71491122
10	0.27519742	0.35861242	0.52855957	0.63952595
11	0.20343767	0.27143469	0.43368423	0.55049646
12	0.12551473	0.17459582	0.31870794	0.43765867

Table 2. Borders of reability for four confidence levels (Led) at the end of the cut $\left[0,1\right]$

Led No.	20%	10%	1%	0.1%
1	199988356	99997723	9999206	1000541
2	200003147	99993970	10001449	1001716
3	199990133	100008878	9997067	1000800
4	199982567	100009826	9999704	999397
5	199995607	100006117	9996229	1001007
6	199991386	100020255	10002878	1001937
7	200022638	100009744	9999832	1002330
8	200021065	100013733	9995901	1001405
9	200017754	100004531	10001494	1000768
10	200010661	99996432	10001575	1000500
11	200009661	100005569	9998226	1000163
12	200001707	100005309	10003698	1000244

 Table 3. Monte Carlo test of four borders of confidence levels (Led). One billion of

 12 random numbers was generated

4. RESULTS AND DISCUSSION

Results of the determination of parities are given in Table 4. It is similar to Table 3 in [2]. However, whereas in the second column of Table 3 in [2] f_{γ} are listed, here in column 3 values $\xi_{\gamma f}$ from expression (1) are led. Additionally, in that Table there was column "resonance", and here column "group" is given, where the numbers of points on [0, 1] cut, for which appropriate confidence level was performed, are listed. The more groups we have, the more reliable the results.

Table 4. Final assignments of transition multipolarity XL are based on the analysis of analytically averaged (a) and of individual (b) γ -ray intensities. All observed levels have either spin 1/2 or 3/2 with parity as indicated. Assignments are made within 0.1% significance level (assignments within 1% are indicated in parentheses)

E_{γ} ,	ΔE_{γ} ,	¢,	Λ٤.	$Group^a$	Mu	ltipolarit	y^b	E_f ,	j^{π}
keV	keV	$\varsigma \gamma f$	$\Delta \zeta \gamma f$	Group	XL(a)	XL(b)	XL	keV	$\frac{1}{2}^{\pi}, \frac{3}{2}^{\pi}$
5943.0	0.2	10.4	0.3	1 2 3 4 5 6 7 8 9	E1	E1	E1	0.0	-
				10 11					
5434.7	0.2	6.6	0.3	1 2 3 4 9 10 11 12	E1	E1	E1	508.3	-
5384.7	0.2	17.7	0.6	2	D	D	D	558.3	-
5341.1	0.3	0.4	0.3	9 10 11 12	M1	M1	M1	601.9	+
5295.9	0.5	0.6	0.3	11 12	M1	M1	M1	647.1	+
5198.1	0.2	0.7	0.3	10 11 12	M1	M1	M1	744.9	+
5161.0	0.5	1.6	0.3	11		M1	M1	782.0	+

Table 4 (continued)

E_{γ} ,	ΔE_{γ} ,	¢.	Δ¢	Group ^a	Mu	ltipolarit	y ^b	E_f ,	j^{π}
keV	keV	$\varsigma \gamma f$	$\Delta \zeta \gamma f$	Group	XL(a)	XL(b)	XL	keV	$\frac{1}{2}^{\pi}, \frac{3}{2}^{\pi}$
5083.0	0.6	1.1	0.3	11	(M1)	M1	M1	860.0	+
4971.0	1.3	1.1	0.5	11	(M1)	M1	M1	972.0	+
4939.7	1.0	1.5	0.4	12		(M1)	(M1)	1003.3	(+)
4881.7	0.3	7.1	0.5	1 2 3 4 5 6 10	E1	E1	E1	1061.3	-
4863.5	0.2	5.8	0.4	1 2 3 4 5 6 7	E1	E1	E1	1079.5	-
4832.2	0.3	3.9	0.5	3	E1	E1	E1	1110.8	-
4814.4	0.3	1.0	0.4	2 10	(M1)	(M1)	(M1)	1128.6	(+)
4803.3	0.2	4.0	0.5	3 4 5 6	E1	E1	E1	1139.7	-
4796.9	0.2	3.5	0.5	2345	E1	E1	E1	1146.1	-
4543.7	1.1	3.7	0.6	789	E1	E1	E1	1399.3	-
4526.1	1.3	0.5	0.6	11	(M1)	M1	M1	1416.9	+
4513.4	1.2	2.0	0.6					1429.6	
4495.2	1.3	-0.6	0.6	3 5 12	M1	M1	M1	1447.8	+
4474.4	1.2	1.3	0.6					1468.6	
4464.7	0.3	2.1	0.6	5		(E1)	(E1)	1478.3	(-)
4438.6	0.8	1.7	0.6	10		(M1)	(M1)	1504.4	(+)
4421.7	0.5	5.3	0.7	145678	E1	E1	E1	1521.3	_
4385.9	1.0	-0.1	0.8	10	(M1)	M1	M1	1557.1	+
4381.7	0.5	4.0	0.8	1678911	E1	(E1)	E1	1561.3	_
4366.0	1.4	2.1	0.8					1577.0	
4360.7	0.9	2.8	0.8	591011		(E1)	(E1)	1582.3	(-)
4348.4	1.5	0.9	0.8	10 11 12		(M1)	(M1)	1594.6	(+)
4340.4	1.5	3.3	1.4			. ,		1602.6	
4327.9	0.6	-0.5	0.8	6 7 9 10 11 12	M1	(M1)	M1	1615.1	+
4308.0	1.0	0.2	0.8	9 10 11	(M1)	(M1)	(M1)	1635.0	(+)
4301.4	0.8	3.3	0.8	9	(E1)	E1	E1	1641.6	_
4273.2	1.5	0.9	0.9	10		(M1)	(M1)	1669.8	(+)
4268.8	0.8	2.4	0.9			. ,		1674.2	
4238.4	1.0	1.4	0.8					1704.6	
4197.0	1.0	1.4	0.9					1746.0	
4172.7	0.9	2.1	0.9					1770.3	
4118.5	0.4	7.6	1.0	10	E1	D	D	1824.5	_
4102.1	1.5	3.8	1.0	10	(E1)	E1	E1	1840.9	_
4074.5	0.3	2.9	1.0					1868.5	
4062.3	1.0	3.4	1.2					1880.7	
4057.7	1.5	4.1	1.3					1885.3	
4053.5	2.0	-1.2	1.2	5 9 10 11 12	(M1)	(M1)	(M1)	1889.5	(+)
4046.2	3.0	-0.2	1.0		(M1)	((M1)	1896.8	(+)
4024.5	1.0	2.1	1.1		((1918.5	(.)
4017.0	0.9	-0.5	1.1		(M1)		(M1)	1926.0	(+)
3997.6	0.8	5.7	1.2	23456789	E1	E1	E1	1945.4	_

Table 4 (continued)

E_{γ} ,	ΔE_{γ} ,	¢.	Δċ	Group ^a	Mu	ltipolarit	y ^b	E_f ,	j^{π}
keV	keV	$\varsigma \gamma f$	$\Delta \zeta \gamma f$	Group	XL(a)	XL(b)	XL	keV	$\frac{1}{2}^{\pi}, \frac{3}{2}^{\pi}$
3988.6	0.5	0.6	1.2					1954.4	
3970.9	0.3	3.9	1.3	12		(E1)	(E1)	1972.1	(-)
3961.4	1.0	0.7	1.3	12		(M1)	(M1)	1981.6	(+)
3934.9	2.5	2.8	1.4					2008.1	
3911.3	1.7	3.0	1.3	26		(E1)	(E1)	2031.7	(-)
3904.7	1.7	5.5	1.3	3 4 5 6 8	E1	E1	E1	2038.3	_
3890.0	2.5	3.6	1.3	456		E1	E1	2053.0	-
3870.4	0.4	6.9	1.4	12	E1	(D)	(D)	2072.6	-
3856.8	1.7	3.3	1.4	1		(E1)	(E1)	2086.2	(-)
3831.6	0.7	3.2	1.5	6		(E1)	(E1)	2111.4	(-)
3821.1	1.7	3.6	1.5	9 10		(E1)	(E1)	2121.9	(-)
3808.7	1.7	4.7	1.5	56		(E1)	(E1)	2134.3	(-)
3789.6	1.0	3.5	1.5					2153.4	
3780.4	1.0	5.8	1.6	12	(E1)	(D)	(D)	2162.6	-
3764.3	1.0	5.1	1.5	2345	(E1)	E1	E1	2178.7	-
3758.0	1.0	5.6	1.6	2 7 9 10 11 12	(E1)	(<i>E</i> 1)	(E1)	2185.0	(-)
3752.2	1.4	4.0	1.6	3 7		(<i>E</i> 1)	(E1)	2190.8	(-)
3742.2	1.0	4.1	1.6	8		(E1)	(E1)	2200.8	(-)
3736.4	1.6	4.0	1.7					2206.6	
3720.6	0.8	5.3	1.7	11	(E1)	(D)	(D)	2222.4	-
3709.0	1.0	4.8	1.7	11		(<i>E</i> 1)	(E1)	2234.0	(-)
3686.9	1.0	5.4	2.0					2256.1	
3683.2	0.8	2.0	2.0					2259.8	
3662.1	0.7	6.6	2.0	89	(E1)	(D)	(D)	2280.9	-
3655.0	1.0	4.5	1.9	7		(D)	(D)	2288.0	-
3628.7	0.7	8.6	3.7	12		(D)	(D)	2314.3	-
3607.6	0.8	0.2	2.1					2335.4	
3596.0	0.5	3.5	2.2	1		(<i>E</i> 1)	(E1)	2347.0	(-)
3591.7	1.7	2.7	2.1	1		E1	E1	2351.3	-
3585.2	0.5	4.0	2.2	1		(E1)	(E1)	2357.8	(-)
3565.4	0.8	-2.5	2.1	7		(<i>M</i> 1)	(M1)	2377.6	(+)
3554.4	0.8	5.5	2.2	1 2 3 4		(E1)	(E1)	2388.6	(-)
^a Numb	er of po	oints o	n [0, 1]	cut for which appro	opriate co	onfidence	e level y	was perf	ormed.
^b Transi	tions w	ith un	usuallv	strong intensities a	re labelle	ed by D	to ind	icate the	possi-
bility of	f a doul	olet or	of a n	onstatistically large	fluctuatio	on.			1

Now results which are worse than in [2] will be listed. Although for transition 4474.4 keV in [2] was parity (+), now parity is not determined. For transitions 4348.4, 4308.0, and 4053.5 keV results from + became (+).

For some transitions now results are better: for 4381.7 and 3720.6 keV results are changed from (–) to – without parentheses. In Table 3 in [2] there are 3 columns with the determination of XL. For 5384.7 keV in these columns there are E1 determinations. Now all three values of XL of 5384.7 keV transition are changed from E1 to D. This indicates probability of nonstatistical big intensity of this transition. For transitions 3780.4, 3720.6, 3662.1, and 3655.0 keV values of XL became (D).

These results demonstrate importance of precision of calculations for more reliable determination of parities.

Now analysis of differences in parity determination by two methods will be obtained. Schematic comparison of the results is shown in Fig. 3.



Fig. 3. Schematical view of the differences of results of parity determination by two methods

One can see that for 19 transitions parities were not determined. For 20 transitions determinations by two methods coincide. For 25 transitions determinations are obtained only by the second method, and for two transitions determination by the second method is more precise. For two transitions determination is obtained only by the first method, and for two transitions this method gave more precise result. This demonstrates that method 2 is a harder criterion than method 1.

There are many D and (D) determinations for transitions in the region 3500–4500 keV. This can demonstrate that E_{γ}^5 is very sharp, and the Lorentzian or Markushev–Furman model may be more real.

SUPPLEMENT

As we have a software toolkit to calculate integrals of some functions, we prepared several tables. We hope that these data will have a wider set of arguments and more precise values than those received from the Internet.

x	$\Phi(x)$	x	$\Phi(x)$
1.00	1.5865525E-01	8.00	6.2209606E-16
2.00	2.2750132E-02	9.00	1.1285884E-19
3.00	1.3498980E-03	10.00	7.6198530E-24
4.00	3.1671242E-05	11.00	1.9106596E-28
5.00	2.8665157E-07	12.00	1.7764821E-33
6.00	9.8658764E-10	13.00	6.1171566E-39
7.00	1.2798125E-12		

Table S1. Values of $\Phi(x) = \frac{1}{\sqrt{2\pi}} \int_{x}^{\infty} \exp(-\frac{z^2}{2}) dz$ for integer values of argument

Table S2. Reverse values for $\Phi(x) = \frac{1}{\sqrt{2\pi}} \int_{x}^{\infty} \exp\left(-\frac{z^2}{2}\right) dz$ for values of 10^{-n} of $\Phi(x)$

$\Phi(x)$	x	$\Phi(x)$	x
1.0E-01	1.2815516E+00	1.0E-14	7.6506281E+00
1.0E-02	2.3263479E+00	1.0E-15	7.9413453E+00
1.0E-03	3.0902323E+00	1.0E-16	8.2220822E+00
1.0E-04	3.7190165E+00	1.0E-17	8.4937932E+00
1.0E-05	4.2648908E+00	1.0E-18	8.7572903E+00
1.0E-06	4.7534243E+00	1.0E-19	9.0132712E+00
1.0E-07	5.1993376E+00	1.0E-20	9.2623401E+00
1.0E-08	5.6120012E+00	1.0E-21	9.5050250E+00
1.0E-09	5.9978070E+00	1.0E-22	9.7417899E+00
1.0E-10	6.3613409E+00	1.0E-23	9.9730456E+00
1.0E-11	6.7060232E+00	1.0E-24	1.0199157E+01
1.0E-12	7.0344838E+00	1.0E-25	1.0420452E+01
1.0E-13	7.3487961E+00	1.0E-26	1.0637224E+01

Table S3. Values of $\Phi(x) = \frac{1}{\sqrt{2\pi}} \int_{x}^{\infty} \exp{(-\frac{z^2}{2})} dz$ for steps of x: $\Delta x = 0.01$

x	00	01	02	03	04
0.00	5.000000E-01	4.9601064E-01	4.9202169E-01	4.8803353E-01	4.8404656E-01
0.10	4.6017216E-01	4.5620469E-01	4.5224157E-01	4.4828321E-01	4.4433000E-01
0.20	4.2074029E-01	4.1683384E-01	4.1293558E-01	4.0904588E-01	4.0516513E-01
0.30	3.8208858E-01	3.7828048E-01	3.7448417E-01	3.7069998E-01	3.6692826E-01
0.40	3.4457826E-01	3.4090297E-01	3.3724273E-01	3.3359782E-01	3.2996855E-01
0.50	3.0853754E-01	3.0502573E-01	3.0153179E-01	2.9805597E-01	2.9459852E-01
0.60	2.7425312E-01	2.7093090E-01	2.6762889E-01	2.6434729E-01	2.6108630E-01
0.70	2.4196365E-01	2.3885207E-01	2.3576250E-01	2.3269509E-01	2.2965000E-01
0.80	2.1185540E-01	2.0897009E-01	2.0610805E-01	2.0326939E-01	2.0045419E-01
0.90	1.8406013E-01	1.8141125E-01	1.7878638E-01	1.7618554E-01	1.7360878E-01
1.00	1.5865525E-01	1.5624765E-01	1.5386423E-01	1.5150500E-01	1.4916995E-01
1.10	1.3566606E-01	1.3349951E-01	1.3135688E-01	1.2923811E-01	1.2714315E-01
1.20	1.1506967E-01	1.1313945E-01	1.1123244E-01	1.0934855E-01	1.0748770E-01
1.30	9.6800485E-02	9.5097918E-02	9.3417509E-02	9.1759136E-02	9.0122672E-02
1.40	8.0756659E-02	7.9269841E-02	7.7803841E-02	7.6358510E-02	7.4933700E-02
1.50	6.6807201E-02	6.5521712E-02	6.4255488E-02	6.3008364E-02	6.1780177E-02
1.60	5.4799292E-02	5.3698928E-02	5.2616138E-02	5.1550748E-02	5.0502583E-02
1.70	4.4565463E-02	4.3632937E-02	4.2716221E-02	4.1815138E-02	4.0929509E-02
1.80	3.5930319E-02	3.5147894E-02	3.4379502E-02	3.3624969E-02	3.2884119E-02
1.90	2.8716560E-02	2.8066607E-02	2.7428950E-02	2.6803419E-02	2.6189845E-02
2.00	2.2750132E-02	2.2215594E-02	2.1691694E-02	2.1178270E-02	2.0675163E-02
2.10	1.7864421E-02	1.7429178E-02	1.7003023E-02	1.6585807E-02	1.6177383E-02
2.20	1.3903448E-02	1.3552581E-02	1.3209384E-02	1.2873721E-02	1.2545461E-02
2.30	1.0724110E-02	1.0444077E-02	1.0170439E-02	9.9030756E-03	9.6418699E-03
2.40	8.1975359E-03	7.9762603E-03	7.7602536E-03	7.5494114E-03	7.3436310E-03
2.50	6.2096653E-03	6.0365581E-03	5.8677417E-03	5.7031263E-03	5.5426234E-03
2.60	4.6611880E-03	4.5271111E-03	4.3964883E-03	4.2692434E-03	4.1453014E-03
2.70	3.4669738E-03	3.3641604E-03	3.2640958E-03	3.1667163E-03	3.0719592E-03
2.80	2.5551303E-03	2.4770750E-03	2.4011825E-03	2.3274002E-03	2.2556767E-03
2.90	1.8658133E-03	1.8071438E-03	1.7501569E-03	1.6948100E-03	1.6410612E-03
3.00	1.3498980E-03	1.3062384E-03	1.2638734E-03	1.2227687E-03	1.1828907E-03
3.10	9.6760321E-04	9.3543672E-04	9.0425520E-04	8.7403152E-04	8.4473917E-04
3.20	6.8713794E-04	6.6367486E-04	6.4095298E-04	6.1895109E-04	5.9764850E-04
3.30	4.8342414E-04	4.6647986E-04	4.5008724E-04	4.3422992E-04	4.1889195E-04
3.40	3.3692927E-04	3.2481440E-04	3.1310568E-04	3.0179062E-04	2.9085709E-04
3.50	2.3262908E-04	2.2405335E-04	2.1577340E-04	2.0777983E-04	2.0006352E-04
3.60	1.5910859E-04	1.5309850E-04	1.4730151E-04	1.4171061E-04	1.3631902E-04
3.70	1.0779973E-04	1.0362962E-04	9.9611389E-05	9.5739885E-05	9.2010127E-05
3.80	7.2348044E-05	6.9483396E-05	6.6725837E-05	6.4071629E-05	6.1517155E-05
3.90	4.8096344E-05	4.6148061E-05	4.4274484E-05	4.2472931E-05	4.0740805E-05
4.00	3.1671242E-05	3.0359374E-05	2.9099071E-05	2.7888426E-05	2.6725601E-05
4.10	2.0657507E-05	1.9782956E-05	1.8943620E-05	1.8138162E-05	1.7365291E-05
4.20	1.3345749E-05	1.2768534E-05	1.2215116E-05	1.1684566E-05	1.1175989E-05
4.30	8.5399055E-06	8.1627273E-06	7.8014600E-06	7.4554671E-06	7.1241358E-06
4.40	5.4125439E-06	5.1685310E-06	4.9350451E-06	4.7116544E-06	4.4979439E-06

Table S3 (continued)

x	05	06	07	08	09
0.00	4.8006119E-01	4.7607782E-01	4.7209683E-01	4.6811863E-01	4.6414361E-01
0.10	4.4038231E-01	4.3644054E-01	4.3250507E-01	4.2857628E-01	4.2465457E-01
0.20	4.0129367E-01	3.9743189E-01	3.9358013E-01	3.8973875E-01	3.8590812E-01
0.30	3.6316935E-01	3.5942357E-01	3.5569125E-01	3.5197271E-01	3.4826827E-01
0.40	3.2635522E-01	3.2275811E-01	3.1917751E-01	3.1561370E-01	3.1206695E-01
0.50	2.9115969E-01	2.8773972E-01	2.8433885E-01	2.8095731E-01	2.7759532E-01
0.60	2.5784611E-01	2.5462691E-01	2.5142890E-01	2.4825223E-01	2.4509709E-01
0.70	2.2662735E-01	2.2362729E-01	2.2064995E-01	2.1769544E-01	2.1476388E-01
0.80	1.9766254E-01	1.9489452E-01	1.9215020E-01	1.8942965E-01	1.8673294E-01
0.90	1.7105613E-01	1.6852761E-01	1.6602325E-01	1.6354306E-01	1.6108706E-01
1.00	1.4685906E-01	1.4457230E-01	1.4230965E-01	1.4007109E-01	1.3785657E-01
1.10	1.2507194E-01	1.2302440E-01	1.2100048E-01	1.1900011E-01	1.1702320E-01
1.20	1.0564977E-01	1.0383468E-01	1.0204232E-01	1.0027257E-01	9.8525329E-02
1.30	8.8507991E-02	8.6914962E-02	8.5343451E-02	8.3793322E-02	8.2264439E-02
1.40	7.3529260E-02	7.2145037E-02	7.0780877E-02	6.9436623E-02	6.8112118E-02
1.50	6.0570758E-02	5.9379941E-02	5.8207556E-02	5.7053433E-02	5.5917403E-02
1.60	4.9471468E-02	4.8457226E-02	4.7459682E-02	4.6478658E-02	4.5513977E-02
1.70	4.0059157E-02	3.9203903E-02	3.8363570E-02	3.7537980E-02	3.6726956E-02
1.80	3.2156775E-02	3.1442763E-02	3.0741909E-02	3.0054039E-02	2.9378980E-02
1.90	2.5588060E-02	2.4997895E-02	2.4419185E-02	2.3851764E-02	2.3295468E-02
2.00	2.0182215E-02	1.9699270E-02	1.9226172E-02	1.8762766E-02	1.8308900E-02
2.10	1.5777607E-02	1.5386335E-02	1.5003423E-02	1.4628731E-02	1.4262118E-02
2.20	1.2224473E-02	1.1910625E-02	1.1603792E-02	1.1303844E-02	1.1010658E-02
2.30	9.3867055E-03	9.1374675E-03	8.8940426E-03	8.6563190E-03	8.4241864E-03
2.40	7.1428107E-03	6.9468508E-03	6.7556526E-03	6.5691191E-03	6.3871548E-03
2.50	5.3861460E-03	5.2336082E-03	5.0849257E-03	4.9400158E-03	4.7987966E-03
2.60	4.0245885E-03	3.9070326E-03	3.7925623E-03	3.6811080E-03	3.5726010E-03
2.70	2.9797632E-03	2.8900681E-03	2.8028146E-03	2.7179449E-03	2.6354021E-03
2.80	2.1859615E-03	2.1182050E-03	2.0523590E-03	1.9883759E-03	1.9262091E-03
2.90	1.5888696E-03	1.5381952E-03	1.4889987E-03	1.4412419E-03	1.3948872E-03
3.00	1.1442068E-03	1.1066850E-03	1.0702939E-03	1.0350030E-03	1.0007825E-03
3.10	8.1635231E-04	7.8884569E-04	7.6219469E-04	7.3637526E-04	7.1136397E-04
3.20	5.7702504E-04	5.5706107E-04	5.3773742E-04	5.1903543E-04	5.0093691E-04
3.30	4.0405780E-04	3.8971236E-04	3.7584092E-04	3.6242915E-04	3.4946312E-04
3.40	2.8029328E-04	2.7008769E-04	2.6022918E-04	2.5070689E-04	2.4151027E-04
3.50	1.9261558E-04	1.8542740E-04	1.7849061E-04	1.7179710E-04	1.6533898E-04
3.60	1.3112015E-04	1.2610762E-04	1.2127523E-04	1.1661698E-04	1.1212703E-04
3.70	8.8417285E-05	8.4956678E-05	8.1623774E-05	7.8414179E-05	7.5323642E-05
3.80	5.9058912E-05	5.6693513E-05	5.4417677E-05	5.2228232E-05	5.0122111E-05
3.90	3.9075597E-05	3.7474882E-05	3.5936316E-05	3.4457634E-05	3.3036648E-05
4.00	2.5608816E-05	2.4536358E-05	2.3506569E-05	2.2517850E-05	2.1568659E-05
4.10	1.6623764E-05	1.5912380E-05	1.5229982E-05	1.4575455E-05	1.3947723E-05
4.20	1.0688526E-05	1.0221345E-05	9.7736484E-06	9.3446657E-06	8.9336559E-06
4.30	6.8068766E-06	6.5031222E-06	6.2123268E-06	5.9339654E-06	5.6675330E-06
4.40	4.2935145E-06	4.0979826E-06	3.9109799E-06	3.7321520E-06	3.5611587E-06

Table S3 (continued)

x	00	01	02	03	04
4.50	3.3976731E-06	3.2413813E-06	3.0919816E-06	2.9491843E-06	2.8127114E-06
4.60	2.1124547E-06	2.0133449E-06	1.9187002E-06	1.8283287E-06	1.7420459E-06
4.70	1.3008075E-06	1.2385840E-06	1.1792232E-06	1.1225992E-06	1.0685911E-06
4.80	7.9332815E-07	7.5465148E-07	7.1779111E-07	6.8266525E-07	6.4919564E-07
4.90	4.7918328E-07	4.5538196E-07	4.3272106E-07	4.1114808E-07	3.9061285E-07
5.00	2.8665157E-07	2.7215018E-07	2.5835740E-07	2.4523992E-07	2.3276592E-07
5.10	1.6982674E-07	1.6107941E-07	1.5276783E-07	1.4487109E-07	1.3736923E-07
5.20	9.9644263E-08	9.4420316E-08	8.9461565E-08	8.4755020E-08	8.0288299E-08
5.30	5.7901340E-08	5.4812617E-08	5.1883626E-08	4.9106383E-08	4.6473291E-08
5.40	3.3320448E-08	3.1512375E-08	2.9799518E-08	2.8177026E-08	2.6640286E-08
5.50	1.8989562E-08	1.7941685E-08	1.6949983E-08	1.6011539E-08	1.5123582E-08
5.60	1.0717590E-08	1.0116331E-08	9.5478729E-09	9.0104811E-09	8.5025082E-09
5.70	5.9903714E-09	5.6488087E-09	5.3262027E-09	5.0215317E-09	4.7338276E-09
5.80	3.3157460E-09	3.1236421E-09	2.9423814E-09	2.7713688E-09	2.6100411E-09
5.90	1.8175079E-09	1.7105387E-09	1.6097081E-09	1.5146734E-09	1.4251104E-09
6.00	9.8658764E-10	9.2761663E-10	8.7208535E-10	8.1979840E-10	7.7057114E-10
6.10	5.3034233E-10	4.9815570E-10	4.6787679E-10	4.3939536E-10	4.1260740E-10
6.20	2.8231580E-10	2.6492301E-10	2.4857744E-10	2.3321759E-10	2.1878545E-10
6.30	1.4882282E-10	1.3951773E-10	1.3078165E-10	1.2258060E-10	1.1488258E-10
6.40	7.7688476E-11	7.2759818E-11	6.8137173E-11	6.3801973E-11	5.9736751E-11
6.50	4.0160006E-11	3.7575403E-11	3.5153696E-11	3.2884846E-11	3.0759417E-11
6.60	2.0557889E-11	1.9216001E-11	1.7959943E-11	1.6784344E-11	1.5684158E-11
6.70	1.0420977E-11	9.7312207E-12	9.0862281E-12	8.4831544E-12	7.9193316E-12
6.80	5.2309575E-12	4.8799373E-12	4.5520255E-12	4.2457316E-12	3.9596590E-12
6.90	2.6001270E-12	2.4232685E-12	2.2582182E-12	2.1042031E-12	1.9604997E-12
7.00	1.2798125E-12	1.1915906E-12	1.1093412E-12	1.0326677E-12	9.6119916E-13
7.10	6.2378445E-13	5.8021477E-13	5.3963532E-13	5.0184464E-13	4.6665460E-13
7.20	3.0106280E-13	2.7975938E-13	2.5993787E-13	2.4149702E-13	2.2434237E-13
7.30	1.4388386E-13	1.3357119E-13	1.2398548E-13	1.1507637E-13	1.0679693E-13
7.40	6.8092249E-14	6.3149708E-14	5.8560167E-14	5.4298840E-14	5.0342650E-14
7.50	3.1908917E-14	2.9563682E-14	2.7388121E-14	2.5370161E-14	2.3498573E-14
7.60	1.4806537E-14	1.3704796E-14	1.2683786E-14	1.1737686E-14	1.0861087E-14
7.70	6.8033115E-15	6.2908869E-15	5.8164853E-15	5.3773292E-15	4.9708407E-15
7.80	3.0953588E-15	2.8593993E-15	2.6411668E-15	2.4393498E-15	2.2527322E-15
7.90	1.3945171E-15	1.2869445E-15	1.1875529E-15	1.0957294E-15	1.0109063E-15
8.00	6.2209606E-16	5.7354222E-16	5.2872583E-16	4.8736333E-16	4.4919236E-16
8.10	2.7479594E-16	2.5309881E-16	2.3309184E-16	2.1464522E-16	1.9763895E-16
8.20	1.2019352E-16	1.1059425E-16	1.0175159E-16	9.3606722E-17	8.6105328E-17
8.30	5.2055697E-17	4.7851036E-17	4.3981656E-17	4.0421177E-17	3.7145267E-17
8.40	2.2323932E-17	2.0500536E-17	1.8824215E-17	1.7283261E-17	1.5866883E-17
8.50	9.4795348E-18	8.6966677E-18	7.9776661E-18	7.3173858E-18	6.7110918E-18
8.60	3.9858050E-18	3.6530288E-18	3.3477056E-18	3.0675987E-18	2.8106511E-18
8.70	1.6594209E-18	1.5193740E-18	1.3910090E-18	1.2733631E-18	1.1655521E-18
8.80	6.8408077E-19	6.2572930E-19	5.7229861E-19	5.2337862E-19	4.7859301E-19
8.90	2.7923344E-19	2.5516282E-19	2.3314411E-19	2.1300440E-19	1.9458519E-19

Table S3 (continued)

x	05	06	07	08	09
4.50	2.6822958E-06	2.5576810E-06	2.4386211E-06	2.3248796E-06	2.2162300E-06
4.60	1.6596751E-06	1.5810469E-06	1.5059987E-06	1.4343746E-06	1.3660252E-06
4.70	1.0170832E-06	9.6796480E-07	9.2112960E-07	8.7647597E-07	8.3390657E-07
4.80	6.1730737E-07	5.8692876E-07	5.5799124E-07	5.3042920E-07	5.0417989E-07
4.90	3.7106741E-07	3.5246590E-07	3.3476451E-07	3.1792137E-07	3.0189646E-07
5.00	2.2090503E-07	2.0962824E-07	1.9890785E-07	1.8871743E-07	1.7903176E-07
5.10	1.3024323E-07	1.2347492E-07	1.1704700E-07	1.1094295E-07	1.0514704E-07
5.20	7.6049605E-08	7.2027701E-08	6.8211879E-08	6.4591943E-08	6.1158180E-08
5.30	4.3977116E-08	4.1610976E-08	3.9368321E-08	3.7242919E-08	3.5228842E-08
5.40	2.5184910E-08	2.3806729E-08	2.2501779E-08	2.1266292E-08	2.0096687E-08
5.50	1.4283480E-08	1.3488733E-08	1.2736967E-08	1.2025929E-08	1.1353481E-08
5.60	8.0223919E-09	7.5686498E-09	7.1398760E-09	6.7347371E-09	6.3519686E-09
5.70	4.4621725E-09	4.2056968E-09	3.9635766E-09	3.7350313E-09	3.5193212E-09
5.80	2.4578651E-09	2.3143359E-09	2.1789757E-09	2.0513324E-09	1.9309781E-09
5.90	1.3407124E-09	1.2611897E-09	1.1862679E-09	1.1156881E-09	1.0492052E-09
6.00	7.2422917E-10	6.8060774E-10	6.3955125E-10	6.0091274E-10	5.6455344E-10
6.10	3.8741473E-10	3.6372472E-10	3.4144996E-10	3.2050801E-10	3.0082108E-10
6.20	2.0522634E-10	1.9248874E-10	1.8052405E-10	1.6928651E-10	1.5873299E-10
6.30	1.0765746E-10	1.0087687E-10	9.4514100E-11	8.8543992E-11	8.2942877E-11
6.40	5.5925076E-11	5.2351491E-11	4.9001459E-11	4.5861309E-11	4.2918187E-11
6.50	2.8768542E-11	2.6903889E-11	2.5157631E-11	2.3522413E-11	2.1991329E-11
6.60	1.4654651E-11	1.3691379E-11	1.2790171E-11	1.1947112E-11	1.1158530E-11
6.70	7.3922578E-12	6.8995870E-12	6.4391198E-12	6.0087941E-12	5.6066772E-12
6.80	3.6924994E-12	3.4430274E-12	3.2100952E-12	2.9926280E-12	2.7896194E-12
6.90	1.8264311E-12	1.7013637E-12	1.5847049E-12	1.4759003E-12	1.3744312E-12
7.00	8.9458896E-13	8.3251302E-13	7.7466849E-13	7.2077231E-13	6.7056000E-13
7.10	4.3388950E-13	4.0338530E-13	3.7498883E-13	3.4855709E-13	3.2395661E-13
7.20	2.0838582E-13	1.9354516E-13	1.7974375E-13	1.6691009E-13	1.5497751E-13
7.30	9.9103427E-14	9.1955114E-14	8.5314018E-14	7.9144766E-14	7.3414407E-14
7.40	4.6670116E-14	4.3261240E-14	4.0097410E-14	3.7161306E-14	3.4436807E-14
7.50	2.1762912E-14	2.0153468E-14	1.8661211E-14	1.7277748E-14	1.5995274E-14
7.60	1.0048966E-14	9.2966542E-15	8.5998175E-15	7.9544295E-15	7.3567513E-15
7.70	4.5946274E-15	4.2464693E-15	3.9243063E-15	3.6262274E-15	3.3504597E-15
7.80	2.0801864E-15	1.9206673E-15	1.7732063E-15	1.6369054E-15	1.5109327E-15
7.90	9.3255758E-16	8.6019640E-16	7.9337184E-16	7.3166645E-16	6.7469377E-16
8.00	4.1397018E-16	3.8147224E-16	3.5149084E-16	3.2383387E-16	2.9832366E-16
8.10	1.8196214E-16	1.6751230E-16	1.5419473E-16	1.4192194E-16	1.3061309E-16
8.20	7.9197263E-17	7.2836234E-17	6.6979507E-17	6.1587641E-17	5.6624234E-17
8.30	3.4131483E-17	3.1359128E-17	2.8809117E-17	2.6463852E-17	2.4307109E-17
8.40	1.4565141E-17	1.3368876E-17	1.2269652E-17	1.1259697E-17	1.0331855E-17
8.50	6.1544256E-18	5.6433761E-18	5.1742520E-18	4.7436570E-18	4.3484663E-18
8.60	2.5749715E-18	2.3588213E-18	2.1606019E-18	1.9788441E-18	1.8121974E-18
8.70	1.0667637E-18	9.7625187E-19	8.9333143E-19	8.1737329E-19	7.4779984E-19
8.80	4.3759648E-19	4.0007220E-19	3.6572951E-19	3.3430181E-19	3.0554455E-19
8.90	1.7774118E-19	1.6233920E-19	1.4825722E-19	1.3538338E-19	1.2361522E-19

Table S3 (continued)

x	00	01	02	03	04
9.00	1.1285884E-19	1.0302825E-19	9.4044651E-20	8.5835899E-20	7.8335909E-20
9.10	4.5165915E-20	4.1190986E-20	3.7562165E-20	3.4249647E-20	3.1226165E-20
9.20	1.7897488E-20	1.6306247E-20	1.4855011E-20	1.3531595E-20	1.2324862E-20
9.30	7.0222842E-21	6.3916175E-21	5.8170151E-21	5.2935454E-21	4.8167059E-21
9.40	2.7281536E-21	2.4806846E-21	2.2554401E-21	2.0504449E-21	1.8638970E-21
9.50	1.0494515E-21	9.5331268E-22	8.6589531E-22	7.8641615E-22	7.1416157E-22
9.60	3.9972212E-22	3.6274493E-22	3.2915582E-22	2.9864739E-22	2.7093988E-22
9.70	1.5074932E-22	1.3666856E-22	1.2389075E-22	1.1229648E-22	1.0177718E-22
9.80	5.6292823E-23	5.0984280E-23	4.6171773E-23	4.1809388E-23	3.7855419E-23
9.90	2.0813752E-23	1.8832309E-23	1.7037809E-23	1.5412777E-23	1.3941357E-23
10.00	7.6198530E-24	6.8876271E-24	6.2251473E-24	5.6258302E-24	5.0837079E-24
10.10	2.7621095E-24	2.4942138E-24	2.2520781E-24	2.0332472E-24	1.8354979E-24
10.20	9.9136251E-25	8.9432419E-25	8.0670440E-25	7.2759690E-25	6.5618185E-25
10.30	3.5230651E-25	3.1750661E-25	2.8611579E-25	2.5780292E-25	2.3226877E-25
10.40	1.2396660E-25	1.1161083E-25	1.0047660E-25	9.0444148E-26	8.1405354E-26
10.50	4.3190063E-26	3.8846774E-26	3.4936792E-26	3.1417240E-26	2.8249449E-26
10.60	1.4899011E-26	1.3387454E-26	1.2028056E-26	1.0805624E-26	9.7064672E-27
10.70	5.0889109E-27	4.5680907E-27	4.1001667E-27	3.6798088E-27	3.3022193E-27
10.80	1.7210178E-27	1.5433503E-27	1.3838869E-27	1.2407766E-27	1.1123553E-27
10.90	5.7628644E-28	5.1628174E-28	4.6247904E-28	4.1424212E-28	3.7099954E-28
11.00	1.9106596E-28	1.7100186E-28	1.5302954E-28	1.3693252E-28	1.2251658E-28
11.10	6.2721944E-29	5.6079758E-29	5.0135996E-29	4.4817753E-29	4.0059674E-29
11.20	2.0386675E-29	1.8209669E-29	1.6263522E-29	1.4523927E-29	1.2969117E-29
11.30	6.5608999E-30	5.8544763E-30	5.2235960E-30	4.6602371E-30	4.1572231E-30
11.40	2.0905954E-30	1.8636466E-30	1.6611697E-30	1.4805441E-30	1.3194277E-30
11.50	6.5957714E-31	5.8739201E-31	5.2305500E-31	4.6571857E-31	4.1462611E-31
11.60	2.0603912E-31	1.8330780E-31	1.6306813E-31	1.4504879E-31	1.2900781E-31
11.70	6.3726749E-32	5.6639810E-32	5.0335999E-32	4.4729337E-32	3.9743226E-32
11.80	1.9515573E-32	1.7328064E-32	1.5384227E-32	1.3657089E-32	1.2122648E-32
11.90	5.9173577E-33	5.2488630E-33	4.6554270E-33	4.1286747E-33	3.6611597E-33
12.00	1.7764821E-33	1.5742253E-33	1.3948573E-33	1.2358038E-33	1.0947782E-33
12.10	5.2805588E-34	4.6747081E-34	4.1379570E-34	3.6624719E-34	3.2413019E-34
12.20	1.5541198E-34	1.3744459E-34	1.2154235E-34	1.0746932E-34	9.5016317E-35
12.30	4.5287070E-35	4.0011594E-35	3.5347145E-35	3.1223362E-35	2.7577942E-35
12.40	1.3066180E-35	1.1532639E-35	1.0178075E-35	8.9817177E-36	7.9251960E-36
12.50	3.7325643E-36	3.2912114E-36	2.9017574E-36	2.5581338E-36	2.2549777E-36
12.60	1.0557226E-36	9.2996508E-37	8.1910641E-37	7.2139119E-37	6.3526976E-37
12.70	2.9564853E-37	2.6017220E-37	2.2893009E-37	2.0141959E-37	1.7719740E-37
12.80	8.1975609E-38	7.2067274E-38	6.3350254E-38	5.5682081E-38	4.8937229E-38
12.90	2.2504851E-38	1.9765045E-38	1.7357066E-38	1.5240935E-38	1.3381467E-38
13.00	6.1171566E-39				

Table S3 (continued)

x	05	06	07	08	09
9.00	7.1484170E-20	6.5225278E-20	5.9508508E-20	5.4287426E-20	4.9519528E-20
9.10	2.8466774E-20	2.5948659E-20	2.3650952E-20	2.1554571E-20	1.9642068E-20
9.20	1.1224634E-20	1.0221611E-20	9.3072962E-21	8.4739283E-21	7.7144163E-21
9.30	4.3823863E-21	3.9868346E-21	3.6266264E-21	3.2986364E-21	3.0000129E-21
9.40	1.6941535E-21	1.5397160E-21	1.3992185E-21	1.2714154E-21	1.1551713E-21
9.50	6.4848145E-22	5.8878352E-22	5.3452837E-22	4.8522468E-22	4.4042506E-22
9.60	2.4577865E-22	2.2293198E-22	2.0218904E-22	1.8335799E-22	1.6626433E-22
9.70	9.2234135E-23	8.3577611E-23	7.5726036E-23	6.8605273E-23	6.2147944E-23
9.80	3.4271988E-23	3.1024696E-23	2.8082305E-23	2.5416455E-23	2.3001395E-23
9.90	1.2609161E-23	1.1403136E-23	1.0311442E-23	9.3233391E-24	8.4290872E-24
10.00	4.5933711E-24	4.1499174E-24	3.7489042E-24	3.3863062E-24	3.0584759E-24
10.10	1.6568171E-24	1.4953822E-24	1.3495433E-24	1.2178069E-24	1.0988211E-24
10.20	5.9171769E-25	5.3353370E-25	4.8102330E-25	4.3363801E-25	3.9088187E-25
10.30	2.0924290E-25	1.8848102E-25	1.6976238E-25	1.5288759E-25	1.3767655E-25
10.40	7.3262614E-26	6.5927834E-26	5.9321503E-26	5.3371871E-26	4.8014196E-26
10.50	2.5398547E-26	2.2833091E-26	2.0524732E-26	1.8447911E-26	1.6579593E-26
10.60	8.7182529E-27	7.8298722E-27	7.0313192E-27	6.3135830E-27	5.6685490E-27
10.70	2.9630809E-27	2.6585083E-27	2.3850060E-27	2.1394288E-27	1.9189477E-27
10.80	9.9712674E-28	8.9374604E-28	8.0100424E-28	7.1781483E-28	6.4320136E-28
10.90	3.3223808E-28	2.9749684E-28	2.6636198E-28	2.3846191E-28	2.1346305E-28
11.00	1.0960744E-28	9.8048762E-29	8.7700305E-29	7.8436282E-29	7.0143882E-29
11.10	3.5803184E-29	3.1995787E-29	2.8590440E-29	2.5544993E-29	2.2821682E-29
11.20	1.1579603E-29	1.0337936E-29	9.2284950E-30	8.2372990E-30	7.3518337E-30
11.30	3.7081351E-30	3.3072319E-30	2.9493794E-30	2.6299866E-30	2.3449486E-30
11.40	1.1757276E-30	1.0475740E-30	9.3329642E-31	8.3140261E-31	7.4055965E-31
11.50	3.6910219E-31	3.2854395E-31	2.9241336E-31	2.6023027E-31	2.3156628E-31
11.60	1.1472941E-31	1.0202120E-31	9.0711623E-32	8.0647765E-32	7.1693307E-32
11.70	3.5309424E-32	3.1367147E-32	2.7862257E-32	2.4746536E-32	2.1977052E-32
11.80	1.0759540E-32	9.5487563E-33	8.4733816E-33	7.5183681E-33	6.6703293E-33
11.90	3.2462619E-33	2.8780961E-33	2.5514313E-33	2.2616185E-33	2.0045258E-33
12.00	9.6974966E-34	8.5891457E-34	7.6067153E-34	6.7359866E-34	5.9643362E-34
12.10	2.8682798E-34	2.5379345E-34	2.2454126E-34	1.9864093E-34	1.7571069E-34
12.20	8.3997961E-35	7.4249946E-35	6.5626673E-35	5.7999131E-35	5.1253016E-35
12.30	2.4355714E-35	2.1507837E-35	1.8991070E-35	1.6767140E-35	1.4802170E-35
12.40	6.9922582E-36	6.1685309E-36	5.4413026E-36	4.7993325E-36	4.2326821E-36
12.50	1.9875501E-36	1.7516638E-36	1.5436195E-36	1.3601494E-36	1.1983669E-36
12.60	5.5937411E-37	4.9249675E-37	4.3357198E-37	3.8165933E-37	3.3592892E-37
12.70	1.5587262E-37	1.3710053E-37	1.2057722E-37	1.0603476E-37	9.3236945E-38
12.80	4.3005115E-38	3.7788328E-38	3.3201068E-38	2.9167773E-38	2.5621898E-38
12.90	1.1747695E-38	1.0312369E-38	9.0515094E-39	7.9440212E-39	6.9713452E-39

Table S4. Critical values of the chi-square distribution. When 9 right signs were not ensured values with fewer signs are displayed

Z			Pr	obability greater th	han the critical val	ue		
	0.001	0.005	0.010	0.025	0.050	0.100	0.250	0.500
1	1.0827566E+01	7.879439E+00	6.634897E+00	5.0238862E+00	3.8414588E+00	2.70554345E+00	1.32330370E+00	4.5493642E-01
0	1.38155106E+01	1.05966347E+01	9.21034037E+00	7.37775891E+00	5.99146455E+00	4.60517019E+00	2.77258872E+00	1.38629436E+00
З	1.626624E+01	1.2838156E+01	1.1344867E+01	9.3484036E+00	7.8147279E+00	6.2513886E+00	4.10834493E+00	2.36597388E+00
4	1.8466827E+01	1.486026E+01	1.32767041E+01	1.11432868E+01	9.48772904E+00	7.77944034E+00	5.38526906E+00	3.3566940E+00
S	2.05150057E+01	1.67496023E+01	1.50862725E+01	1.28325020E+01	1.10704977E+01	9.23635690E+00	6.62567976E+00	4.35146019E+00
9	2.2458E+01	1.85475842E+01	1.68118938E+01	1.44493753E+01	1.25915872E+01	1.06446407E+01	7.84080412E+00	5.34812063E+00
\sim	2.4321886E+01	2.02777399E+01	1.84753069E+01	1.60127643E+01	1.40671404E+01	1.20170366E+01	9.03714755E+00	6.34581120E+00
×	2.6124482E+01	2.19549550E+01	2.00902350E+01	1.75345461E+01	1.55073131E+01	1.33615661E+01	1.02188550E+01	7.34412150E+00
6	2.78772E+01	2.358935E+01	2.1665994E+01	1.9022768E+01	1.6918978E+01	1.46836566E+01	1.13887514E+01	8.3428327E+00
10	2.95882984E+01	2.51881796E+01	2.32092512E+01	2.04831774E+01	1.83070381E+01	1.59871792E+01	1.25488614E+01	9.34181777E+00
11	3.12641336E+01	2.67568489E+01	2.47249703E+01	2.19200493E+01	1.96751376E+01	1.72750085E+01	1.37006928E+01	1.03409981E+01
12	3.2909490E+01	2.82995187E+01	2.62169672E+01	2.33366641E+01	2.10260698E+01	1.85493478E+01	1.48454037E+01	1.13403224E+01
13	3.45282E+01	2.981947E+01	2.7688250E+01	2.4735605E+01	2.236203E+01	1.98119293E+01	1.59839062E+01	1.23397559E+01
14	3.612327E+01	3.1319350E+01	2.9141238E+01	2.6118948E+01	2.3684791E+01	2.10641442E+01	1.7116934E+01	1.3339274E+01
15	3.769730E+01	3.2801321E+01	3.0577914E+01	2.74883929E+01	2.49957901E+01	2.23071296E+01	1.82450856E+01	1.43388595E+01
16	3.92524E+01	3.4267187E+01	3.19999269E+01	2.88453507E+01	2.62962276E+01	2.35418289E+01	1.93688602E+01	1.53384989E+01
17	4.0790217E+01	3.57184657E+01	3.34086636E+01	3.01910091E+01	2.75871116E+01	2.4769035E+01	2.04886762E+01	1.63381824E+01
18	4.2312396E+01	3.71564515E+01	3.48053057E+01	3.15263784E+01	2.88692994E+01	2.59894231E+01	2.16048898E+01	1.73379024E+01
19	4.38201960E+01	3.85822566E+01	3.61908691E+01	3.28523269E+01	3.01435272E+01	2.72035710E+01	2.27178067E+01	1.83376529E+01
20	4.53147466E+01	3.99968463E+01	3.75662348E+01	3.41696069E+01	3.14104328E+01	2.84119806E+01	2.38276920E+01	1.93374292E+01
21	4.6797038E+01	4.14010648E+01	3.89321727E+01	3.54788759E+01	3.26705733E+01	2.96150894E+01	2.49347770E+01	2.03372276E+01
22	4.82679423E+01	4.27957E+01	4.02893604E+01	3.67807121E+01	3.39244385E+01	3.08132823E+01	2.60392650E+01	2.13370448E+01
23	4.97282325E+01	4.4181275E+01	4.16383981E+01	3.80756273E+01	3.51724616E+01	3.20068997E+01	2.71413360E+01	2.23368784E+01
24	5.11785978E+01	4.55585119E+01	4.29798201E+01	3.93640770E+01	3.64150285E+01	3.31962443E+01	2.82411500E+01	2.33367263E+01
25	5.26196558E+01	4.69278902E+01	4.43141049E+01	4.06464691E+01	3.76524841E+01	3.43815870E+01	2.93388503E+01	2.43365867E+01
26	5.40519624E+01	4.82898823E+01	4.56416827E+01	4.19231701E+01	3.88851387E+01	3.55631713E+01	3.04345654E+01	2.53364581E+01

Table S4 (continued)

Table S4 (continued)

2.63363393E+01 2.93360315E+01 3.03359425E+01 3.13358591E+01 3.23357809E+01 3.33357074E+01 3.43356381E+01 3.53355728E+01 3.63355111E+01 3.73354527E+01 3.83353974E+01 4.03352949E+01 4.13352474E+01 4.23352022E+01 4.33351590E+01 4.43351178E+01 4.53350784E+01 4.63350407E+01 4.73350046E+01 8.53505646E+01 7.82307081E+01 7.49194743E+01 7.02224136E+01 6.63386489E+01 6.20375368E+01 5.52653399E+01 4.83349699E+01 8.66608152E+01 7.94899785E+01 7.61538912E+01 7.14201952E+01 6.75048065E+01 6.31671210E+01 5.63336049E+01 4.93349367E+01 2.73362292E+01 2.83361269E+01 3.93353448E+01 0.5007.36826385E+01 6.90225858E+01 6.51707689E+01 6.09066070E+01 5.41963650E+01 3.79159225E+01 3.26204941E+01 4.34619070E+01 5.97742889E+01 5.31266576E+01 4.01132721E+01 3.67412167E+01 3.15284116E+01 3.37109086E+01 4.13036155E+01 5.21923197E+01 4.83634084E+01 4.23833057E+01 4.45394627E+01 3.47997425E+01 3.58870759E+01 3.91407790E+01 4.02227899E+01 4.56160136E+01 4.66915977E+01 4.77662506E+01 4.88400060E+01 4.99128954E+01 5.09849487E+01 5.20561939E+01 3.69729821E+01 3.80575290E+01 0.250 5.09984602E+01 4.72121739E+01 3.90874698E+01 4.98018496E+01 4.60587884E+01 5.33835406E+01 4.95125798E+01 5.06597705E+01 5.18050572E+01 5.86405374E+01 4.49031575E+01 5.29485120E+01 5.40902025E+01 4.37729718E+01 4.02560237E+01 4.14217358E+01 4.37451796E+01 5.52301921E+01 5.63685407E+01 4.25847451E+01 5.7505305E+01 0.100 Probability greater than the critical value 4.13371382E+01 4.86023674E+01 5.45722278E+01 6.40011120E+01 4.25569678E+01 4.49853433E+01 4.61942595E+01 4.73998839E+01 5.57584793E+01 5.69423871E+01 5.81240377E+01 5.93035120E+01 6.04808866E+01 6.16562334E+01 6.28296204E+01 0.050 4.31945110E+01 4.82782358E+01 4.44607918E+01 7.24433074E+01 6.78206470E+01 4.5722858E+01 5.56679733E+01 5.68955205E+01 5.32033485E+01 5.44372936E+01 5.81200597E+01 6.66165288E+01 4.69792422E+01 4.82318896E+01 5.07250801E+01 5.19659952E+01 5.93417071E+01 6.05605717E+01 6.42014615E+01 6.54101590E+01 4.94804377E+01 6.17767558E+01 6.29903555E+01 0.025 4.69629421E+01 4.95878845E+01 5.08921813E+01 5.86192145E+01 5.9892500E+01 6.11620868E+01 6.24281210E+01 6.36907398E+01 7.12014003E+01 5.21913948E+01 5.34857718E+01 6.49500713E+01 6.99568321E+01 5.47755398E+01 5.60609087E+01 5.73420734E+01 6.62062363E+01 6.74593479E+01 6.87095130E+01 0.010 4.96449153E+01 5.09933763E+01 7.69687677E+01 5.23356178E+01 6.02747709E+01 6.15811791E+01 6.28833354E+01 6.41814124E+01 6.54755709E+01 6.67659618E+01 7.44365354E+01 7.57040731E+01 5.76484453E+01 5.89639259E+01 6.80527265E+01 6.93359975E+01 7.31660608E+01 5.36719619E+01 5.50027039E+01 5.63281150E+01 7.06158996E+01 7.18925505E+01 0.005 8.27204225E+01 8.40371337E+01 5.68922854E+01 6.93464525E+01 5.54760202E+01 6.66188288E+01 6.79851676E+01 7.07028874E+01 7.2054663E+01 7.34019575E+01 8.14003257E+01 5.83011735E+01 6.52472175E+01 7.47449384E+01 7.74185782E+01 7.87495242E+01 8.00767320E+01 5.97030643E+01 6.24872191E+01 6.38700985E+01 7.60837627E+01 6.10983061E+01 0.001 49 28 29 30 35 36 38 39 40 46 47 48 50 33 33 45 37 4 4 43 4 45 5 31 z

Table S4 (continued)

Z		57	28	29	30	31	32	33	34	35	36	7	38	39	0‡	†1	1 2	1 3	4	1 5	1 6	L†	1 8	6t	50
~		0	1 2	1 2	11 3	11 3	11 3	11 3	11 3	11 3	11 3	11 3	1 3	1 3	01 4	1	1	11 4	1	11 4	11 4	11	11 4	10	1 5
		E+(E+C	E+(E+C	Ε+C	E+()H+(3E+C)HH(E+C	3E+C	3E+()E+(EHC EHC	Ε+C)E+()H+(E+(E+()H+(E+(E+(Ξ+C	3E+(
	666.	269Z	8791	0535	951]	2504	654(889(698	847(1128	2903	1868	622(426	441	5169	512(2936	7359	720(1332	868(8247	9053
	0	3027	3390	986	1587	2196	2810	3430	4056	4687	5324	5965	5611	7261	7916	3575	9238	9 05	J576	1250	1928	2610	3294	3982	4673
		3.6	1.0	1.0	1.	1.1	1.5		1.4	1.4	1.5	1.5	1.6			1.8	1.5	1.9	5.0	5	5	22	2	5.0	5.4
		E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	E+01	3+01	E+01	E+01	E+01
	995	874]	359]	489]	199]	'674]	321	744	[725]	3203	'265]	3125	116	679]	353]	'768]	633]	136	932]	142	343]	557E	1016	161	489]
	0	8075	4613	1211	7867	4577	1340	8152	5012	1918	8867	5858	2885	9958	7065	4207	1384	8594	5836	3110	0413	774	5105	2493	7066
		1.1	1.2°	1.3	1.3	1.4	1.5	1.5	1.6	1.7	1.7	1.8	1.9	1.9	2.0	2.1	2.2	2.2	2.3	2.4	2.5	2.5	2.6	2.7	2.7
		+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01	+01
Je	06)44E	98E	546E	65E	64E	155E	37E	169E	262E	758E	320E	121E	331E	513E	11E	947E	10E	54E	92E	91E	H69E	89E	160E	827E
valı	0.9	7850	647(5645	5345	5545	6221	7351	8912	0892	3267	6023	9142	2616	6426	0561	5005	976(4802	0126	5723	1584	7700	4062	0668
itical		1.28	1.35	1.42	1.49	1.56	1.63	1.70	1.77	1.85	1.92	1.99	2.06	2.14	2.21	2.29	2.36	2.43	2.51	2.59	2.66	2.74	2.81	2.89	2.97
le cr		-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01	-01
greater than th	0.975	27E4)6E4	17E4	23E4	36E4	49E4	15E4	29E4	56EH	16E4	72E4	23E4	46E+	92E4	36E4	20E4	42E4	57E4	23E4	41E-	57EH	57E4	55EH	37E4
		3382	786	707	CLT0	8738	076	.999	6252	937(588	562	8482	432	3039	4518	866	5374	456	6152	0027	619	450	4910	736
		1.457	1.530	l.604	1.679	l.753	1.829	1.904	1.980	2.056	2.133	2.210	2.287	2.365	.443	2.521	2.595	2.678	2.757	2.836	2.916	2.995	3.075	3.155	3.235
ity g		01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01
lidac	C	8E+I	0E+I	2E+I	0E+I	6E+I	5E+I	0E+I	7E+(2E+I	0E+I	6E+I	4E+	4E+	2E+(5E+I	5E+I	7E+I	1E+	1E+	3E+I	5E+I	4E+(6E+I	7E+I
Prol	0.95(1395	7875	3366	2661)568	1913	5534	t280	5015	8609	t942	3904	5390	9303	5551	t049	t716	7477	2259	3995	7621	3077	305	t251
		6151	6927	3077.0	8492	928(001	086	1664	246	3268	407	488	5695	6509	7325	8142	8967	9787	0612	1438	2267	3098	393(4764
		1 1.	1 1.	1 1.	1 1.	1	1 2.	1	1	1	1 2.	1 2.	1 2.	1 2.	1 2.	1 2.	1 2.	1 2.	1 2.	1 3.	1 3.	1 3.	1 3.	1 3.	1 3.
	006	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0	E+0
		3960	2424	7436	2346	5645	5945	1967	2533	5548	2999	943	9500	7852	5229)914	4 2 30	4544	1258	3809	1665	4324	1310	2173	5484
	0	1138	9392	767	5992	433	2705	110	9522	7960	643.	492(3429	195	050)70Q	7654	6254	487	350	215	081	949	818	688
		1.8	1.8	1.9	2.0	2.1	2.2	2.3	2.3	4.7	2.5	2.6	2.7	2.8	2.9	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.5	3.6	3.7
		3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01	3+01
	50	050E	557E	861E	07.7E	393E	066E	412E	797E	63.7E	390E	552E	653E	256E	949E	351E	100E	859E	309E	151E	100E	890E	268E	993E	838E
	0.	494	571	665	9776	901	041	194	360	539	730	932	3145	369	602	846	660	360	631	910	197	491	794	103	420
		2.17	2.26	2.35	4.	2.53	2.63	2.72	2.81	2.90	2.99	3.08	3.18	3.27	3.36	3.45	3.55	3.64	3.73	3.82	3.92	4.01	4.10	4.20	4.25

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Издательский отдел Объединенного института ядерных исследований 141980, г. Дубна, Московская обл., ул. Жолио-Кюри, 6. E-mail: publish@jinr.ru www.jinr.ru/publish/